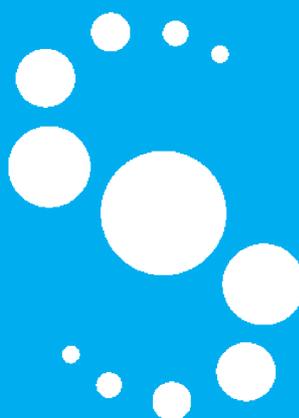


COMUNE DI SCANDICCI

SCANDICCI CENTRO Srl



Project Financing “Nuovo Centro Civico e
Stazione Tramvia Veloce Firenze S.M.N. - Scandicci”

PROGETTO ESECUTIVO

5.2.3 - Calcoli Esecutivi Strutture Edificio Direzionale

rev. A 10.12.2009

COMUNE DI SCANDICCI

Scandicci Centro Srl



Scandicci Centro

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PROGETTO ESECUTIVO

5.2.3 CALCOLI ESECUTIVI STRUTTURE EDIFICIO DIREZIONALE

rev. A 10.12.2009

POLITECNICA Soc. Coop.
Ing. Andrea Dal Cerro

INDICE

1. GENERALITA'	2
1.1. PREMESSA	2
1.2. DESCRIZIONE DEL MODELLO DI CALCOLO	2
1.3. MODELLAZIONI EFFETTUATE	3
2. MODELLAZIONE A	8
2.1. FATTORE DI STRUTTURA	8
2.2. PARAMETRI DI CALCOLO	9
2.3. VALUTAZIONE DEL PARAMETRO θ	22
2.3.1. <i>Metodo di calcolo</i>	22
2.3.2. <i>Risultati</i>	22
2.4. SPOSTAMENTI RELATIVI MASSIMI	23
2.5. MODI DI VIBRARE	24
2.5.1. <i>Primo modo di vibrare periodo 1.447 s.</i>	24
2.5.2. <i>Secondo modo di vibrare periodo 1.182 s.</i>	24
2.6. INVILUPPO DIAGRAMMI SOLLECITAZIONI	25
2.7. PERCENTUALE DI SFRUTTAMENTO DEI CONTROVENTI METALLICI	26
2.8. -VERIFICA NODI IN ACCIAIO	27
2.8.1. <i>Nodo controvento tipo a</i>	27
2.8.2. <i>Nodo controvento tipo</i>	29
2.8.3. <i>Collegamento tubolari $\varnothing 101.6 \times 8$ alla struttura in c.a.</i>	30
3. MODELLAZIONE B	31
3.1. PARAMETRI DI CALCOLO	31
3.2. MAPPE D'ARMATURA SOLETTA SUPERIORE BLOCCO A	45
4. MODELLAZIONE C	50
4.1. FATTORE DI STRUTTURA	50
4.2. PARAMETRI DI CALCOLO SCALE IN CA	50
4.3. SPOSTAMENTI DIFFERENZIALI MASSIMI SCALA IN C.A.	69
4.4. MAPPE D'ARMATURA SOLETTA SUPERIORE BLOCCO B	70
5. MODELLAZIONE D	72
5.1. PARAMETRI DI CALCOLO	72
5.2. PRESSIONI SUL TERRENO	121
5.3. MAPPE DI ARMATURA ELEMENTI PLATEA DI FONDAZIONE	122
6. MODELLAZIONE E	134
6.1. PERCENTUALE DI SFRUTTAMENTO DEI PROFILATI METALLICI	134
7. CABINA ENEL	135
7.1. PARAMETRI DI CALCOLO STRUTTURA IN ELEVAZIONE	135
7.2. MAPPE D'ARMATURA SOLETTA PIANO TERRA	146
7.3. PARAMETRI DI CALCOLO PER CALCOLO FONDAZIONI CABINA ENEL	150
7.4. MAPPE D'ARMATURA PLATEA DI FONDAZIONE	159
7.5. TENSIONE SUL TERRENO	161
7.6. ALLEGATI IN FORMATO DIGITALE	161

1. GENERALITA'

1.1. PREMESSA

La presente documentazione è relativa al progetto esecutivo delle opere strutturali inerenti il project financing per la realizzazione del "Nuovo Centro Civico e Stazione Tramvia Veloce Firenze S.M.N. – Scandicci" nel comune di Scandicci in provincia di Firenze. In particolare, la presente relazione riporta il fascicolo dei calcoli eseguiti per il dimensionamento delle strutture dell'edificio 3 "Direzionale" e deve essere letta avendo come riferimento anche gli altri elaborati di progetto, sia grafici che dattiloscritti, riportati nello specifico documento "elenco elaborati". Considerando il gran numero di verifiche eseguite, si riporta in forma cartacea un inquadramento complessivo delle elaborazioni svolte e una sintesi dei risultati, rimandando ad allegati su supporto digitale per eventuali ulteriori approfondimenti.

L'edificio 3 è costituito da tre blocchi strutturali separati, in elevazione, da giunti sismici. Nel presente documento è riportato anche il fascicolo di calcolo relativo anche al parcheggio con sopra la cabina Enel, blocco strutturale compreso fra le "Residenze" ed il "Direzionale".

1.2. DESCRIZIONE DEL MODELLO DI CALCOLO

Si esegue il calcolo delle strutture degli edifici mediante modelli tridimensionale agli elementi finiti.

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:

ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. – Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:

Xfinest ver. 8.1, prodotto da Ce.A.S. S.r.l. – Milano

Le strutture in acciaio sono state verificate con il programma steelword che applica l'eurocodice 3 con i DAN riportati nella normativa italiana.

Ogni struttura è stata modellata utilizzando per i pilastri e per le travi elementi tipo "beam", ovvero elementi monodimensionali tipo asta, definiti mediante due nodi "i" e "j" posti alle estremità e dotati di varie proprietà (sezione, orientamento nello spazio etc.) ed in particolare di una terna cartesiana locale di riferimento, destrorsa, il cui asse 1 coincide con l'asse dell'elemento.

In particolare il programma distingue – in fase di verifiche- tra elementi tipo "trave" e tipo "pilastro", cui in fase post-calcolo vengono applicati i diversi criteri di verifica previsti dalla normativa utilizzata.

Le pareti in c.a., ed i muri perimetrali dell'interrato sono stati modellati utilizzando elementi bidimensionali tipo "setto", definiti da quattro nodi i,j,k,l, posti agli angoli di ogni singolo elemento e caratterizzati da comportamento flessionale e uno spessore costante. Anche tali elementi hanno una terna locale cartesiana destrorsa, in cui l'asse 3 coincide con la normale al piano medio dell'elemento, nonché proprietà di massa e rigidità funzione delle caratteristiche del materiale e della geometria del singolo elemento.

Le platee sono modellate utilizzando elementi bidimensionali tradizionali a quattro nodi caratterizzati da comportamento flessionale e/o membranale e da uno spessore costante, che hanno un sistema di riferimento locale dato da una terna cartesiana destrorsa in cui l'asse 3 coincide con la normale al piano medio dell'elemento. Tali elementi in fondazione sono caratterizzati anche da un valore del coefficiente di sottofondo o coefficiente di risposta alla Winkler per suolo elastico lineare.

I solai ai vari livelli sono stati modellati utilizzando l'opzione "solaio", che definisce superfici caricate in direzione verticale. Per tenere conto dell'effetto "piano rigido" del solaio si utilizza l'opzione "definizione impalcato rigido" che attiva un metodo di valutazione degli spostamenti nel piano dei nodi che ne fanno parte del tipo master-slave, vincolando rigidamente tutti i nodi ad un nodo principale, che solitamente è il baricentro di massa di piano. L'effetto combinato di queste due opzioni consente di definire solai rigidi unidirezionali (o bidirezionali) in cui le azioni permanenti ed accidentali sono valutate in diverse condizioni elementari di carico. E' stato assegnato l'impalcato 0 ai nodi non collegati ad un piano rigido Il movimento dei nodi appartenenti al solaio 0 risulta indipendente ma la massa relativa è comunque stata considerata.

La risoluzione dell'analisi dinamica è stata sviluppata mediante il metodo standard, detto di Subspace Iteration.

1.3. MODELLAZIONI EFFETTUATE

Come detto in premessa e meglio specificato nella relazione illustrativa, l'edificio 3 è composto da 3 blocchi strutturali indipendenti in elevazione sostenuti da una fondazione comune. Sono state eseguite pertanto le seguenti modellazioni.

A) Per l'edificio alto centrale è stato eseguito inizialmente un modello agli elementi finiti della sola struttura in elevazione incastrando il piede dei pilastri e dei setti e dando un vincolo di appoggio semplice ai nodi della scala metallica esterna. La geometria della scala metallica esterna è stata semplificata al fine di attribuire correttamente i carichi e le masse sismiche ma eliminando forme dinamiche secondarie per lo studio della struttura principale in elevazione. Successivamente, la scala metallica è stata analizzata nel dettaglio mediante una modellazione separata.

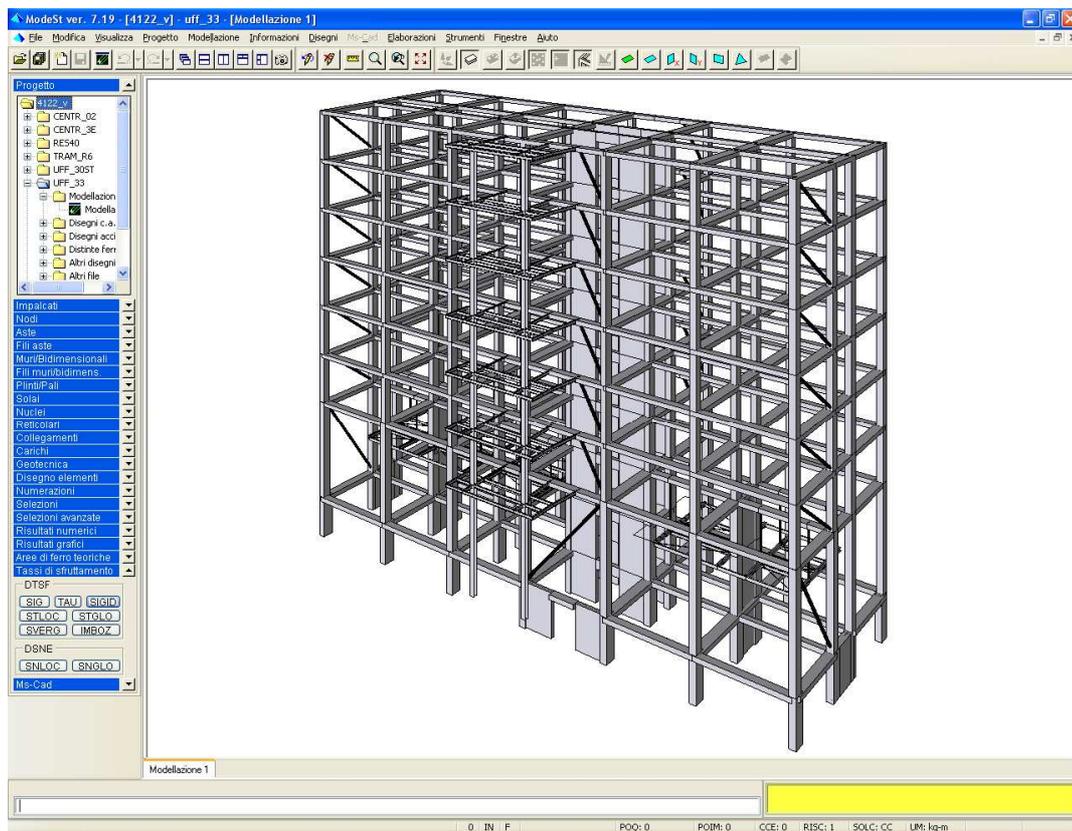


Figura 1 – modello della struttura centrale in elevazione

Nel modello sono state inserite come carichi nodali le reazioni delle mensole che sostengono la soletta del blocco a parcheggio presente inferiormente.

Poiché i controventi sono pensati per reagire solamente a trazione, né è stato modellato solamente uno e per tale elemento non è stata effettuata la verifica di instabilità. E' stato comunque fatto anche la verifica con un modello agli elementi finiti dove sono stati inseriti entrambi i controventi. Nella seguente immagine è mostrato il modello agli elementi finiti che, ad esclusione dei controventi è uguale al precedente. Nel fascicolo di calcolo in versione digitale sono riportate le verifiche degli elementi.

Il calcolo è stato sviluppato senza impalcati rigidi per considerare eventuali sollecitazioni di membrana sulla soletta.

Non sono state modellate le mazzette del blocco ascensore e delle porte.

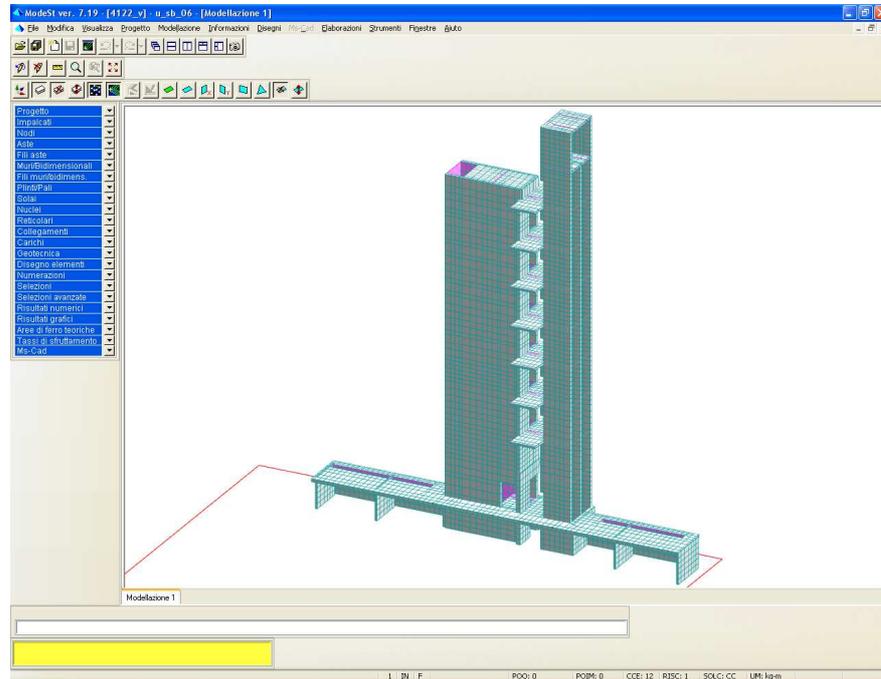


Figura 4 – modello della struttura in elevazione del parcheggio e della scala superiore A

D) Per l'analisi ed il dimensionamento delle fondazioni è stato sviluppato un modello complessivo con le tre strutture in elevazione e la fondazione a comune. Tale modello è stato risolto utilizzando un fattore di struttura unitario poiché come riportato al paragrafo 7.2.5 le fondazioni devono essere progettate per rimanere in campo elastico e devono essere dimensionate eseguendo la gerarchia delle resistenze amplificando le sollecitazioni nella platea in funzione delle resistenze degli elementi soprastanti; tuttavia, il valore di verifica deve essere limitato a quello derivante da un'analisi elastica della struttura in elevazione eseguita con il fattore di struttura unitario. Per semplicità sono stati assunti direttamente i valori derivanti da quest'ultimo tipo di analisi: tali valori sono cautelativi in quanto sono una limitazione superiore.

La fondazione è stata modellata su suolo di tipo elastico alla Winkler.

Le mensole sono state modellate assegnando un vincolo capace di trasferire solamente un'azione di taglio verticale.

Al fine di eccitare le masse, agli elementi bidimensionali del piano terra è stato assegnato un numero di solaio, uno per la parte inferiore un altro per quella superiore.

Le altre parti sono state modellate in conformità a quanto già eseguito per le strutture in elevazione.

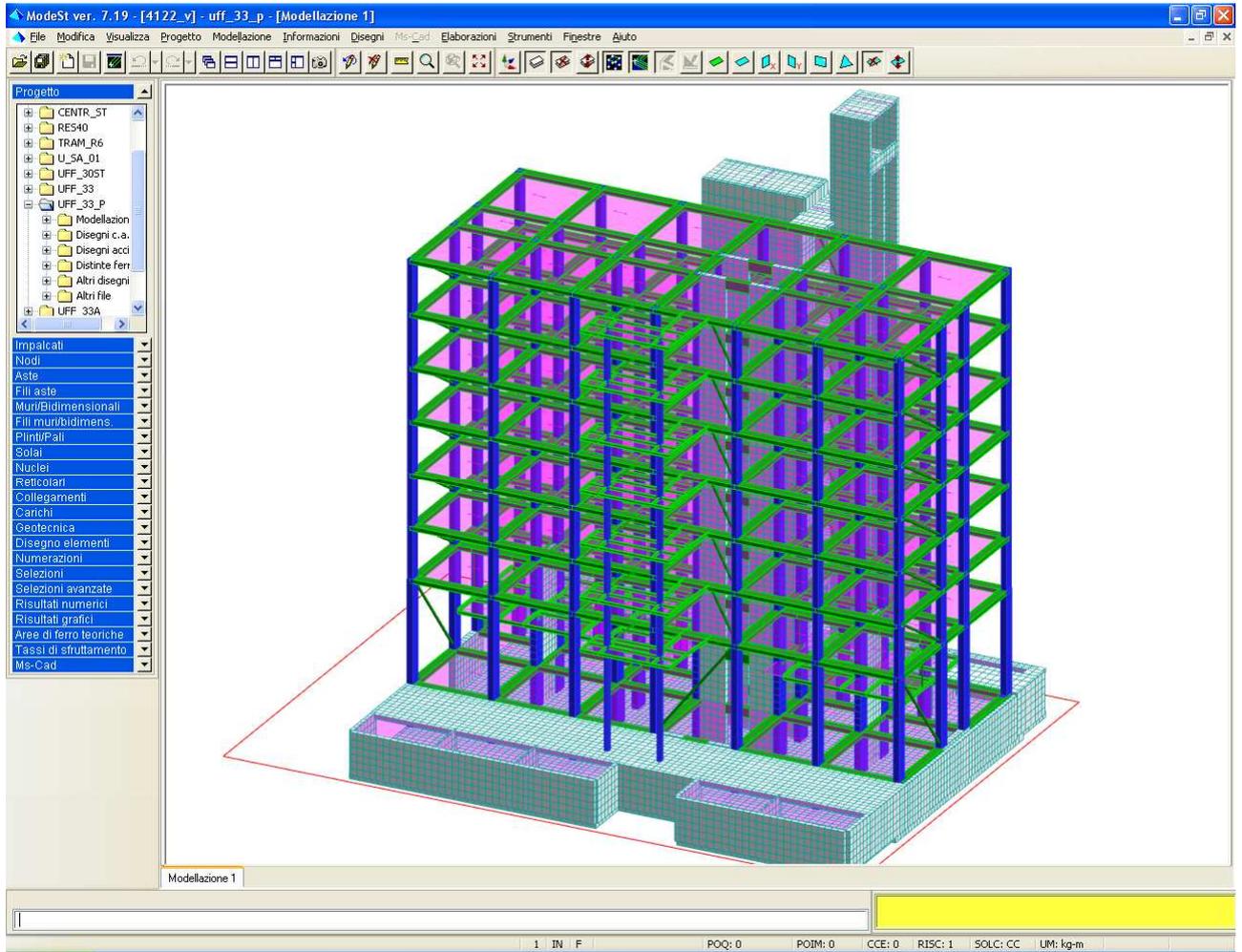


Figura 5 – modello complessivo della struttura

E) Modello di dettaglio della scala metallica. In tale modello i nodi collegati all'edificio principale sono stati vincolati con vincolo di cerniera. E' stato aggiunto il vento come azione che nell'edificio principale è stato ignorato.

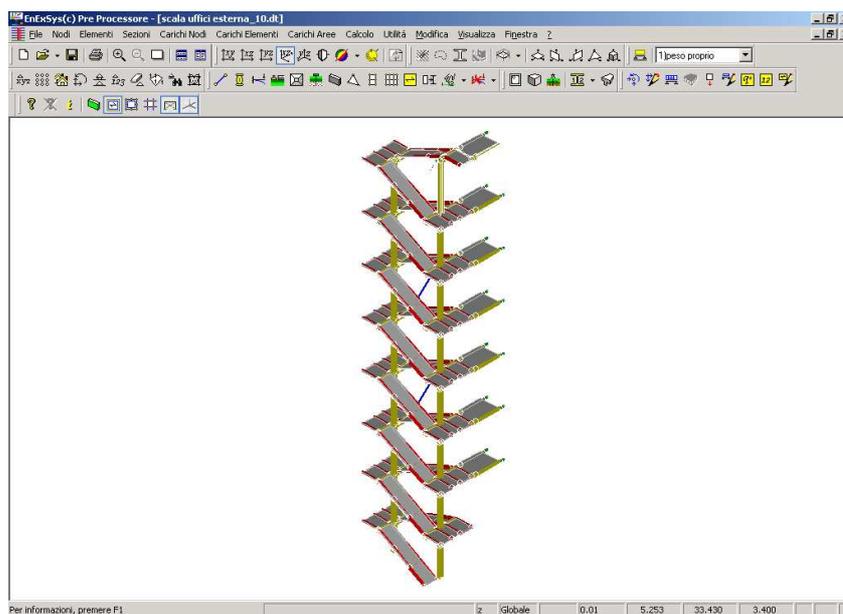


Figura 6 – modello di dettaglio della scala metallica

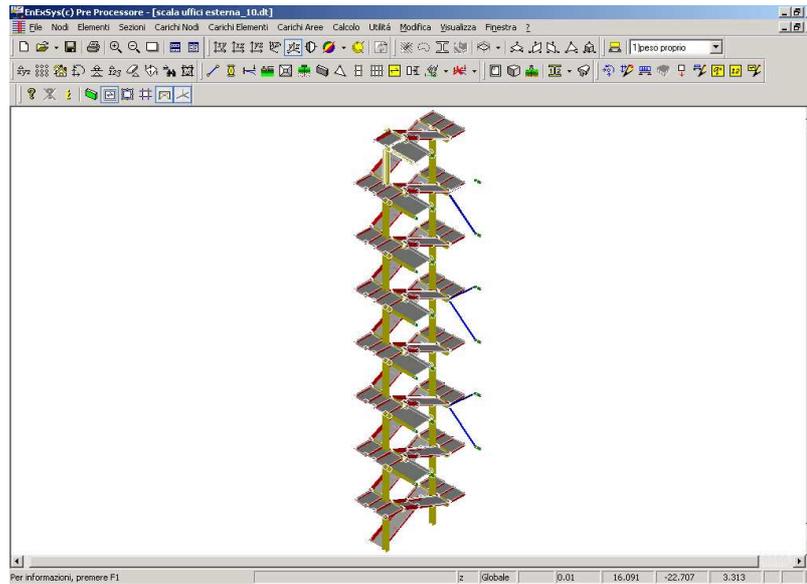


Figura 7 – modello di dettaglio della scala metallica

F) Modello della cabina Enel, struttura compresa fra il blocco delle residenze e quello direzionale. Anche nel presente caso è stato fatto un modello con incastri alla base per la verifica della struttura in elevazione ed un altro con platea su suolo elastico per e coefficiente di struttura unitario per lo studio delle fondazioni.

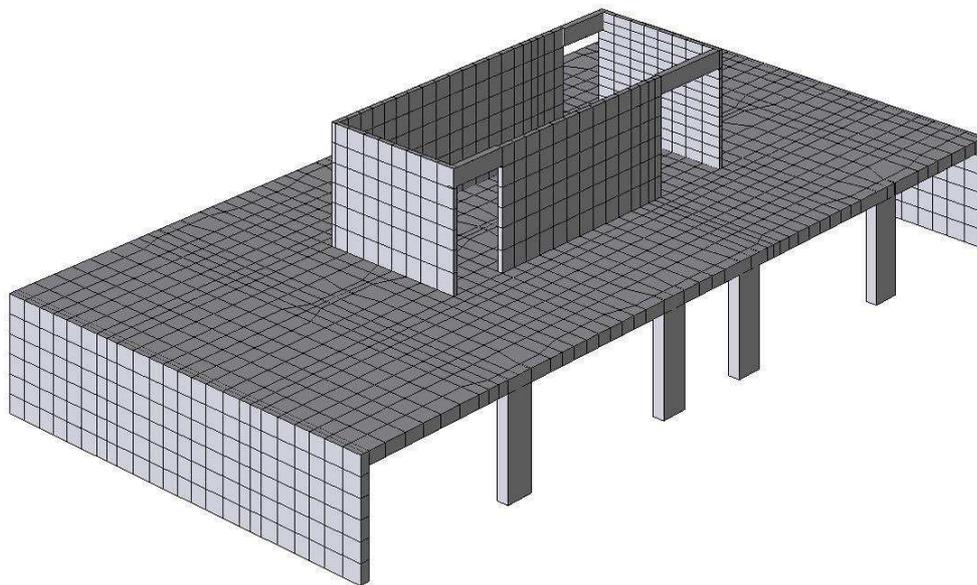


Figura 8 – modello struttura in elevazione cabina Enel

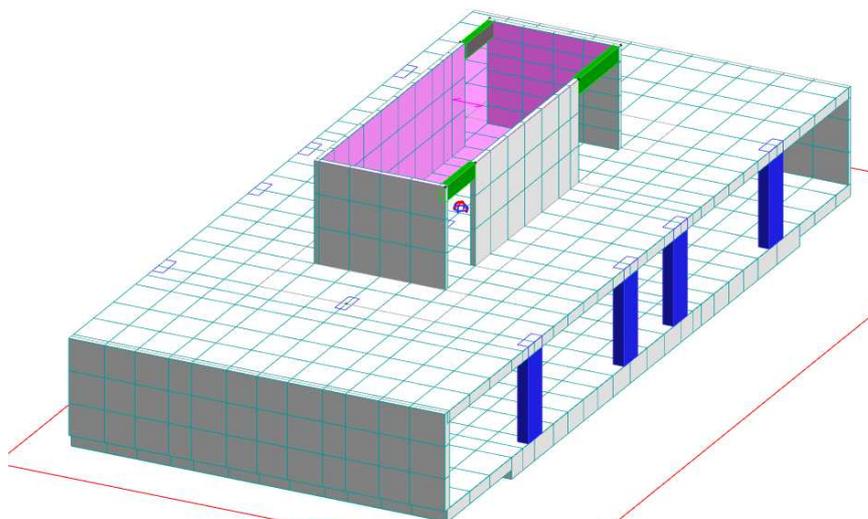


Figura 9 – modello struttura complessiva cabina Enel

2. MODELLAZIONE A

2.1. FATTORE DI STRUTTURA

La struttura non possiede un unico sistema sismo resistente sia per quanto riguarda le due direzioni d'ingresso del sisma sia lungo lo sviluppo in altezza: infatti, il sistema di controventi metallici non arriva fino in fondazione e, in direzione trasversale, i controventi diagonali sono concentrici mentre in quella longitudinale, i controventi sono eccentrici, tranne alla prima elevazione fuori terra dove sono a croce. Per tutta l'altezza in direzione longitudinale e fino al piano primo in quella trasversale vi è anche la presenza di setti sismo resistenti in c.a. E' stato valutato il fattore di struttura per ogni tipologia strutturale ipotizzata ed è stato assunto, cautelativamente, il fattore di struttura più basso. Il progetto è sviluppato con classe di duttilità bassa.

1. Strutture intelaiate con controventi eccentrici (tabella 7.5.II, tipologia c) $q_s=4$.
2. Strutture intelaiate con controventi a diagonale tesa attiva (tabella 7.5.II, tipologia b1) $q_s=4$.
3. Strutture a pareti non accoppiate (tabella 7.4.I) $q_s=3$.

La struttura non è regolare in altezza; per cui il fattore di struttura più basso risulta $3 \times 0.8 = 2.4$.

La struttura è regolare in pianta ad esclusione del piano del mezzanino.

La struttura non è stata considerata mista telaio pareti poiché all'interrato anche la maggioranza del carico verticale, oltre a quello orizzontale, è assorbito dai setti. Infatti, si valutano sinteticamente le aree d'influenza dei pilastri e dei setti da cui si evince quanto asserito.

aree d'influenza pilastri

n°	lunghezza d'influenza x	lunghezza d'influenza y	Area	
4	3	3.15	37.8	spigolo
6	6	3.15	113.4	bordo longitudinale
2	6	4.1	49.2	interni
			200.4	totale

aree d'influenza setti

n°	lunghezza d'influenza x	lunghezza d'influenza y	Area	
4	3	4.1	49.2	bordo laterale
4	6	3.15	75.6	bordo longitudinale
8	6	4.1	196.8	interni
			321.6	totale

2.2. PARAMETRI DI CALCOLO

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con: ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti: Xfinest ver. 8.1, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08

Tipo di calcolo: analisi sismica dinamica

Schematizzazione piani rigidi: metodo Master-Slave

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <kg/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: Sì
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per Buckling: No
- Trascura Buckling torsionale: No

Dati struttura

- Zona sismica: zona 3
- Sito di costruzione: scandicci 43.758015,11.182408 LON. 11.18240 LAT. 43.75800
Contenuto tra ID reticolo: 20058 20057 20280 20279

Simbologia

TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo

SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività

Ag = Accelerazione orizzontale massima al sito
 FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

TCC	Ag	FO	TC*
SLO	0.5163	2.59	0.26
SLD	0.6103	2.63	0.28
SLV	1.4446	2.39	0.30

- Tipo di opera: Opera ordinaria
- Vita nominale V_N : 50.00
- Classe d'uso: classe III
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 34.16 <m>
- Numero piani edificio: 9
- Coefficiente θ : 0
- Edificio regolare in altezza: no
- Edificio regolare in pianta: no
- Forze orizzontali convenzionali per stati limite non sismici: no

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. o prefabbricato a pareti non accoppiate

Coeff. C_1	0.05
Periodo T_1	0.70649
Coeff. λ SLO	0.85
Coeff. λ SLD	0.85
Coeff. λ SLV	0.85
Rapporto di sovraresistenza (α_s/α_r)	1.05
Valore di riferimento del fattore di struttura (q_0)	3.00
Fattore riduttivo (K_w)	1.00
Fattore di struttura (q)	2.40

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica: 1.00
- Modi da calcolare: 210
- Modi da considerare: con singola massa superiore a 1.00%
- Smorzamento spettro: 5.00

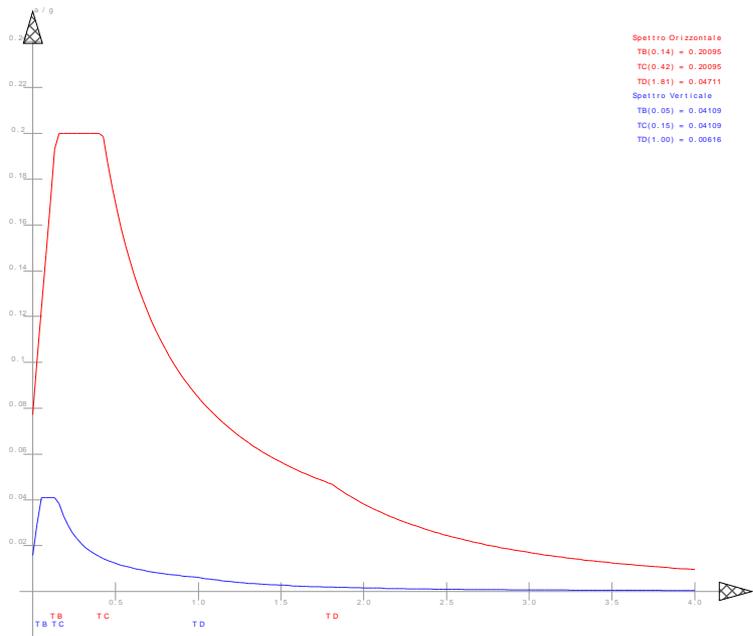


Figura numero 1: Spettro allo SLO

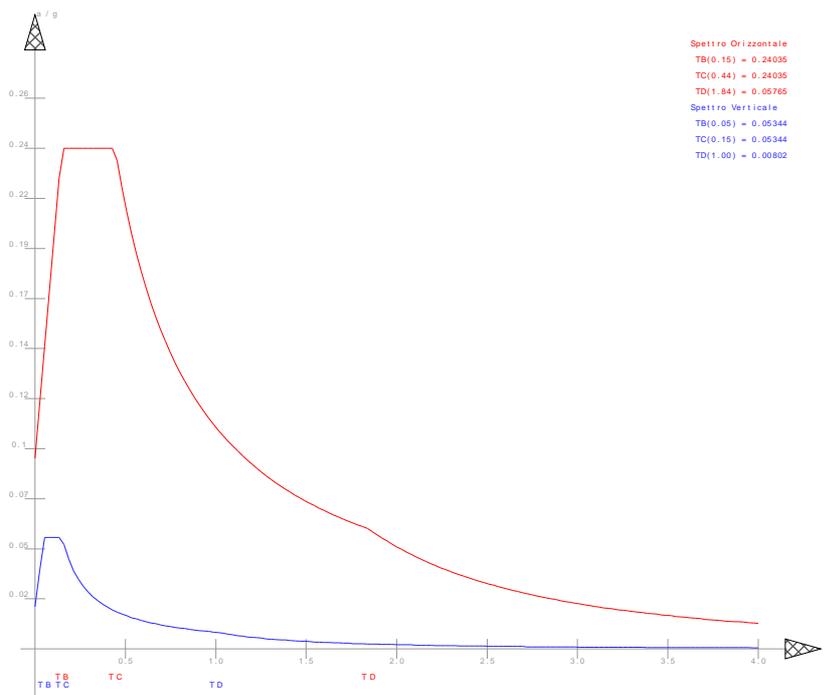


Figura numero 2: Spettro allo SLD

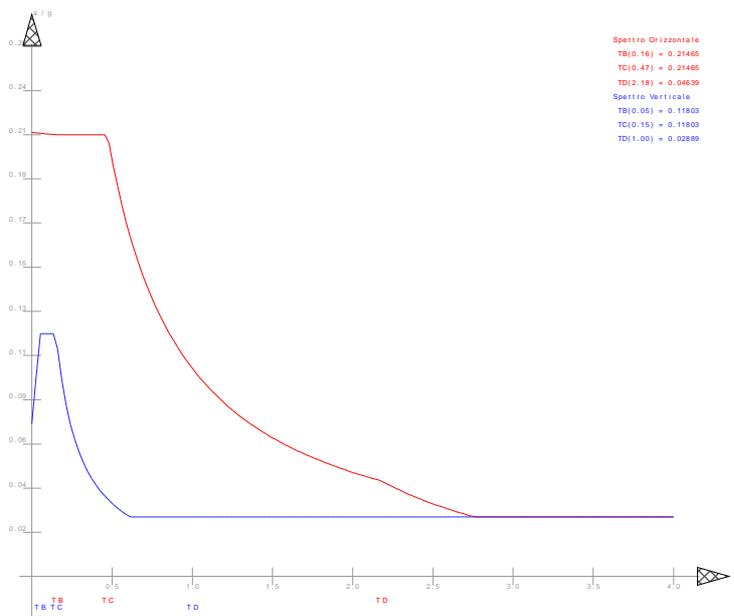


Figura numero 3: Spettro allo SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Dati di piano

Simbologia

- Imp. = Numero dell'impalcato
- Lx = Dimensione del piano in dir. X
- Ly = Dimensione del piano in dir. Y
- Ex = Eccentricità in dir. X
- Ey = Eccentricità in dir. Y
- Ea = Eccentricità complessiva

Imp.	Lx	Ly	Ex	Ey	Ea
<m>	<m>	<m>	<m>	<m>	<m>
1	36.00	15.90	1.80	0.80	1.97
2	6.00	3.35	0.30	0.17	0.34
3	36.00	21.44	1.80	1.07	2.10
4	36.00	21.44	1.80	1.07	2.10
5	36.00	21.44	1.80	1.07	2.10
6	36.00	21.44	1.80	1.07	2.10
7	36.00	21.44	1.80	1.07	2.10
8	36.00	21.44	1.80	1.07	2.10
9	36.00	21.44	1.80	1.07	2.10

Condizioni di carico elementari

Simbologia

- CCE = Numero della condizione di carico elementare
- Comm. = Commento
- s = Coeff. di riduzione
- Mx = Moltiplicatore della massa in dir. X
- My = Moltiplicatore della massa in dir. Y
- Mz = Moltiplicatore della massa in dir. Z
- Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
- Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
- Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	s	Mx	My	Mz	Jpx	Jpy	Jpz
1	pp e perm	1.00	1.00	1.00	1.00	0.00	0.00	1.00
2	tamponamenti	1.00	1.00	1.00	1.00	0.00	0.00	1.00
3	permanente solette	1.00	1.00	1.00	1.00	0.00	0.00	1.00
4	parcheggio	1.00	1.00	1.00	1.00	0.00	0.00	1.00
5	negozi (2)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
6	carrabile	1.00	1.00	1.00	1.00	0.00	0.00	1.00
7	mezzanino (4)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
8	uffici (3)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
9	copertura (5 6 9)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
10	scale (1 7 8)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
11	permanenti non strutturali solai	1.00	1.00	1.00	1.00	0.00	0.00	1.00

279	322.48	322.48	280	165.12	165.12	301	0.00	380.51	302	0.00	383.76	303	0.00	2148.48
304	0.00	3083.38	305	0.00	2877.68	306	0.00	1880.16	307	0.00	2519.81	308	0.00	3083.38
309	0.00	2148.48	310	0.00	2006.39	311	0.00	544.04	312	0.00	568.77	313	0.00	2512.58
314	0.00	741.88	315	0.00	2512.58	316	0.00	741.88	317	0.00	2172.00	318	0.00	2159.64
319	0.00	741.88	320	0.00	2524.95	321	0.00	568.77	322	0.00	544.04	323	0.00	2006.39
324	0.00	2006.39	325	0.00	544.04	326	0.00	568.77	327	0.00	2512.58	328	0.00	741.88
329	0.00	2512.58	330	0.00	741.88	331	0.00	2172.00	332	0.00	2159.64	333	0.00	741.88
334	0.00	2524.95	335	0.00	568.77	336	0.00	544.04	337	0.00	2006.39	338	0.00	2148.48
339	0.00	3083.38	340	0.00	3083.38	341	0.00	2519.81	342	0.00	2519.81	343	0.00	3083.38
344	0.00	2148.48	345	0.00	42.38	346	0.00	160.52	347	0.00	160.52	348	0.00	42.38
349	0.00	83.22	350	0.00	86.42	351	0.00	42.38	352	0.00	156.45	353	0.00	281.72
354	0.00	170.33	355	0.00	848.08	356	0.00	691.76	357	0.00	691.76	358	0.00	442.08
359	0.00	442.08	360	0.00	442.08	361	0.00	442.08	362	0.00	563.57	363	0.00	563.57
401	0.00	206.63	402	0.00	208.28	403	0.00	1964.60	404	0.00	2893.11	405	0.00	2687.41
406	0.00	1689.89	407	0.00	2329.54	408	0.00	2893.11	409	0.00	1958.21	410	0.00	2345.41
413	0.00	3108.34	415	0.00	3108.34	417	0.00	2615.80	418	0.00	2615.80	420	0.00	3108.34
423	0.00	2339.02	424	0.00	2339.02	427	0.00	3108.34	429	0.00	3108.34	431	0.00	2615.80
432	0.00	2615.80	434	0.00	3108.34	437	0.00	2339.02	438	0.00	1958.21	439	0.00	2893.11
440	0.00	2893.11	441	0.00	2329.54	442	0.00	2329.54	443	0.00	2893.11	444	0.00	1958.21
445	0.00	22.70	446	0.00	83.99	447	0.00	83.99	448	0.00	22.70	449	0.00	43.86
450	0.00	45.46	451	0.00	22.70	452	0.00	83.13	453	0.00	146.29	454	0.00	88.54
455	0.00	848.08	456	0.00	629.34	457	0.00	629.35	458	0.00	442.08	459	0.00	442.08
460	0.00	442.08	461	0.00	442.08	462	0.00	563.57	463	0.00	563.57	501	0.00	206.93
502	0.00	208.58	503	0.00	1959.99	504	0.00	2894.90	505	0.00	2689.19	506	0.00	1691.67
507	0.00	2331.33	508	0.00	2894.90	509	0.00	1959.99	510	0.00	2340.80	513	0.00	3090.50
515	0.00	3090.50	517	0.00	2597.96	518	0.00	2597.96	520	0.00	3090.50	523	0.00	2340.80
524	0.00	2340.80	527	0.00	3090.50	529	0.00	3090.50	531	0.00	2597.96	532	0.00	2597.96
534	0.00	3090.50	537	0.00	2340.80	538	0.00	1959.99	539	0.00	2894.90	540	0.00	2894.90
541	0.00	2331.33	542	0.00	2331.33	543	0.00	2894.90	544	0.00	1959.99	545	0.00	22.70
546	0.00	83.99	547	0.00	83.99	548	0.00	22.70	549	0.00	43.86	550	0.00	45.46
551	0.00	22.70	552	0.00	83.13	553	0.00	146.29	554	0.00	88.54	555	0.00	848.08
556	0.00	629.34	557	0.00	629.35	558	0.00	442.08	559	0.00	442.08	560	0.00	442.08
561	0.00	442.08	562	0.00	563.57	563	0.00	563.57	601	0.00	206.93	602	0.00	208.58
603	0.00	1959.99	604	0.00	2894.90	605	0.00	2689.19	606	0.00	1691.67	607	0.00	2331.33
608	0.00	2894.90	609	0.00	1959.99	610	0.00	2340.80	613	0.00	3090.50	615	0.00	3090.50
617	0.00	2597.96	618	0.00	2597.96	620	0.00	3090.50	623	0.00	2340.80	624	0.00	2340.80
627	0.00	3090.50	629	0.00	3090.50	631	0.00	2597.96	632	0.00	2597.96	634	0.00	3090.50
637	0.00	2340.80	638	0.00	1959.99	639	0.00	2894.90	640	0.00	2894.90	641	0.00	2331.33
642	0.00	2331.33	643	0.00	2894.90	644	0.00	1959.99	645	0.00	22.70	646	0.00	83.99
647	0.00	83.99	648	0.00	22.70	649	0.00	43.86	650	0.00	45.46	651	0.00	22.70
652	0.00	83.13	653	0.00	146.29	654	0.00	88.54	655	0.00	848.08	656	0.00	629.34
657	0.00	629.35	658	0.00	442.08	659	0.00	442.08	660	0.00	442.08	661	0.00	442.08
662	0.00	563.57	663	0.00	563.57	701	0.00	206.93	702	0.00	208.58	703	0.00	1959.99
704	0.00	2894.90	705	0.00	2689.19	706	0.00	1691.67	707	0.00	2331.33	708	0.00	2894.90
709	0.00	1959.99	710	0.00	2340.80	713	0.00	3090.50	715	0.00	3090.50	717	0.00	2597.96
718	0.00	2597.96	720	0.00	3090.50	723	0.00	2340.80	724	0.00	2340.80	727	0.00	3090.50
729	0.00	3090.50	731	0.00	2597.96	732	0.00	2597.96	734	0.00	3090.50	737	0.00	2340.80
738	0.00	1959.99	739	0.00	2894.90	740	0.00	2894.90	741	0.00	2331.33	742	0.00	2331.33
743	0.00	2894.90	744	0.00	1959.99	745	0.00	22.70	746	0.00	83.99	747	0.00	83.99
748	0.00	22.70	749	0.00	43.86	750	0.00	45.46	751	0.00	22.70	752	0.00	83.13
753	0.00	146.29	754	0.00	88.54	755	0.00	848.08	756	0.00	629.34	757	0.00	629.35
758	0.00	442.08	759	0.00	442.08	760	0.00	442.08	761	0.00	442.08	762	0.00	563.57
763	0.00	563.57	801	0.00	206.93	802	0.00	208.58	803	0.00	1959.99	804	0.00	2894.90
805	0.00	2689.19	806	0.00	1691.67	807	0.00	2331.33	808	0.00	2894.90	809	0.00	1959.99
810	0.00	2340.80	813	0.00	3090.50	815	0.00	3090.50	817	0.00	2597.96	818	0.00	2597.96
820	0.00	3090.50	823	0.00	2340.80	824	0.00	2340.80	827	0.00	3090.50	829	0.00	3090.50
831	0.00	2597.96	832	0.00	2597.96	834	0.00	3090.50	837	0.00	2340.80	838	0.00	1959.99
839	0.00	2894.90	840	0.00	2894.90	841	0.00	2331.33	842	0.00	2331.33	843	0.00	2894.90
844	0.00	1959.99	845	0.00	22.70	846	0.00	83.99	847	0.00	83.99	848	0.00	22.70
849	0.00	43.86	850	0.00	45.46	851	0.00	22.70	852	0.00	83.13	853	0.00	146.29
854	0.00	88.54	855	0.00	848.08	856	0.00	629.34	857	0.00	629.35	858	0.00	442.08
859	0.00	442.08	860	0.00	442.08	861	0.00	442.08	862	0.00	563.57	863	0.00	563.57
901	0.00	183.66	902	0.00	185.31	903	0.00	1271.46	904	0.00	2571.69	905	0.00	2769.26
906	0.00	1866.18	907	0.00	2445.27	908	0.00	2955.49	909	0.00	1655.26	910	0.00	1674.03
913	0.00	3466.46	915	0.00	4055.14	917	0.00	3383.24	918	0.00	3383.23	920	0.00	4055.14
923	0.00	2262.71	924	0.00	1674.03	927	0.00	3466.46	929	0.00	4055.14	931	0.00	3383.24
932	0.00	3383.23	934	0.00	4055.14	937	0.00	2262.71	938	0.00	1271.46	939	0.00	2571.69
940	0.00	2955.49	941	0.00	2445.27	942	0.00	2445.27	943	0.00	2955.49	944	0.00	1655.26
945	0.00	22.70	946	0.00	83.99	947	0.00	83.99	948	0.00	22.70	949	0.00	43.86
950	0.00	45.46	951	0.00	22.70	952	0.00	83.13	953	0.00	146.29	954	0.00	88.54
955	0.00	768.04	956	0.00	575.98	957	0.00	575.99	958	0.00	621.45	959	0.00	621.45
960	0.00	621.45	961	0.00	621.45	962	0.00	510.21	963	0.00	510.21			

Totali masse nodi

Mo Mz
 <KG> <KG>
 20831.10 690257.00

Elenco forze sismiche di impalcato allo SLO

Simbologia

Imp. = Numero dell'impalcato
 cx = Coeff. c in dir. X
 cy = Coeff. c in dir. Y
 Mz = Momento intorno all'asse Z

Imp.	cx	cy	Mz
<kgm>			
1	0.03	0.03	47970.00
2	0.00	0.00	7142.88
3	0.07	0.07	126294.00
4	0.09	0.09	158039.00
5	0.11	0.11	199746.00

6 0.13 0.13 241719.00
 7 0.16 0.16 283691.00
 8 0.18 0.18 325664.00
 9 0.21 0.21 381706.00

Totali forze sismiche

Mz
 <kgm>
 1771970.00

Elenco forze sismiche di impalcato allo SLD

Imp. cx cy Mz
 <kgm>
 1 0.03 0.03 59921.40
 2 0.00 0.00 8922.48
 3 0.07 0.07 157759.00
 4 0.09 0.09 197414.00
 5 0.11 0.11 249511.00
 6 0.13 0.13 301941.00
 7 0.16 0.16 354371.00
 8 0.18 0.18 406801.00
 9 0.21 0.21 476806.00

Totali forze sismiche

Mz
 <kgm>
 2213450.00

Elenco forze sismiche di impalcato allo SLV

Imp. cx cy Mz
 <kgm>
 1 0.03 0.03 56944.30
 2 0.00 0.00 8479.18
 3 0.07 0.07 149921.00
 4 0.09 0.09 187606.00
 5 0.11 0.11 237115.00
 6 0.13 0.13 286940.00
 7 0.16 0.16 336765.00
 8 0.18 0.18 386590.00
 9 0.21 0.21 453117.00

Totali forze sismiche

Mz
 <kgm>
 2103480.00

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione**Simbologia**

Modo = Numero del modo di vibrare
 C = * indica che il modo è stato considerato
 Per. = Periodo
 Diff. = Minima differenza percentuale dagli altri periodi
 Φ_x = Coefficiente di partecipazione in dir. X
 Φ_y = Coefficiente di partecipazione in dir. Y
 Φ_z = Coefficiente di partecipazione in dir. Z
 %Mx = Percentuale massa partecipante in dir. X
 %My = Percentuale massa partecipante in dir. Y
 %Mz = Percentuale massa partecipante in dir. Z
 %Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φ_x	Φ_y	Φ_z	%Mx	%My	%Mz	%Jpz
1	*	1.45	22.43	-0.95	-683.78	-0.21	0.00	64.62	0.00	0.15
2	*	1.18	2.19	684.65	-8.91	0.49	64.78	0.01	0.00	3.26
3	*	1.16	2.19	-153.76	-35.56	-0.03	3.27	0.17	0.00	64.02
4		1.08	0.53	2.39	-39.07	-0.01	0.00	0.21	0.00	0.35
5		1.07	0.53	-2.08	-40.15	0.00	0.00	0.22	0.00	0.30
6		0.55	10.29	0.11	45.55	0.04	0.00	0.29	0.00	0.00
7		0.49	10.29	-0.10	75.49	0.12	0.00	0.79	0.00	0.00
8		0.44	0.09	-0.17	-19.06	1.79	0.00	0.05	0.00	0.00
9	*	0.44	0.09	-0.41	-282.86	-1.56	0.00	11.06	0.00	0.09
10		0.43	3.05	13.53	0.74	0.41	0.03	0.00	0.00	0.00
11		0.41	2.87	-1.25	-0.06	53.83	0.00	0.00	0.42	0.00
12		0.40	2.74	-1.32	0.08	-40.73	0.00	0.00	0.24	0.00
13		0.39	2.74	-0.14	-0.04	2.08	0.00	0.00	0.00	0.00
14	*	0.36	1.06	22.24	-16.70	-0.19	0.07	0.04	0.00	10.77
15		0.36	1.06	4.06	0.34	15.81	0.00	0.00	0.04	0.01
16		0.34	3.23	0.88	0.06	-19.39	0.00	0.00	0.05	0.00
17	*	0.33	2.60	308.18	0.76	-3.93	13.13	0.00	0.00	0.04
18		0.32	1.48	-1.19	-0.63	0.01	0.00	0.00	0.00	0.01
19		0.32	0.60	-0.37	0.82	-0.06	0.00	0.00	0.00	0.01
20		0.31	0.60	0.57	-0.92	-0.02	0.00	0.00	0.00	0.02
21	*	0.31	0.92	-128.37	-0.04	3.08	2.28	0.00	0.00	0.01
22		0.31	1.57	-2.17	-8.77	-10.08	0.00	0.01	0.01	0.00
23		0.29	4.14	0.74	3.67	-0.08	0.00	0.00	0.00	0.01
24		0.28	2.20	0.43	-4.69	-0.01	0.00	0.00	0.00	0.01
25		0.28	1.92	0.01	20.49	0.64	0.00	0.06	0.00	0.00
26		0.27	1.65	-13.76	0.52	0.55	0.03	0.00	0.00	0.00

27	0.27	1.65	0.13	8.93	-0.03	0.00	0.01	0.00	0.00
28	0.26	0.18	-0.96	0.13	14.69	0.00	0.00	0.03	0.00
29	0.26	0.18	1.80	0.07	13.35	0.00	0.00	0.03	0.00
30	0.25	1.54	-0.44	36.13	-9.86	0.00	0.18	0.01	0.00
31	* 0.24	1.54	-0.09	-193.12	-1.48	0.00	5.15	0.00	0.00
32	0.22	0.03	-0.16	0.05	0.07	0.00	0.00	0.00	0.01
33	0.22	0.03	-0.10	1.84	-0.09	0.00	0.00	0.00	0.00
34	* 0.21	0.34	-3.28	9.32	5.53	0.00	0.01	0.00	2.68
35	0.21	0.34	-1.02	-0.44	-10.35	0.00	0.00	0.02	0.69
36	0.20	0.92	0.14	-2.64	-9.76	0.00	0.00	0.01	0.00
37	0.20	0.44	-0.79	1.31	20.54	0.00	0.00	0.06	0.00
38	0.20	0.44	0.07	1.72	11.88	0.00	0.00	0.02	0.00
39	0.20	0.22	0.19	-16.63	4.08	0.00	0.04	0.00	0.03
40	0.20	0.22	1.66	-12.92	0.93	0.00	0.02	0.00	0.16
41	0.20	0.34	0.60	3.46	4.49	0.00	0.00	0.00	0.10
42	0.18	8.40	-1.11	-35.22	-0.03	0.00	0.17	0.00	0.09
43	0.16	0.94	-0.07	1.52	-1.21	0.00	0.00	0.00	0.00
44	* 0.16	0.94	-1.50	-126.66	-0.90	0.00	2.22	0.00	0.01
45	0.15	0.89	-0.39	0.15	-0.26	0.00	0.00	0.00	0.00
46	* 0.15	0.89	-158.09	1.23	8.91	3.45	0.00	0.01	0.00
47	0.15	5.07	-0.02	0.29	0.03	0.00	0.00	0.00	0.00
48	0.14	0.41	4.69	-0.19	3.99	0.00	0.00	0.00	0.00
49	* 0.14	0.41	1.20	3.65	3.12	0.00	0.00	0.00	1.41
50	0.13	1.41	-8.07	0.03	-11.44	0.01	0.00	0.02	0.00
51	0.13	0.15	-0.86	2.79	-11.98	0.00	0.00	0.02	0.00
52	0.13	0.15	0.02	-0.01	0.87	0.00	0.00	0.00	0.00
53	* 0.12	0.57	-4.94	-1.84	-361.82	0.00	0.00	18.97	0.01
54	0.12	0.35	-0.72	-1.35	-23.18	0.00	0.00	0.08	0.00
55	* 0.12	0.01	1.41	4.60	-87.22	0.00	0.00	1.10	0.00
56	* 0.12	0.01	-3.07	0.75	192.53	0.00	0.00	5.37	0.00
57	0.12	0.23	0.05	0.86	0.14	0.00	0.00	0.00	0.00
58	* 0.12	1.03	-6.81	1.86	-229.26	0.01	0.00	7.61	0.00
59	0.12	0.42	-0.33	1.27	-54.76	0.00	0.00	0.43	0.00
60	0.12	0.17	0.27	-0.18	-1.87	0.00	0.00	0.00	0.00
61	0.12	0.17	-0.35	0.59	-45.30	0.00	0.00	0.30	0.00
62	* 0.12	0.17	2.05	-0.55	-161.88	0.00	0.00	3.80	0.00
63	* 0.12	0.17	-0.28	0.74	166.41	0.00	0.00	4.01	0.00
64	0.12	0.27	1.64	0.45	-45.33	0.00	0.00	0.30	0.00
65	0.12	0.43	0.14	-9.60	-2.19	0.00	0.01	0.00	0.00
66	0.11	0.24	1.50	-0.17	-65.19	0.00	0.00	0.62	0.00
67	0.11	0.20	-0.48	2.47	-2.30	0.00	0.00	0.00	0.00
68	0.11	0.20	-4.34	-0.25	-43.59	0.00	0.00	0.28	0.00
69	0.11	0.17	-0.63	-0.40	35.00	0.00	0.00	0.18	0.00
70	0.11	0.17	1.49	0.13	-45.71	0.00	0.00	0.30	0.00
71	0.11	0.21	-0.31	-2.85	3.07	0.00	0.00	0.00	0.00
72	0.11	0.17	1.06	0.47	6.44	0.00	0.00	0.01	0.00
73	0.11	0.17	-33.09	0.77	-58.77	0.15	0.00	0.50	0.00
74	* 0.11	0.19	-41.49	-3.35	143.34	0.24	0.00	2.98	0.00
75	0.11	0.06	-0.13	0.04	4.32	0.00	0.00	0.00	0.00
76	* 0.11	0.06	7.16	-0.84	166.49	0.01	0.00	4.02	0.00
77	0.11	0.55	-0.40	3.03	36.82	0.00	0.00	0.20	0.00
78	0.11	0.73	-1.29	80.91	-5.12	0.00	0.90	0.00	0.00
79	* 0.11	0.48	-15.39	-0.89	-155.51	0.03	0.00	3.50	0.00
80	* 0.11	0.48	-9.32	-0.37	-88.12	0.01	0.00	1.13	0.00
81	* 0.10	0.83	4.85	0.19	-152.45	0.00	0.00	3.37	0.00
82	0.10	0.56	1.45	0.89	26.82	0.00	0.00	0.10	0.00
83	0.10	0.56	-0.47	1.99	43.01	0.00	0.00	0.27	0.00
84	* 0.10	0.68	8.54	-0.99	154.03	0.01	0.00	3.44	0.00
85	0.10	0.13	26.44	-0.03	-59.46	0.10	0.00	0.51	0.00
86	0.10	0.13	1.41	0.06	-2.98	0.00	0.00	0.00	0.00
87	0.10	0.57	0.09	0.90	-0.59	0.00	0.00	0.00	0.00
88	0.10	0.30	-1.38	-6.37	-2.25	0.00	0.01	0.00	0.03
89	0.10	0.07	-28.06	0.92	-63.81	0.11	0.00	0.59	0.00
90	0.10	0.07	-1.81	-4.26	-7.38	0.00	0.00	0.01	0.01
91	0.10	0.53	0.36	-5.61	-12.18	0.00	0.00	0.02	0.27
92	0.10	1.31	1.60	0.57	76.23	0.00	0.00	0.84	0.01
93	0.09	0.34	5.64	-1.05	-78.87	0.00	0.00	0.90	0.00
94	0.09	0.07	-2.07	3.76	-0.36	0.00	0.00	0.00	0.00
95	0.09	0.07	3.35	0.34	5.27	0.00	0.00	0.00	0.00
96	0.09	0.72	-10.37	-0.30	22.84	0.01	0.00	0.08	0.00
97	0.09	0.72	74.14	0.07	1.55	0.76	0.00	0.00	0.00
98	0.09	0.29	0.81	3.03	-3.74	0.00	0.00	0.00	0.00
99	0.09	0.07	-14.62	1.78	17.45	0.03	0.00	0.04	0.00
100	0.09	0.07	27.83	4.21	-17.07	0.11	0.00	0.04	0.00
101	0.09	0.24	-15.85	-1.40	16.88	0.03	0.00	0.04	0.00
102	0.09	0.24	-29.60	1.68	-28.35	0.12	0.00	0.12	0.00
103	0.09	0.18	-18.07	2.09	-4.50	0.05	0.00	0.00	0.00
104	0.09	0.18	-0.47	0.09	-5.14	0.00	0.00	0.00	0.00
105	0.09	0.37	-2.74	-3.44	0.68	0.00	0.00	0.00	0.00
106	0.09	0.19	-0.58	-41.60	18.62	0.00	0.24	0.05	0.07
107	0.09	0.19	2.75	-39.40	-21.85	0.00	0.21	0.07	0.13
108	0.09	0.43	-0.87	5.42	-0.60	0.00	0.00	0.00	0.00
109	0.09	0.20	1.13	-4.93	2.43	0.00	0.00	0.00	0.00
110	0.09	0.10	-0.17	-6.35	0.06	0.00	0.01	0.00	0.00
111	0.09	0.10	1.70	5.23	-1.52	0.00	0.00	0.00	0.00
112	0.09	0.13	-0.61	4.24	2.53	0.00	0.00	0.00	0.00
113	0.09	0.13	-2.18	-1.71	0.90	0.00	0.00	0.00	0.00
114	0.08	0.69	-1.02	-43.84	-2.83	0.00	0.27	0.00	0.34
115	0.08	0.69	-1.22	-3.71	6.33	0.00	0.00	0.01	0.00
116	0.08	0.13	-0.08	-0.93	1.02	0.00	0.00	0.00	0.00
117	0.08	0.13	-0.71	0.16	-9.12	0.00	0.00	0.01	0.00
118	0.08	1.18	-0.37	-2.95	1.22	0.00	0.00	0.00	0.00
119	0.08	1.18	0.84	0.61	-6.71	0.00	0.00	0.01	0.00
120	0.08	0.32	0.79	1.38	4.35	0.00	0.00	0.00	0.00
121	0.08	0.32	3.61	-0.81	2.58	0.00	0.00	0.00	0.00
122	0.08	0.54	0.04	-2.94	1.98	0.00	0.00	0.00	0.00
123	0.08	1.13	0.04	-72.14	13.04	0.00	0.72	0.02	0.00
124	0.08	1.13	0.26	25.35	20.07	0.00	0.09	0.06	0.01

125	0.08	0.22	0.47	-6.89	-17.93	0.00	0.01	0.05	0.02
126	0.08	0.22	-0.03	1.05	-14.11	0.00	0.00	0.03	0.00
127	0.07	1.54	0.18	1.48	-5.79	0.00	0.00	0.00	0.02
128	0.07	1.06	1.28	2.14	-3.02	0.00	0.00	0.00	0.19
129	0.07	1.06	-0.33	-8.28	4.74	0.00	0.01	0.00	0.02
130	0.07	0.88	10.14	-0.53	-2.26	0.01	0.00	0.00	0.02
131	0.07	0.44	3.75	5.96	-1.21	0.00	0.00	0.00	0.01
132	0.07	0.17	-60.84	0.32	1.62	0.51	0.00	0.00	0.00
133	0.07	0.17	4.67	0.96	-1.98	0.00	0.00	0.00	0.00
134	0.07	0.66	2.76	0.09	0.35	0.00	0.00	0.00	0.00
135	* 0.07	0.11	-0.99	0.01	285.22	0.00	0.00	11.79	0.00
136	0.07	0.11	32.86	-0.39	5.51	0.15	0.00	0.00	0.00
137	0.07	0.62	13.88	-0.14	-12.91	0.03	0.00	0.02	0.00
138	0.07	0.12	-6.55	0.07	-17.75	0.01	0.00	0.05	0.00
139	0.07	0.12	0.82	4.66	4.30	0.00	0.00	0.00	0.00
140	0.07	0.08	-27.59	0.04	5.42	0.11	0.00	0.00	0.00
141	0.07	0.08	35.67	0.05	18.91	0.18	0.00	0.05	0.00
142	0.07	0.38	25.31	0.08	-20.79	0.09	0.00	0.06	0.00
143	0.07	0.38	3.27	-0.19	5.21	0.00	0.00	0.00	0.00
144	0.07	0.34	0.64	-2.90	-3.28	0.00	0.00	0.00	0.00
145	0.07	0.34	-57.69	1.62	-0.67	0.46	0.00	0.00	0.00
146	0.07	0.06	-1.25	-5.87	4.50	0.00	0.00	0.00	0.00
147	0.07	0.06	-0.49	-6.33	0.84	0.00	0.01	0.00	0.00
148	0.07	0.11	-0.43	5.39	-0.42	0.00	0.00	0.00	0.00
149	0.07	0.17	0.52	2.32	5.92	0.00	0.00	0.01	0.00
150	0.06	0.29	-1.02	-0.51	-0.38	0.00	0.00	0.00	0.00
151	0.06	0.12	0.06	0.75	-1.24	0.00	0.00	0.00	0.00
152	0.06	0.12	2.20	1.20	-10.29	0.00	0.00	0.02	0.00
153	0.06	0.15	-0.08	-1.25	-3.11	0.00	0.00	0.00	0.00
154	0.06	0.38	-0.82	1.90	-16.00	0.00	0.00	0.04	0.00
155	0.06	0.13	-4.44	-52.93	-1.05	0.00	0.39	0.00	0.00
156	0.06	0.13	0.71	12.71	-0.58	0.00	0.02	0.00	0.00
157	0.06	0.36	1.22	9.85	-0.20	0.00	0.01	0.00	0.00
158	0.06	1.15	-81.10	2.84	1.57	0.91	0.00	0.00	0.00
159	0.06	1.11	1.78	32.64	0.38	0.00	0.15	0.00	0.00
160	0.06	0.31	-0.03	1.02	-2.59	0.00	0.00	0.00	0.04
161	0.06	0.31	11.82	0.42	30.27	0.02	0.00	0.13	0.00
162	0.06	0.46	8.69	-0.86	27.73	0.01	0.00	0.11	0.00
163	0.06	0.36	-25.68	1.92	-2.49	0.09	0.00	0.00	0.00
164	0.06	0.36	0.85	-0.07	-14.55	0.00	0.00	0.03	0.00
165	0.06	0.68	-11.22	-6.50	0.35	0.02	0.01	0.00	0.06
166	0.06	0.41	-41.48	0.51	-4.35	0.24	0.00	0.00	0.00
167	0.06	0.16	9.74	0.32	15.14	0.01	0.00	0.03	0.00
168	0.06	0.16	8.78	-0.46	3.72	0.01	0.00	0.00	0.00
169	0.06	1.67	23.47	0.02	4.49	0.08	0.00	0.00	0.00
170	0.06	0.64	-55.60	0.05	2.99	0.43	0.00	0.00	0.00
171	0.06	0.37	-57.77	-1.14	-7.52	0.46	0.00	0.01	0.00
172	0.06	0.05	-28.49	1.69	1.97	0.11	0.00	0.00	0.00
173	0.06	0.05	-45.06	3.08	1.25	0.28	0.00	0.00	0.00
174	0.06	0.16	17.18	-0.63	2.24	0.04	0.00	0.00	0.00
175	0.06	0.23	4.69	0.08	-0.20	0.00	0.00	0.00	0.00
176	* 0.05	0.67	160.20	1.17	0.43	3.55	0.00	0.00	0.00
177	* 0.05	0.48	-124.83	-0.04	-1.47	2.15	0.00	0.00	0.00
178	0.05	0.48	55.91	-0.17	-22.83	0.43	0.00	0.08	0.00
179	0.05	0.05	-1.33	38.05	2.58	0.00	0.20	0.00	0.00
180	* 0.05	0.05	-0.30	-178.40	0.15	0.00	4.40	0.00	0.00
181	0.05	0.35	-0.79	4.61	1.96	0.00	0.00	0.00	0.00
182	0.05	0.29	1.17	-2.54	1.76	0.00	0.00	0.00	0.00
183	0.05	0.10	6.89	0.48	-16.87	0.01	0.00	0.04	0.00
184	0.05	0.10	1.62	0.76	0.65	0.00	0.00	0.00	0.00
185	0.05	0.19	0.83	0.15	-0.22	0.00	0.00	0.00	0.00
186	0.05	0.19	-0.05	0.13	-0.78	0.00	0.00	0.00	0.00
187	0.05	0.10	5.87	0.10	23.02	0.00	0.00	0.08	0.00
188	0.05	0.10	11.42	-0.01	-16.34	0.02	0.00	0.04	0.00
189	0.05	0.84	-5.66	0.02	0.08	0.00	0.00	0.00	0.00
190	0.05	0.26	-53.25	1.54	2.07	0.39	0.00	0.00	0.00
191	0.05	0.26	-27.27	0.48	1.19	0.10	0.00	0.00	0.00
192	0.05	0.33	0.72	0.09	0.14	0.00	0.00	0.00	0.00
193	0.05	0.33	-2.54	0.09	-0.39	0.00	0.00	0.00	0.00
194	0.05	0.21	0.66	-0.04	-0.35	0.00	0.00	0.00	0.00
195	0.05	0.21	-0.20	-0.01	0.00	0.00	0.00	0.00	0.00
196	* 0.05	0.34	0.18	97.58	0.37	0.00	1.32	0.00	0.00
197	0.05	0.34	-0.39	-18.41	-0.03	0.00	0.05	0.00	0.24
198	* 0.04	2.41	-0.13	-191.74	-0.18	0.00	5.08	0.00	0.02
199	0.04	2.40	9.25	-1.12	-8.58	0.01	0.00	0.01	0.03
200	0.04	0.09	2.07	0.20	-70.11	0.00	0.00	0.71	0.00
201	0.04	0.09	-15.19	-0.40	-9.56	0.03	0.00	0.01	0.00
202	0.04	0.35	-1.76	0.03	-13.19	0.00	0.00	0.03	0.00
203	0.04	0.02	-0.28	0.49	42.75	0.00	0.00	0.26	0.00
204	0.04	0.00	-0.13	-0.25	-60.21	0.00	0.00	0.53	0.00
205	0.04	0.00	0.22	-0.57	23.53	0.00	0.00	0.08	0.01
206	0.04	0.09	-4.08	2.44	-22.46	0.00	0.00	0.07	0.68
207	0.04	0.09	-0.23	0.40	6.96	0.00	0.00	0.01	0.05
208	0.04	0.11	-0.68	-2.30	17.70	0.00	0.00	0.05	0.02
209	0.04	0.04	-0.21	-0.75	-49.65	0.00	0.00	0.36	0.00
210	0.04	0.04	-0.43	-1.15	13.38	0.00	0.00	0.03	0.07

Tot.cons.

92.99 94.09 71.09 82.49

Elenco coefficienti di risposta**Simbologia**

Modo = Numero del modo di vibrare

Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X

Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Sz = Coefficiente di risposta (moltiplicato per 100) in dir. Z

Stato limite di operatività

Modo	Sx	Sy	Sz
1	5.88	5.88	0.29
2	7.20	7.20	0.44
3	7.36	7.36	0.46
4	7.90	7.90	0.53
5	7.94	7.94	0.54
6	15.59	15.59	1.13
7	17.20	17.20	1.25
8	19.37	19.37	1.40
9	19.38	19.38	1.40
10	19.98	19.98	1.45
11	20.09	20.09	1.50
12	20.09	20.09	1.54
13	20.09	20.09	1.58
14	20.09	20.09	1.70
15	20.09	20.09	1.72
16	20.09	20.09	1.82
17	20.09	20.09	1.88
18	20.09	20.09	1.93
19	20.09	20.09	1.96
20	20.09	20.09	1.97
21	20.09	20.09	1.98
22	20.09	20.09	2.02
23	20.09	20.09	2.10
24	20.09	20.09	2.19
25	20.09	20.09	2.24
26	20.09	20.09	2.28
27	20.09	20.09	2.32
28	20.09	20.09	2.37
29	20.09	20.09	2.38
30	20.09	20.09	2.48
31	20.09	20.09	2.52
32	20.09	20.09	2.86
33	20.09	20.09	2.86
34	20.09	20.09	2.98
35	20.09	20.09	2.99
36	20.09	20.09	3.06
37	20.09	20.09	3.09
38	20.09	20.09	3.11
39	20.09	20.09	3.13
40	20.09	20.09	3.14
41	20.09	20.09	3.15
42	20.09	20.09	3.41
43	20.09	20.09	3.92
44	20.09	20.09	3.95
45	20.09	20.09	3.99
46	20.09	20.09	4.03
47	20.09	20.09	4.11
48	19.72	19.72	4.11
49	19.67	19.67	4.11
50	19.06	19.06	4.11
51	18.90	18.90	4.11
52	18.88	18.88	4.11
53	18.48	18.48	4.11
54	18.42	18.42	4.11
55	18.39	18.39	4.11
56	18.39	18.39	4.11
57	18.36	18.36	4.11
58	18.25	18.25	4.11
59	18.05	18.05	4.11
60	18.01	18.01	4.11
61	17.99	17.99	4.11
62	17.91	17.91	4.11
63	17.90	17.90	4.11
64	17.87	17.87	4.11
65	17.83	17.83	4.11
66	17.69	17.69	4.11
67	17.67	17.67	4.11
68	17.65	17.65	4.11
69	17.62	17.62	4.11
70	17.60	17.60	4.11
71	17.58	17.58	4.11
72	17.54	17.54	4.11
73	17.53	17.53	4.11
74	17.24	17.24	4.11
75	17.22	17.22	4.11
76	17.21	17.21	4.11
77	17.16	17.16	4.11
78	17.09	17.09	4.11
79	16.98	16.98	4.11
80	16.94	16.94	4.11
81	16.84	16.84	4.11
82	16.77	16.77	4.11
83	16.72	16.72	4.11
84	16.59	16.59	4.11
85	16.53	16.53	4.11
86	16.52	16.52	4.11
87	16.36	16.36	4.11
88	16.31	16.31	4.11
89	16.29	16.29	4.11
90	16.28	16.28	4.11
91	16.24	16.24	4.11
92	16.13	16.13	4.11
93	15.93	15.93	4.11

94	15.91	15.91	4.11
95	15.90	15.90	4.11
96	15.84	15.84	4.11
97	15.75	15.75	4.11
98	15.69	15.69	4.11
99	15.67	15.67	4.11
100	15.67	15.67	4.11
101	15.57	15.57	4.11
102	15.55	15.55	4.11
103	15.50	15.50	4.11
104	15.48	15.48	4.11
105	15.41	15.41	4.11
106	15.39	15.39	4.11
107	15.37	15.37	4.11
108	15.34	15.34	4.11
109	15.31	15.31	4.11
110	15.29	15.29	4.11
111	15.28	15.28	4.11
112	15.27	15.27	4.11
113	15.26	15.26	4.11
114	15.17	15.17	4.11
115	15.12	15.12	4.11
116	15.04	15.04	4.11
117	15.03	15.03	4.11
118	14.95	14.95	4.11
119	14.86	14.86	4.11
120	14.78	14.78	4.11
121	14.75	14.75	4.11
122	14.72	14.72	4.11
123	14.56	14.56	4.11
124	14.48	14.48	4.11
125	14.32	14.32	4.11
126	14.31	14.31	4.11
127	14.20	14.20	4.11
128	14.10	14.10	4.11
129	14.03	14.03	4.11
130	13.96	13.96	4.11
131	13.91	13.91	4.11
132	13.88	13.88	4.11
133	13.87	13.87	4.11
134	13.79	13.79	4.11
135	13.75	13.75	4.11
136	13.74	13.74	4.11
137	13.67	13.67	4.11
138	13.64	13.64	4.11
139	13.63	13.63	4.11
140	13.61	13.61	4.11
141	13.61	13.61	4.11
142	13.58	13.58	4.11
143	13.56	13.56	4.11
144	13.51	13.51	4.11
145	13.49	13.49	4.11
146	13.47	13.47	4.11
147	13.46	13.46	4.11
148	13.46	13.46	4.11
149	13.45	13.45	4.11
150	13.43	13.43	4.11
151	13.40	13.40	4.11
152	13.39	13.39	4.11
153	13.38	13.38	4.11
154	13.35	13.35	4.11
155	13.33	13.33	4.11
156	13.32	13.32	4.11
157	13.30	13.30	4.11
158	13.24	13.24	4.11
159	13.13	13.13	4.11
160	13.07	13.07	4.11
161	13.06	13.06	4.11
162	12.97	12.97	4.11
163	12.95	12.95	4.11
164	12.93	12.93	4.11
165	12.89	12.89	4.11
166	12.85	12.85	4.11
167	12.82	12.82	4.11
168	12.82	12.82	4.11
169	12.73	12.73	4.11
170	12.64	12.64	4.11
171	12.61	12.61	4.11
172	12.59	12.59	4.11
173	12.59	12.59	4.11
174	12.58	12.58	4.11
175	12.57	12.57	4.11
176	12.54	12.54	4.11
177	12.49	12.49	4.11
178	12.47	12.47	4.11
179	12.27	12.27	4.11
180	12.27	12.27	4.11
181	12.22	12.22	4.11
182	12.20	12.20	4.11
183	12.19	12.19	4.11
184	12.19	12.19	4.11
185	12.16	12.16	4.11
186	12.16	12.16	4.11
187	12.04	12.04	4.06
188	12.04	12.04	4.06
189	11.92	11.92	3.99
190	11.88	11.88	3.97

191	11.87	11.87	3.97
192	11.85	11.85	3.95
193	11.84	11.84	3.95
194	11.82	11.82	3.94
195	11.82	11.82	3.93
196	11.71	11.71	3.87
197	11.70	11.70	3.86
198	11.60	11.60	3.81
199	11.42	11.42	3.71
200	11.34	11.34	3.66
201	11.33	11.33	3.66
202	11.32	11.32	3.65
203	11.29	11.29	3.63
204	11.29	11.29	3.63
205	11.29	11.29	3.63
206	11.25	11.25	3.61
207	11.24	11.24	3.60
208	11.24	11.24	3.60
209	11.23	11.23	3.60
210	11.23	11.23	3.60

Stato limite di danno

Modo	Sx	Sy	Sz
1	7.35	7.35	0.38
2	9.00	9.00	0.57
3	9.19	9.19	0.60
4	9.87	9.87	0.69
5	9.92	9.92	0.70
6	19.48	19.48	1.47
7	21.48	21.48	1.62
8	24.04	24.04	1.82
9	24.04	24.04	1.83
10	24.04	24.04	1.88
11	24.04	24.04	1.95
12	24.04	24.04	2.00
13	24.04	24.04	2.06
14	24.04	24.04	2.22
15	24.04	24.04	2.24
16	24.04	24.04	2.37
17	24.04	24.04	2.44
18	24.04	24.04	2.51
19	24.04	24.04	2.54
20	24.04	24.04	2.56
21	24.04	24.04	2.58
22	24.04	24.04	2.62
23	24.04	24.04	2.74
24	24.04	24.04	2.85
25	24.04	24.04	2.91
26	24.04	24.04	2.97
27	24.04	24.04	3.02
28	24.04	24.04	3.09
29	24.04	24.04	3.09
30	24.04	24.04	3.23
31	24.04	24.04	3.28
32	24.04	24.04	3.72
33	24.04	24.04	3.72
34	24.04	24.04	3.87
35	24.04	24.04	3.89
36	24.04	24.04	3.98
37	24.04	24.04	4.02
38	24.04	24.04	4.04
39	24.04	24.04	4.07
40	24.04	24.04	4.08
41	24.04	24.04	4.09
42	24.04	24.04	4.44
43	24.04	24.04	5.10
44	24.04	24.04	5.14
45	24.04	24.04	5.19
46	24.04	24.04	5.24
47	23.85	23.85	5.34
48	22.97	22.97	5.34
49	22.92	22.92	5.34
50	22.20	22.20	5.34
51	22.02	22.02	5.34
52	22.00	22.00	5.34
53	21.55	21.55	5.34
54	21.48	21.48	5.34
55	21.43	21.43	5.34
56	21.43	21.43	5.34
57	21.40	21.40	5.34
58	21.28	21.28	5.34
59	21.05	21.05	5.34
60	21.00	21.00	5.34
61	20.98	20.98	5.34
62	20.89	20.89	5.34
63	20.87	20.87	5.34
64	20.84	20.84	5.34
65	20.79	20.79	5.34
66	20.63	20.63	5.34
67	20.60	20.60	5.34
68	20.58	20.58	5.34
69	20.55	20.55	5.34
70	20.53	20.53	5.34
71	20.50	20.50	5.34
72	20.46	20.46	5.34
73	20.44	20.44	5.34

74	20.11	20.11	5.34	172	14.74	14.74	5.34	54	21.49	21.49	11.80
75	20.09	20.09	5.34	173	14.74	14.74	5.34	55	21.49	21.49	11.80
76	20.08	20.08	5.34	174	14.73	14.73	5.34	56	21.49	21.49	11.80
77	20.02	20.02	5.34	175	14.72	14.72	5.34	57	21.49	21.49	11.80
78	19.94	19.94	5.34	176	14.68	14.68	5.34	58	21.49	21.49	11.80
79	19.81	19.81	5.34	177	14.63	14.63	5.34	59	21.49	21.49	11.80
80	19.76	19.76	5.34	178	14.60	14.60	5.34	60	21.49	21.49	11.80
81	19.65	19.65	5.34	179	14.38	14.38	5.34	61	21.49	21.49	11.80
82	19.56	19.56	5.34	180	14.38	14.38	5.34	62	21.49	21.49	11.80
83	19.51	19.51	5.34	181	14.32	14.32	5.34	63	21.49	21.49	11.80
84	19.36	19.36	5.34	182	14.30	14.30	5.34	64	21.49	21.49	11.80
85	19.29	19.29	5.34	183	14.28	14.28	5.34	65	21.49	21.49	11.80
86	19.28	19.28	5.34	184	14.28	14.28	5.34	66	21.49	21.49	11.80
87	19.10	19.10	5.34	185	14.25	14.25	5.34	67	21.49	21.49	11.80
88	19.04	19.04	5.34	186	14.24	14.24	5.34	68	21.49	21.49	11.80
89	19.01	19.01	5.34	187	14.11	14.11	5.28	69	21.49	21.49	11.80
90	19.00	19.00	5.34	188	14.11	14.11	5.28	70	21.49	21.49	11.80
91	18.95	18.95	5.34	189	13.97	13.97	5.19	71	21.49	21.49	11.80
92	18.82	18.82	5.34	190	13.93	13.93	5.17	72	21.49	21.49	11.80
93	18.60	18.60	5.34	191	13.92	13.92	5.16	73	21.49	21.49	11.80
94	18.57	18.57	5.34	192	13.89	13.89	5.14	74	21.50	21.50	11.80
95	18.56	18.56	5.34	193	13.88	13.88	5.13	75	21.50	21.50	11.80
96	18.50	18.50	5.34	194	13.86	13.86	5.12	76	21.50	21.50	11.80
97	18.39	18.39	5.34	195	13.85	13.85	5.11	77	21.50	21.50	11.80
98	18.33	18.33	5.34	196	13.73	13.73	5.03	78	21.50	21.50	11.80
99	18.30	18.30	5.34	197	13.71	13.71	5.02	79	21.50	21.50	11.80
100	18.29	18.29	5.34	198	13.61	13.61	4.95	80	21.50	21.50	11.80
101	18.18	18.18	5.34	199	13.40	13.40	4.82	81	21.50	21.50	11.80
102	18.16	18.16	5.34	200	13.30	13.30	4.75	82	21.50	21.50	11.80
103	18.10	18.10	5.34	201	13.29	13.29	4.75	83	21.50	21.50	11.80
104	18.08	18.08	5.34	202	13.28	13.28	4.74	84	21.50	21.50	11.80
105	18.00	18.00	5.34	203	13.24	13.24	4.71	85	21.50	21.50	11.80
106	17.97	17.97	5.34	204	13.24	13.24	4.71	86	21.50	21.50	11.80
107	17.95	17.95	5.34	205	13.24	13.24	4.71	87	21.50	21.50	11.80
108	17.92	17.92	5.34	206	13.20	13.20	4.68	88	21.50	21.50	11.80
109	17.88	17.88	5.34	207	13.19	13.19	4.68	89	21.50	21.50	11.80
110	17.86	17.86	5.34	208	13.18	13.18	4.68	90	21.50	21.50	11.80
111	17.85	17.85	5.34	209	13.18	13.18	4.67	91	21.50	21.50	11.80
112	17.84	17.84	5.34	210	13.18	13.18	4.67	92	21.50	21.50	11.80
113	17.83	17.83	5.34					93	21.51	21.51	11.80
114	17.72	17.72	5.34					94	21.51	21.51	11.80
115	17.67	17.67	5.34					95	21.51	21.51	11.80
116	17.57	17.57	5.34					96	21.51	21.51	11.80
117	17.56	17.56	5.34					97	21.51	21.51	11.80
118	17.46	17.46	5.34					98	21.51	21.51	11.80
119	17.37	17.37	5.34					99	21.51	21.51	11.80
120	17.27	17.27	5.34					100	21.51	21.51	11.80
121	17.24	17.24	5.34					101	21.51	21.51	11.80
122	17.20	17.20	5.34					102	21.51	21.51	11.80
123	17.01	17.01	5.34					103	21.51	21.51	11.80
124	16.93	16.93	5.34					104	21.51	21.51	11.80
125	16.74	16.74	5.34					105	21.51	21.51	11.80
126	16.73	16.73	5.34					106	21.51	21.51	11.80
127	16.60	16.60	5.34					107	21.51	21.51	11.80
128	16.49	16.49	5.34					108	21.51	21.51	11.80
129	16.41	16.41	5.34					109	21.51	21.51	11.80
130	16.33	16.33	5.34					110	21.51	21.51	11.80
131	16.26	16.26	5.34					111	21.51	21.51	11.80
132	16.23	16.23	5.34					112	21.51	21.51	11.80
133	16.22	16.22	5.34					113	21.51	21.51	11.80
134	16.12	16.12	5.34					114	21.51	21.51	11.80
135	16.08	16.08	5.34					115	21.51	21.51	11.80
136	16.07	16.07	5.34					116	21.51	21.51	11.80
137	16.00	16.00	5.34					117	21.51	21.51	11.80
138	15.95	15.95	5.34					118	21.51	21.51	11.80
139	15.95	15.95	5.34					119	21.51	21.51	11.80
140	15.92	15.92	5.34					120	21.51	21.51	11.80
141	15.92	15.92	5.34					121	21.51	21.51	11.80
142	15.89	15.89	5.34					122	21.52	21.52	11.80
143	15.87	15.87	5.34					123	21.52	21.52	11.80
144	15.81	15.81	5.34					124	21.52	21.52	11.80
145	15.79	15.79	5.34					125	21.52	21.52	11.80
146	15.76	15.76	5.34					126	21.52	21.52	11.80
147	15.75	15.75	5.34					127	21.52	21.52	11.80
148	15.74	15.74	5.34					128	21.52	21.52	11.80
149	15.73	15.73	5.34					129	21.52	21.52	11.80
150	15.71	15.71	5.34					130	21.52	21.52	11.80
151	15.68	15.68	5.34					131	21.52	21.52	11.80
152	15.67	15.67	5.34					132	21.52	21.52	11.80
153	15.66	15.66	5.34					133	21.52	21.52	11.80
154	15.62	15.62	5.34					134	21.52	21.52	11.80
155	15.59	15.59	5.34					135	21.52	21.52	11.80
156	15.59	15.59	5.34					136	21.52	21.52	11.80
157	15.56	15.56	5.34					137	21.52	21.52	11.80
158	15.49	15.49	5.34					138	21.52	21.52	11.80
159	15.37	15.37	5.34					139	21.52	21.52	11.80
160	15.30	15.30	5.34					140	21.52	21.52	11.80
161	15.28	15.28	5.34					141	21.52	21.52	11.80
162	15.19	15.19	5.34					142	21.52	21.52	11.80
163	15.16	15.16	5.34					143	21.52	21.52	11.80
164	15.14	15.14	5.34					144	21.52	21.52	11.80
165	15.10	15.10	5.34					145	21.52	21.52	11.80
166	15.04	15.04	5.34					146	21.52	21.52	11.80
167	15.02	15.02	5.34					147	21.52	21.52	11.80
168	15.01	15.01	5.34					148	21.52	21.52	11.80
169	14.91	14.91	5.34					149	21.52	21.52	11.80
170	14.80	14.80	5.34					150	21.52	21.52	11.80
171	14.76	14.76	5.34					151	21.52	21.52	11.80

Stato limite di salvaguardia della vita

Modo	Sx	Sy	Sz
1	6.98	6.98	2.89
2	8.55	8.55	2.89
3	8.74	8.74	2.89
4	9.37	9.37	2.89
5	9.42	9.42	2.89
6	18.51	18.51	3.24
7	20.42	20.42	3.58
8	21.47	21.47	4.03
9	21.47	21.47	4.03
10	21.47	21.47	4.16
11	21.47	21.47	4.30
12	21.47	21.47	4.42
13	21.47	21.47	4.54
14	21.47	21.47	4.89
15	21.47	21.47	4.95
16	21.47	21.47	5.22
17	21.47	21.47	5.39
18	21.47	21.47	5.53
19	21.47	21.47	5.62
20	21.47	21.47	5.65
21	21.47	21.47	5.70
22	21.47	21.47	5.79
23	21.47	21.47	6.05
24	21.47	21.47	6.30
25	21.47	21.47	6.43
26	21.47	21.47	6.56
27	21.47	21.47	6.67
28	21.47	21.47	6.82
29	21.47	21.47	6.83
30	21.47	21.47	7.14
31	21.47	21.47	7.25
32	21.47	21.47	8.22
33	21.47	21.47	8.22
34	21.47	21.47	8.56
35	21.47	21.47	8.59
36	21.47	21.47	8.80
37	21.47	21.47	8.88
38	21.47	21.47	8.92
39	21.47	21.47	8.99
40	21.47	21.47	9.01
41	21.47	21.47	9.04
42	21.47	21.47	9.80
43	21.47	21.47	11.25
44	21.47	21.47	11.36
45	21.47	21.47	11.47
46	21.47	21.47	11.57
47	21.47	21.47	11.80
48	21.48	21.48	11.80
49	21.48	21.48	11.80
50	21.		

152	21.52	21.52	11.80	172	21.53	21.53	11.80	192	21.54	21.54	11.53
153	21.52	21.52	11.80	173	21.53	21.53	11.80	193	21.54	21.54	11.52
154	21.53	21.53	11.80	174	21.53	21.53	11.80	194	21.54	21.54	11.51
155	21.53	21.53	11.80	175	21.53	21.53	11.80	195	21.54	21.54	11.50
156	21.53	21.53	11.80	176	21.53	21.53	11.80	196	21.54	21.54	11.39
157	21.53	21.53	11.80	177	21.53	21.53	11.80	197	21.54	21.54	11.38
158	21.53	21.53	11.80	178	21.53	21.53	11.80	198	21.54	21.54	11.28
159	21.53	21.53	11.80	179	21.53	21.53	11.80	199	21.54	21.54	11.10
160	21.53	21.53	11.80	180	21.53	21.53	11.80	200	21.54	21.54	11.02
161	21.53	21.53	11.80	181	21.53	21.53	11.80	201	21.54	21.54	11.01
162	21.53	21.53	11.80	182	21.53	21.53	11.80	202	21.54	21.54	11.00
163	21.53	21.53	11.80	183	21.53	21.53	11.80	203	21.54	21.54	10.97
164	21.53	21.53	11.80	184	21.53	21.53	11.80	204	21.54	21.54	10.97
165	21.53	21.53	11.80	185	21.53	21.53	11.80	205	21.54	21.54	10.97
166	21.53	21.53	11.80	186	21.53	21.53	11.80	206	21.54	21.54	10.93
167	21.53	21.53	11.80	187	21.53	21.53	11.72	207	21.54	21.54	10.92
168	21.53	21.53	11.80	188	21.53	21.53	11.72	208	21.54	21.54	10.92
169	21.53	21.53	11.80	189	21.54	21.54	11.60	209	21.54	21.54	10.91
170	21.53	21.53	11.80	190	21.54	21.54	11.57	210	21.54	21.54	10.91
171	21.53	21.53	11.80	191	21.54	21.54	11.56				

2.3. VALUTAZIONE DEL PARAMETRO θ

2.3.1. Metodo di calcolo

Il coefficiente θ è stato valutato mediante il modello agli elementi finiti sul quale è stata eseguita un'analisi sismica statica bloccando i nodi di piede dei pilastri (incastri) per evitare l'influenza delle fondazioni e bloccando le rotazioni Rx ed Ry dei nodi di impalcato.

Il calcolo delle rigidezze di piano viene effettuato dividendo il tagliante di piano (somma delle azioni sismiche sopra il piano in esame), per la differenza di spostamento del piano in esame con quello immediatamente precedente.

Il coefficiente θ viene calcolato secondo la formula (7.3.2) del par. 7.3.1 del D.M. 14/01/08

2.3.2. Risultati

Simbologia

Imp. = Numero dell'impalcato
 Sx = Spostamento impalcato in dir. X
 Rig X = Rigidezza teorica in direzione X
 Dif X % = Differenza percentuale della rigidezza X rispetto all'impalcato precedente
 Θ_x = Coefficiente Θ in dir. X
 Sy = Spostamento impalcato in dir. Y
 Rig Y = Rigidezza teorica in direzione Y
 Dif Y % = Differenza percentuale della rigidezza Y rispetto all'impalcato precedente
 Θ_y = Coefficiente Θ in dir. Y

Imp.	Sx <m>	Rig X <kg/m>	Dif X %	Θ_x	Sy <m>	Rig Y <kg/m>	Dif Y %	Θ_y
1	7.58E-004	803283000.00	0.00	3.18E-003	7.21E-004	843641000.00	0.00	0.00
2	3.28E-003	234331000.00	-70.83	7.44E-003	4.42E-003	160253000.00	-81.00	0.01
3	6.13E-003	207349000.00	-11.51	8.35E-003	9.54E-003	114979000.00	-28.25	0.02
4	9.21E-003	176945000.00	-14.66	8.08E-003	1.89E-002	58588400.00	-49.04	0.02
5	1.23E-002	162010000.00	-8.44	7.25E-003	3.00E-002	44354900.00	-24.29	0.03
6	1.50E-002	153777000.00	-5.08	6.10E-003	4.03E-002	41086600.00	-7.37	0.02
7	1.74E-002	144679000.00	-5.92	4.85E-003	4.89E-002	39299300.00	-4.35	0.02
8	1.92E-002	128949000.00	-10.87	3.60E-003	5.56E-002	36591000.00	-6.89	0.01
9	2.07E-002	90252400.00	-30.01	2.53E-003	6.02E-002	28070000.00	-23.29	0.01

Poiché il coefficiente risulta minore di 0.1 non si riduce il fattore di struttura.

2.4. SPOSTAMENTI RELATIVI MASSIMI

Essendo l'edificio di classe III si verificano gli spostamenti relativi d'interpiano nelle combinazioni agli Stati Limite di Danno ed allo stato limite di Operatività.

E' stato scelto come limite di spostamento relativo $0.005 H$ allo SLD e di $2/3 \times 0.005 H = 0.0033 H$ allo SLO.

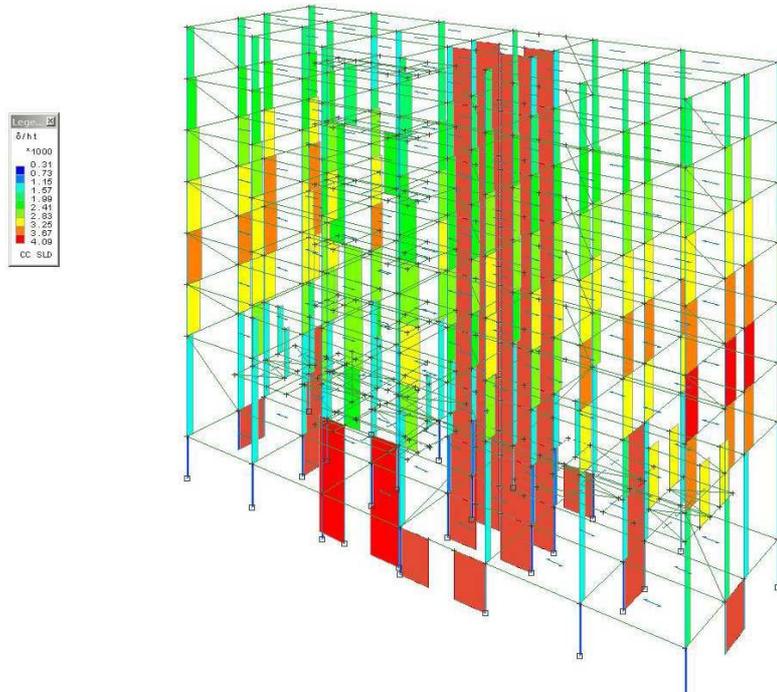


Figura 10 – Spostamenti differenziali massimi SLD

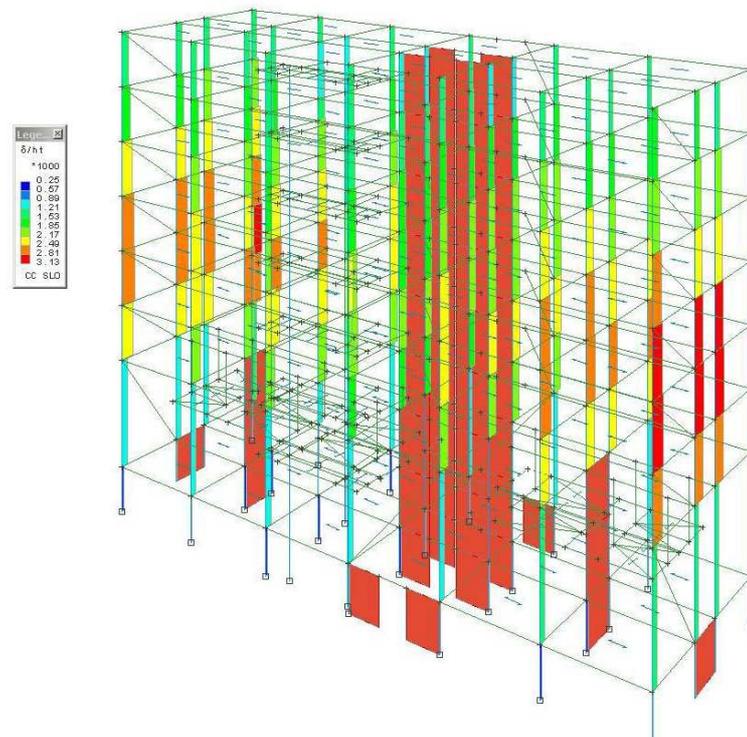


Figura 11 – Spostamenti differenziali massimi SLO

2.5. MODI DI VIBRARE

2.5.1. Primo modo di vibrare periodo 1.447 s.

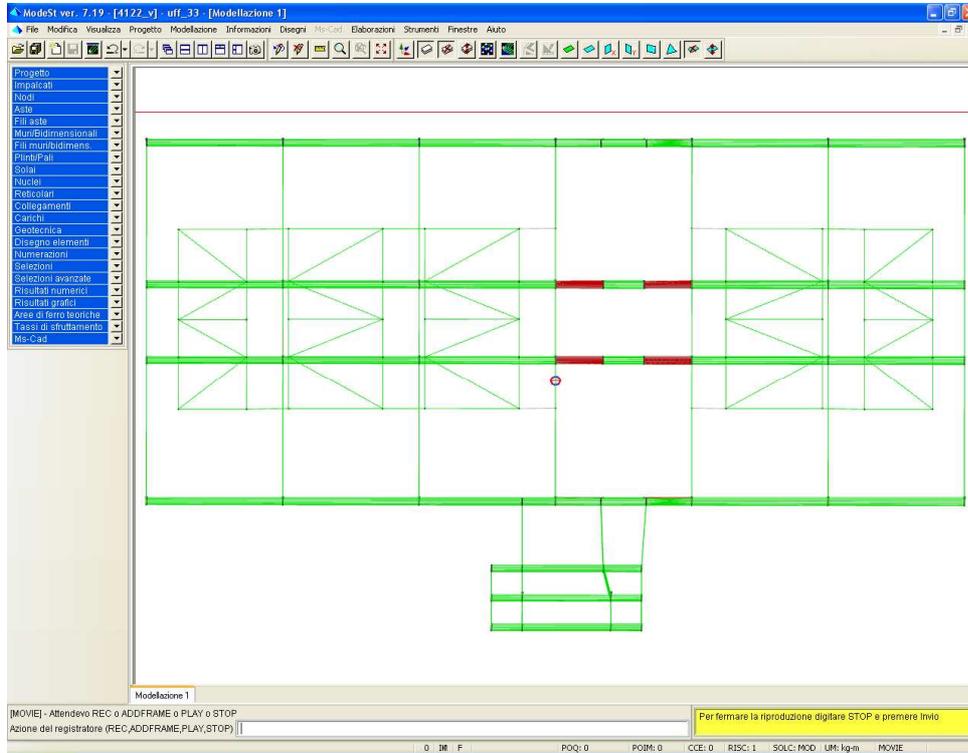


Figura 12 - Primo modo di vibrare

2.5.2. Secondo modo di vibrare periodo 1.182 s.

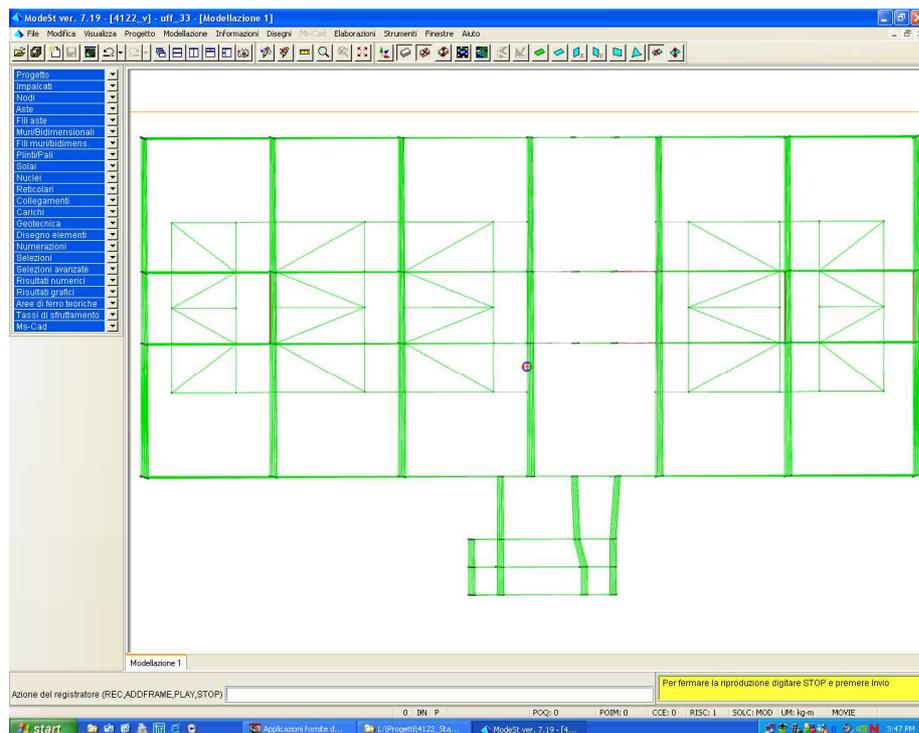
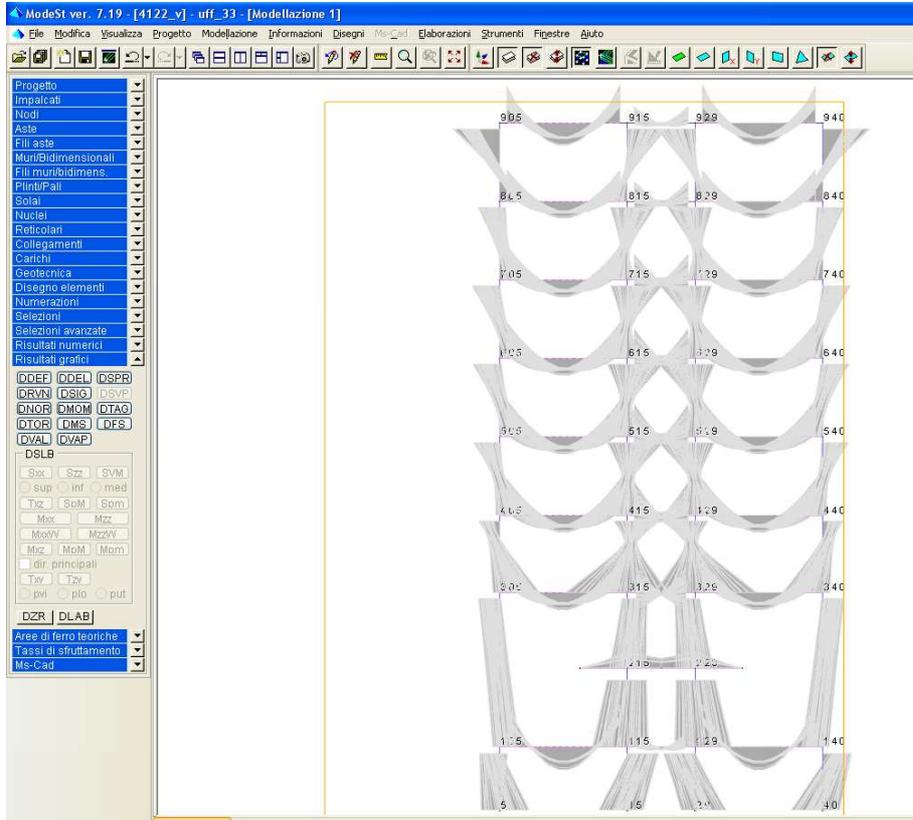


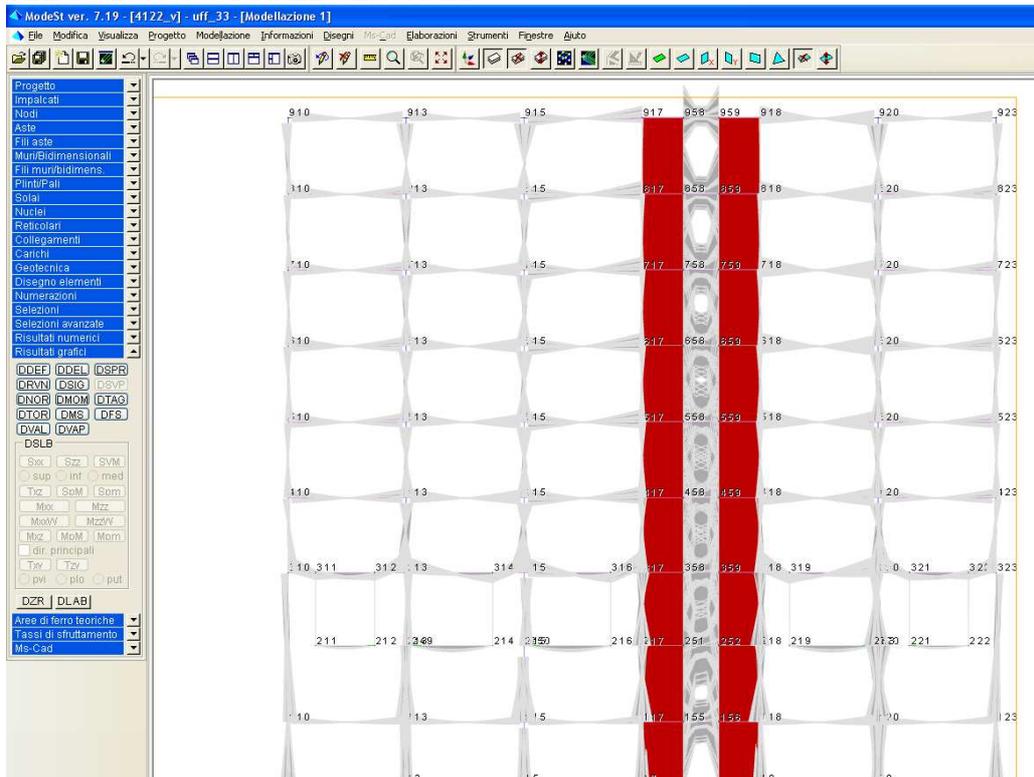
Figura 13 - secondo modo di vibrare

2.6. INVILUPPO DIAGRAMMI SOLLECITAZIONI

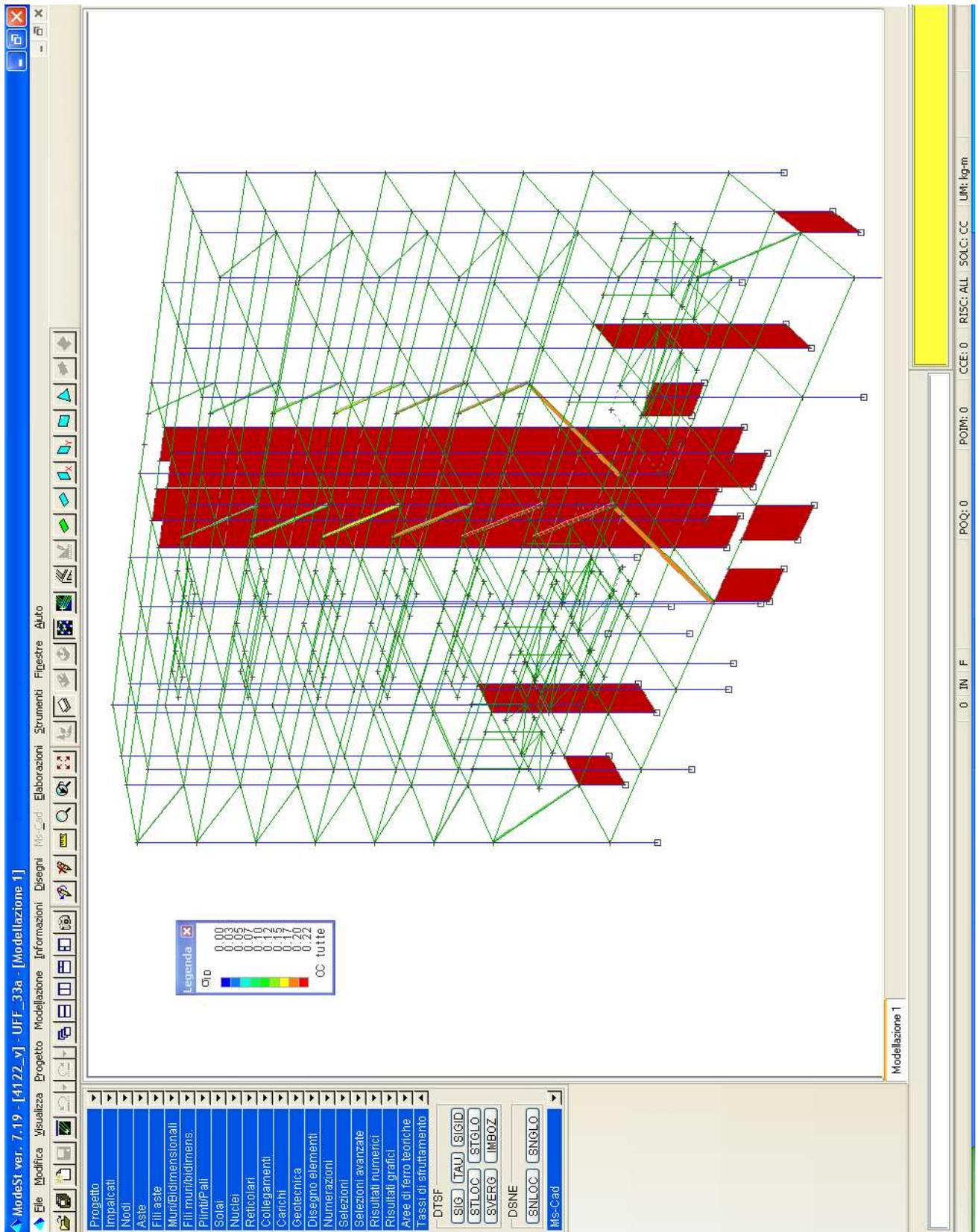
TELAIO TRASVERSALE CENTRALE



TELAIO LONGITUDINALE CENTRALE



2.7. PERCENTUALE DI SFRUTTAMENTO DEI CONTROVENTI METALLICI



2.8. –VERIFICA NODI IN ACCIAIO

2.8.1. Nodo controvento tipo a

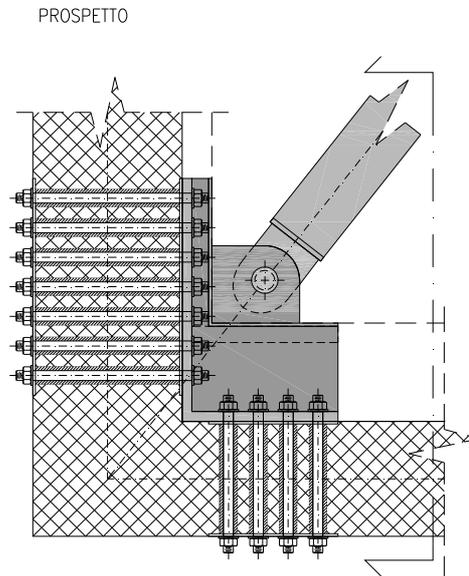


Figura 14 NODO COLLEGAMENTO DEL CONTROVENTO Ø193.7x11 ALLA STRUTTURA IN C.A.

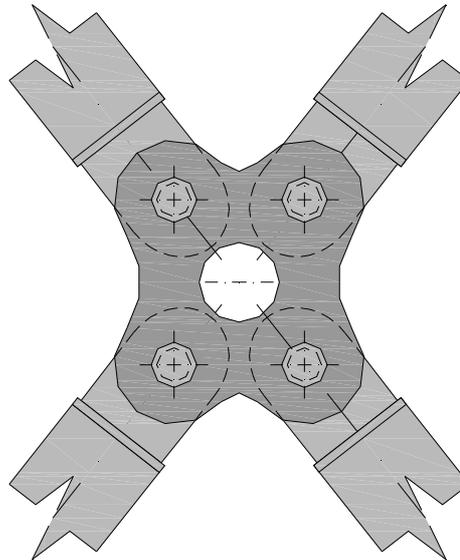


Figura 15 DETTAGLIO DEL COLLEGAMENTO DEI CONTROVENTI Ø193.7X11

tipo acciaio	f_{yk} [N/mm ²]	f_{tk} [N/mm ²]	γ_{rd} [N/mm ²]
S275	275	430	1.15
S355	355	510	1.1

Tabella 1 CARATTERISTICHE MECCANICHE ACCIAIO

I nodi di collegamento dei controventi alla struttura in calcestruzzo armato sono stati calcolati a completo ripristino.

RESISTENZA DI PROGETTO A TRAZIONE DEL CONTROVENTO Ø 193.7x11								
tubo	tipo acciaio	A [cm ²]	J [cm ⁴]	W [cm ³]	f _{yk} [N/mm ²]	γ _{rd}	N _{pl,rd} [N]	R _{j,rd} [N]
193.7x11	S275	63.1	2644	273	275	1.15	1652619	2090563.1

Tabella 2 rESISTENZA DI PROGETTO A TRAZIONE DEL CONTROVENTO Ø193.7x11

VERIFICA AREA LORDA DEL COLLEGAMENTO PER CONTROVENTO Ø 193.7x11									
tipo acciaio	f _{yk} [N/mm ²]	R _{j,rd} [N]	n _{piastre} [-]	d _{tondo} [cm]	B [cm]	sp. [cm]	A _{lord.prog.} [cm ²]	A _{lord.calc.} [cm ²]	VERIFICA
S355	355	2090563	2	6	18	3	54	33.861233	SI

Tabella 3 VERIFICA AREA LORDA DEL COLLEGAMENTO PER CONTROVENTO Ø193.7X11

VERIFICA AREA NETTA DEL COLLEGAMENTO PER CONTROVENTO Ø 193.7X11									
tipo acciaio	f _{tk} [N/mm ²]	R _{j,rd} [N]	n _{piastre} [-]	d _{tondo} [cm]	B-d _{tondo} [cm]	sp. [cm]	A _{net.prog.} [cm ²]	A _{net.calc.} [cm ²]	VERIFICA
S355	510	2090563	2	6	12	3	36	28.466273	SI

Tabella 4 VERIFICA AREA NETTA DEL COLLEGAMENTO PER CONTROVENTO Ø193.7X11

CALCOLO SPESSORE MINIMO DELLA PIASTRA DI COLLEGAMENTO CONTROVENTO Ø 193.7X11												
tipo acciaio	f _{tk} [N/mm ²]	R _{j,rd} [N]	n _{piastre} [-]	d _{tondo} [mm]	e ₁ [mm]	e ₁ /3d ₀ [-]	f _{tb} /f _t [-]	α	e ₂ [mm]	e ₂ /d ₀ [-]	k	t _{min.} [mm]
S355	510	2090563	2	60	105	0.583333	1	0.58	90	1.5	2.5	29.2796

Tabella 5 CALCOLO SPESSORE MINIMO DELLA PIASTRA DI COLLEGAMENTO CONTROVENTO Ø193.7X11

VERIFICA A TAGLIO TONDO CONTROVENTO Ø 193.7x11							
tipo acciaio	f _{tk} [N/mm ²]	d _{tondo} [mm]	A [mm ²]	Piani di Taglio [-]	F _{v,rd} [N]	F _{v,Ed} [N]	VERIFICA
S355	510	60	2827.4334	4	692155.7	522640.8	SI

Tabella 6 VERIFICA A TAGLIO TONDO CONTROVENTO Ø193.7X11

2.8.2. Nodo controvento tipo

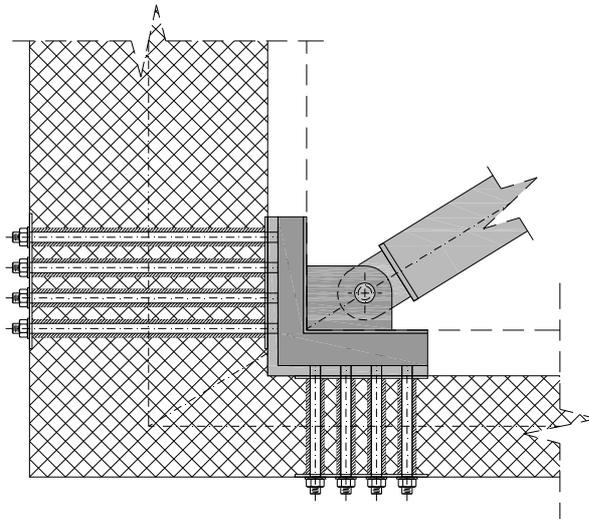


Figura 16 NODO PER COLLEGAMENTO CONTROVENTO Ø193.7X5

RESISTENZA DI PROGETTO DEL CONTROVENTO Ø193.7x5								
tubo	tipo acciaio	A [cm ²]	J [cm ⁴]	W [cm ³]	f _{yk} [N/mm ²]	γ _{rd}	N _{pl,rd} [N]	R _{j,rd} [N]
193.7x5	S275	29.6	1320	136	275	1.15	775238.1	980676.19

Tabella 7 RESISTENZA DI PROGETTO DEL CONTROVENTO Ø193.7x5

VERIFICA AREA LORDA DEL COLLEGAMENTO DEL CONTROVENTO Ø193.7x5									
tipo acciaio	f _{yk} [N/mm ²]	R _{j,rd} [N]	n _{piastre} [-]	d _{tondo} [cm]	B [cm]	sp. [cm]	A _{lord,prog.} [cm ²]	A _{lord.calc.} [cm ²]	VERIFICA
S355	510	980676.2	2	4	16	2	32	11.056643	SI

Tabella 8 VERIFICA AREA LORDA DEL COLLEGAMENTO DEL CONTROVENTO Ø193.7X5

VERIFICA AREA NETTA DEL COLLEGAMENTO DEL COLLEGAMENTO Ø193.7x5									
tipo acciaio	f _{tk} [N/mm ²]	R _{j,rd} [N]	n _{piastre} [-]	d _{tondo} [cm]	B-d _{tondo} [cm]	sp. [cm]	A _{net,prog.} [cm ²]	A _{net.calc.} [cm ²]	VERIFICA
S355	510	980676.2	2	4	8	2	16	13.353434	SI

Tabella 9 verifica area netta del collegamento Ø193.7X5

CALCOLO DELLO SPESSORE MINIMO DELLA PIASTRA CONTROVENTO Ø193.7x5												
tipo acciaio	f _{tk} [N/mm ²]	R _{j,rd} [N]	n _{piastre} [-]	d _{tondo} [mm]	e ₁ [mm]	e ₁ /3d ₀ [-]	f _{tb} /f _t [-]	α	e ₂ [mm]	e ₂ /d ₀ [-]	k	t _{min.} [mm]
S355	510	980676.2	2	40	80	0.666667	1	0.667	80	2	2.5	18.02714

Tabella 10 CALCOLO DELLO SPESSORE MINIMO DELLA PIASTRA CONTROVENTO Ø193.7x5

VERIFICA A TAGLIO TONDO CONTROVENTO Ø193.7x5							
tipo acciaio	f_{tk} [N/mm ²]	d_{tondo} [mm]	A [mm ²]	Piani di Taglio [-]	$F_{v,rd}$ [N]	$F_{v,Ed}$ [N]	VERIFICA
S355	510	40	1256.6371	4	307624.8	245169	SI

Tabella 11 VERIFICA A TAGLIO TONDO CONTROVENTO Ø193.7X5

2.8.3. Collegamento tubolari Ø101.6x8 alla struttura in c.a.

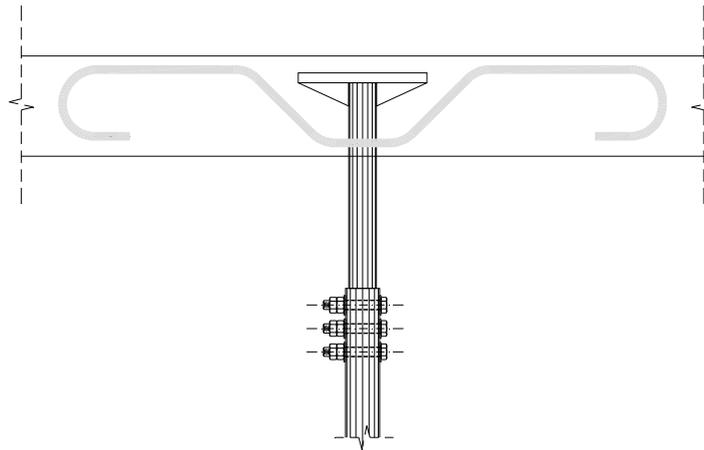


Figura 17 COLLEGAMENTO TUBOLARE Ø101.6X8 ALLA TRAVE IN C.A.

RESISTENZA PLASTICA A TRAZIONE DELLA SEZIONE NETTA E LORDA								
profilato	A [mm ²]	tipo acciaio	f_{yk} [N/mm ²]	f_{tk} [N/mm ²]	d_0 [mm]	A_{net} [mm ²]	$N_{pl,Rd}$ [N]	$N_{u,Rd}$ [N]
Ø101.6x8	2350	S275	275	430	28.5	1894	615476.2	586382.4

Tabella 12 RESISTENZA PLASTICA A TRAZIONE DELLA SEZIONE NETTA E LORDA

VERIFICA A TAGLIO BULLONI PENDINO Ø101.6X8							
CLASSE	$N_{bullone}$ [-]	$N_{piani\ taglio}$ [-]	d [mm]	$A_{res.}$ [mm ²]	$F_{v,Ed}$ [N]	$F_{v,Rd}$ [N]	VERIFICA
8.8	3	2	27	459	117276.5	146880	SI

Tabella 13 VERIFICA A TAGLIO BULLONI PENDINO Ø101.6X8

VERIFICA A RIFOLLAMENTO PENDINO Ø101.6X8												
CLASSE	d_0 [mm]	t [mm]	f_{tk} [N/mm ²]	e_1 [mm]	e_2 [mm]	f_{tb}/f_t [-]	$e_1/3d_0$ [-]	α_{min} [-]	k_{min}	$F_{b,Ed}$ [N]	$F_{b,Rd}$ [N]	VERIFICA
S275	27	8	430	70	70	1.86	0.86	0.86	2.5	117276.5	160533.3	SI

Tabella 14 VERIFICA A RIFOLLAMENTO PENDINO Ø101.6X8

VERIFICA PRESSIONE DI CONTATTO ROSETTA PER PENDINO Ø101.6X8											
CLASSE	d_1 [mm]	d_2 [mm]	t [mm]	tipo acciaio	f_{yk} [N/mm ²]	Area [mm]	R_{ck} [N/mm ²]	f_{cd} [N/mm ²]	$f_{c,E}$ [N/mm ²]	$F_{b,Ed}$ [N]	VERIFICA
S275	101.6	251.6	70	S275	275	41610.3947	35	16.46167	14.092	586382.4	SI

Tabella 15 VERIFICA PRESSIONE DI CONTATTO ROSETTA PER PENDINO Ø101.6X8

VERIFICA A FLESSIONE ROSETTA PER PENDINO					
q	I ₀	W _{pl}	M _{max}	M _{pl,Rd}	VERIFICA
[N/mm]	[mm]	[mm ³]	[Nmm]	[Nmm]	
140.9221	150	8166.667	1585374	2138889	SI

Tabella 16 VERIFICA A FLESSIONE ROSETTA PER PENDINO Ø101.6X8

3. MODELLAZIONE B

3.1. PARAMETRI DI CALCOLO

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con: ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti: Xfinest ver. 8.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08

Tipo di calcolo: analisi sismica dinamica

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <kg/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: ISOSHELL
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Si
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per Buckling: No
- Trascura Buckling torsionale: No

Dati struttura

- Zona sismica: zona 3
- Sito di costruzione: LON. 11.18240 LAT. 43.75800
- Contenuto tra ID reticolo: 20058 20057 20280 20279

Simbologia

TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 Ag = Accelerazione orizzontale massima al sito
 FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

TCC	Ag	FO	TC*
SLO	0.5163	2.59	0.26
SLD	0.6103	2.63	0.28
SLV	1.4446	2.39	0.30

- Tipo di opera: Opera ordinaria
- Vita nominale V_N : 50.00
- Classe d'uso: classe III
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 3.15 <m>
- Numero piani edificio: 0
- Coefficiente θ : 0
- Edificio regolare in altezza: no
- Edificio regolare in pianta: no
- Forze orizzontali convenzionali per stati limite non sismici: no

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. o prefabbricato a telaio a più piani e più campate

Coeff. C_1	0.075
Periodo T_1	0.17733
Coeff. λ SLO	1.00
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α_s/α_t)	1.15
Valore di riferimento del fattore di struttura (q_0)	3.45
Fattore riduttivo (K_w)	1.00
Fattore di struttura (q)	1.50

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica: 1.00
- Modi da calcolare: 240
- Modi da considerare: con singola massa superiore a 0.50%
- Smorzamento spettro: 5.00

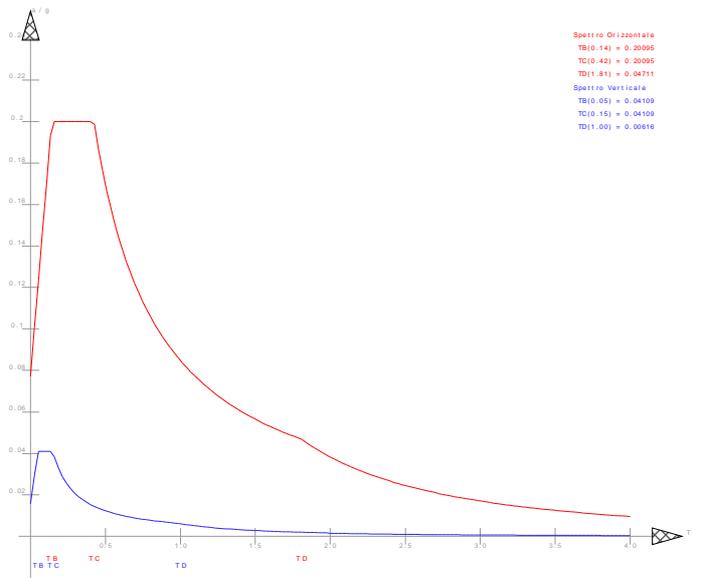


Figura numero 1: Spettro allo SLO

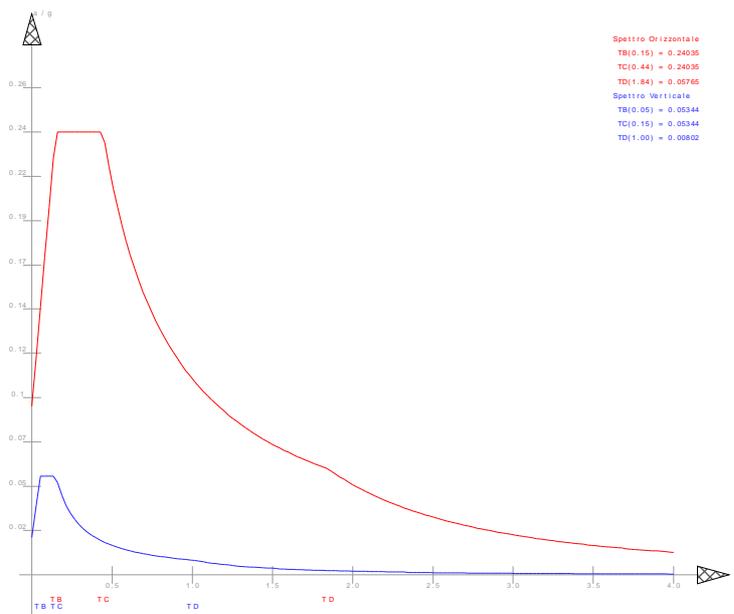


Figura numero 2: Spettro allo SLD

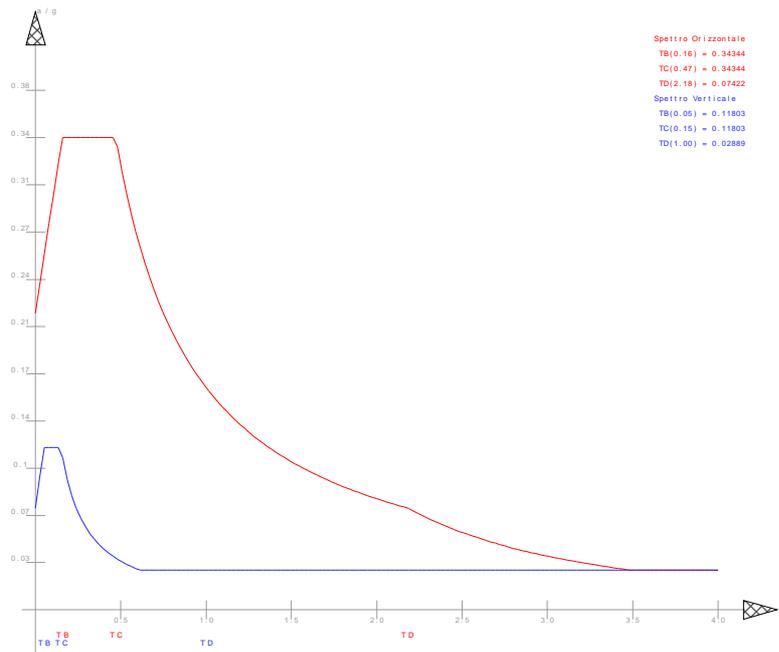


Figura numero 3: Spettro allo SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Condizioni di carico elementari

Simbologia

- CCE = Numero della condizione di carico elementare
- Comm. = Commento
- s = Coeff. di riduzione
- Mx = Moltiplicatore della massa in dir. X
- My = Moltiplicatore della massa in dir. Y
- Mz = Moltiplicatore della massa in dir. Z
- Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
- Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
- Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	s	Mx	My	Mz	Jpx	Jpy	Jpz
1	pp e perm	1.00	1.00	1.00	0.00	0.00	0.00	1.00
2	permanente solette	1.00	1.00	1.00	0.00	0.00	0.00	1.00
3	carrabile	1.00	1.00	1.00	0.00	0.00	0.00	1.00
4	permanenti non strutturali solai	1.00	1.00	1.00	0.00	0.00	0.00	1.00
5	grigliati esterni (10)	1.00	1.00	1.00	0.00	0.00	0.00	1.00
6	spinta della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
7	spinta accidentale della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
8	variazione termica uniforme	1.00	0.00	0.00	0.00	0.00	0.00	0.00
9	reazione scala	1.00	0.00	0.00	0.00	0.00	0.00	0.00
10	Sisma dir. X - SLO	--	--	--	--	--	--	--
11	Sisma dir. Y - SLO	--	--	--	--	--	--	--
12	Sisma dir. X - SLD	--	--	--	--	--	--	--
13	Sisma dir. Y - SLD	--	--	--	--	--	--	--
14	Sisma dir. X - SLV	--	--	--	--	--	--	--
15	Sisma dir. Y - SLV	--	--	--	--	--	--	--

Elenco tipi cce definiti

Simbologia

- Tipo CCE = Tipo condizione di carico elementare
- Comm. = Commento
- Tipo = Tipologia
 - G = Permanente
 - Q = Variabile
 - I = Da ignorare
 - A = Azione eccezionale
 - P = Precompressione
- Durata = Durata del carico
 - N = Non definita
 - P = Permanente
 - L = Lunga
 - M = Media
 - B = Breve
 - I = Istantanea
- $\gamma_{min.}$ = Coeff. $\gamma_{min.}$

γ_{max} = Coeff. γ_{max}
 ψ_0 = Coeff. ψ_0
 ψ_1 = Coeff. ψ_1
 ψ_2 = Coeff. ψ_2
 $\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo	CCE	Comm.	Tipo	Durata	γ_{min}	γ_{max}	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$
1	Perm.	STR	G	P	1.00	1.30				
2	Perm.	NON STR	G	N	0.00	1.50				
3	A-	ABITAZIONI	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
4	B-	UFFICI	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
5	C-	AFFOLLAMENTO	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
6	D-	COMMERCIALE	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
7	E-	INDUSTRIALE	Q	N	0.00	1.50	1.00	0.90	0.80	0.00
8	F	PARCHEGGI <30	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
9		CARRABILE	Q	N	0.00	1.50	0.17	0.17	0.15	0.00
10		VENTO	Q	N	0.00	1.50	0.60	0.20	0.00	0.00
11		NEVE	Q	N	0.00	1.50	0.50	0.20	0.00	0.00
12		temperatura	Q	N	0.00	1.50	0.60	0.50	0.00	0.00
13		reazione scala	Q	N	1.00	1.00	1.00	1.00	1.00	0.00
14	D.M. 96	Permanenti	G	N	1.00	1.40				
15	D.M. 96	Variabili A	Q	N	0.00	1.50	0.70	0.50	0.20	0.70
16	D.M. 96	Variabili U	Q	N	0.00	1.50	0.70	0.60	0.30	0.70
17	D.M. 96	Variabili A	Q	N	0.00	1.50	0.70	0.70	0.60	0.70
18	D.M. 96	Variabili V	Q	N	0.00	1.50	0.70	0.20	0.00	0.00

Ambienti di carico

Simbologia

N Numero

Comm. Commento

1 pp e perm

2 permanente solette

3 carrabile

4 permanenti non strutturali solai

5 grigliati esterni (10)

6 spinta della terra

7 spinta accidentale della terra

8 variazione termica uniforme

9 reazione scala

F azioni orizzontali convenzionali

SLU Stato limite ultimo

SLR Stato limite per combinazioni rare

SLF Stato limite per combinazioni frequenti

SLQ Stato limite per combinazioni quasi permanenti o di danno

N	Comm.	1	2	3	4	5	6	7	8	9	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	si	no	no	no										
2	Calcolo statico	si	no	si	si	si									

Elenco combinazioni di carico simboliche

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLU S = Stato limite ultimo (azione sismica)

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SLV = Stato limite di salvaguardia della vita

SLC = Stato limite di prevenzione del collasso

SLO = Stato limite di operatività

CC	Comm.	TCC	1	2	3	4	5	6	7	8	9	$\pm S$	
1	Amb. 1 (SLU S)	SLU S	1	ψ_2	1	ψ_2	1	ψ_2	ψ_2	ψ_2	ψ_2	1	
2	Amb. 2 (SLU)	SLU	γ_{max}	ψ_0^*	γ_{max}	----							
3	Amb. 2 (SLE R)	SLE R	1	1	1	1	1	1	1	1	ψ_0	1	----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	1	ψ_1	1	ψ_1	1	ψ_2	ψ_1	----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	1	ψ_2	1	ψ_2	ψ_2	ψ_2	----	

Combinazioni delle cce

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
 Comm. = Commento
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 An. = Tipo di analisi
 L = Lineare
 NL = Non lineare
 Bk = Buckling
 S = Si
 N = No

CC Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	8	9	±S X	±S Y
1 CC 1 - Amb. 1 (SLU S) S +X+0.3Y	SLV	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.16	1.00	0.30
2 CC 2 - Amb. 1 (SLU S) S +X+0.3Y	SLD	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	3.99	1.00	0.30
3 CC 3 - Amb. 1 (SLU S) S +X+0.3Y	SLO	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.07	1.00	0.30
4 CC 4 - Amb. 1 (SLU S) S +X-0.3Y	SLV	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.16	1.00	-0.30
5 CC 5 - Amb. 1 (SLU S) S +X-0.3Y	SLD	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	3.99	1.00	-0.30
6 CC 6 - Amb. 1 (SLU S) S +X-0.3Y	SLO	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.07	1.00	-0.30
7 CC 7 - Amb. 1 (SLU S) S +0.3X+Y	SLV	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.16	0.30	1.00
8 CC 8 - Amb. 1 (SLU S) S +0.3X+Y	SLD	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	3.99	0.30	1.00
9 CC 9 - Amb. 1 (SLU S) S +0.3X+Y	SLO	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.07	0.30	1.00
10 CC 10 - Amb. 1 (SLU S) S -0.3X+Y	SLV	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.16	-0.30	1.00
11 CC 11 - Amb. 1 (SLU S) S -0.3X+Y	SLD	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	3.99	-0.30	1.00
12 CC 12 - Amb. 1 (SLU S) S -0.3X+Y	SLO	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	4.07	-0.30	1.00
13 CC 13 - Amb. 2 (SLU)	SLU	L	N	1.30	1.30	1.50	1.30	1.50	1.30	1.50	0.90	6.78	0.00	0.00
14 CC 14 - Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.60	4.67	0.00	0.00
15 CC 15 - Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.17	1.00	0.17	1.00	0.17	0.00	3.86	0.00	0.00
16 CC 16 - Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.15	1.00	0.15	1.00	0.15	0.00	3.59	0.00	0.00

Elenco masse nodi

Simbologia

Nodo = Numero del nodo
 Mo = Massa orizzontale

| Nodo Mo |
|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| <KG> |
-8109 3.51	-8102 16.06	-8101 16.65	-8100 16.22	-8099 16.22	-8098 16.22	-8097 16.86	-8096 17.50
-8095 17.50	-8094 17.50	-8093 17.50	-8092 17.50	-8091 17.50	-8090 17.50	-8089 17.07	-8088 17.07
-8087 17.07	-8086 17.93	-8085 18.78	-8084 18.78	-8083 18.78	-8082 17.07	-8081 15.37	-8080 15.37
-8079 15.37	-8078 17.93	-8077 17.93	-8076 17.93	-8075 16.65	-8074 15.37	-8073 15.37	-8072 15.37
-8071 16.65	-8070 17.93	-8069 17.93	-8068 17.93	-8067 16.62	-8066 16.62	-8065 16.82	-8064 17.02
-8063 17.02	-8062 17.02	-8061 17.02	-8060 17.02	-8059 17.33	-8058 17.64	-8057 17.64	-8056 17.07
-8055 17.07	-8054 17.07	-8053 17.07	-8052 17.07	-8051 17.07	-8050 17.07	-8049 17.07	-8048 17.07
-8047 17.07	-8046 17.07	-8045 17.50	-8044 17.50	-8043 17.50	-8042 17.51	-8041 17.53	-8040 17.53
-8039 17.53	-8038 16.86	-8037 16.20	-8036 16.20	-8035 16.20	-8034 3.84	-8033 24.32	-8032 32.25
-8031 31.43	-8030 31.43	-8029 31.43	-8028 32.67	-8027 33.91	-8026 33.91	-8025 33.91	-8024 33.91
-8023 33.91	-8022 33.91	-8021 33.91	-8020 33.50	-8019 33.08	-8018 33.08	-8017 33.08	-8016 34.74
-8015 36.39	-8014 36.39	-8013 36.39	-8012 33.08	-8011 29.77	-8010 29.77	-8009 29.77	-8008 32.25
-8007 34.74	-8006 34.74	-8005 34.74	-8004 32.25	-8003 29.77	-8002 29.77	-8001 29.77	-8000 32.25
-7999 34.74	-7998 34.74	-7997 34.74	-7996 33.47	-7995 32.20	-7994 32.20	-7993 32.59	-7992 32.97
-7991 32.97	-7990 32.97	-7989 32.97	-7988 32.97	-7987 33.58	-7986 34.18	-7985 34.18	-7984 33.63
-7983 33.08	-7982 33.08	-7981 33.08	-7980 33.08	-7979 33.08	-7978 33.08	-7977 33.08	-7976 33.08
-7975 33.08	-7974 33.08	-7973 33.08	-7972 33.50	-7971 33.91	-7970 33.91	-7969 33.91	-7968 33.93
-7967 33.96	-7966 33.96	-7965 33.96	-7964 32.67	-7963 31.38	-7962 31.38	-7961 31.38	-7960 23.13
-7959 7.44	-7958 23.53	-7957 31.21	-7956 30.41	-7955 30.41	-7954 30.41	-7953 31.61	-7952 32.81
-7951 32.81	-7950 32.81	-7949 32.81	-7948 32.81	-7947 32.81	-7946 32.81	-7945 32.41	-7944 32.01
-7943 32.01	-7942 32.01	-7941 33.62	-7940 35.22	-7939 35.22	-7938 35.22	-7937 32.01	-7936 28.81
-7935 28.81	-7934 28.81	-7933 31.21	-7932 33.62	-7931 33.62	-7930 33.62	-7929 31.21	-7928 28.81
-7927 28.81	-7926 28.81	-7925 31.21	-7924 33.62	-7923 33.62	-7922 33.62	-7921 32.39	-7920 31.16
-7919 31.16	-7918 31.53	-7917 31.91	-7916 31.91	-7915 31.91	-7914 31.91	-7913 31.91	-7912 32.49
-7911 33.08	-7910 33.08	-7909 32.55	-7908 32.01	-7907 32.01	-7906 32.01	-7905 32.01	-7904 32.01
-7903 32.01	-7902 32.01	-7901 32.01	-7900 32.01	-7899 32.01	-7898 32.01	-7897 32.41	-7896 32.81
-7895 32.81	-7894 32.81	-7893 32.84	-7892 32.86	-7891 32.86	-7890 32.86	-7889 31.61	-7888 30.37
-7887 30.37	-7886 30.37	-7885 22.39	-7884 7.20	-7883 26.83	-7882 35.58	-7881 34.67	-7880 34.67
-7879 34.67	-7878 36.04	-7877 37.41	-7876 37.41	-7875 37.41	-7874 37.41	-7873 37.41	-7872 37.41
-7871 37.41	-7870 36.95	-7869 36.50	-7868 36.50	-7867 36.50	-7866 38.32	-7865 40.15	-7864 40.15
-7863 40.15	-7862 36.50	-7861 32.85	-7860 32.85	-7859 32.85	-7858 35.58	-7857 38.32	-7856 38.32
-7855 38.32	-7854 35.58	-7853 32.85	-7852 32.85	-7851 32.85	-7850 35.58	-7849 38.32	-7848 38.32
-7847 38.32	-7846 36.92	-7845 35.52	-7844 35.52	-7843 35.95	-7842 36.37	-7841 36.38	-7840 36.37
-7839 36.37	-7838 36.38	-7837 37.04	-7836 37.71	-7835 37.71	-7834 37.10	-7833 36.50	-7832 36.50
-7831 36.50	-7830 36.50	-7829 36.50	-7828 36.50	-7827 36.50	-7826 36.50	-7825 36.50	-7824 36.50
-7823 36.50	-7822 36.95	-7821 37.41	-7820 37.41	-7819 37.41	-7818 37.44	-7817 37.46	-7816 37.46
-7815 37.46	-7814 36.04	-7813 34.62	-7812 34.62	-7811 34.62	-7810 25.52	-7809 8.21	-7808 30.12
-7807 39.95	-7806 38.93	-7805 38.93	-7804 38.93	-7803 40.47	-7802 42.00	-7801 42.00	-7800 42.00
-7799 42.00	-7798 42.00	-7797 42.00	-7796 42.00	-7795 41.49	-7794 40.98	-7793 40.98	-7792 40.98
-7791 43.03	-7790 45.08	-7789 45.08	-7788 45.08	-7787 40.98	-7786 36.88	-7785 36.88	-7784 36.88
-7783 39.95	-7782 43.03	-7781 43.03	-7780 43.03	-7779 39.95	-7778 36.88	-7777 36.88	-7776 36.88
-7775 39.95	-7774 43.03	-7773 43.03	-7772 43.03	-7771 41.46	-7770 39.89	-7769 39.89	-7768 40.36
-7767 40.84	-7766 40.84	-7765 40.84	-7764 40.84	-7763 40.84	-7762 41.59	-7761 42.34	-7760 42.34
-7759 41.66	-7758 40.98	-7757 40.98	-7756 40.98	-7755 40.98	-7754 40.98	-7753 40.98	-7752 40.98
-7751 40.98	-7750 40.98	-7749 40.98	-7748 40.98	-7747 41.49	-7746 42.00	-7745 42.00	-7744 42.00
-7743 42.03	-7742 42.06	-7741 42.06	-7740 42.06	-7739 40.47	-7738 38.87	-7737 38.87	-7736 38.87
-7735 28.65	-7734 9.22	-7733 30.12	-7732 39.95	-7731 38.93	-7730 38.93	-7729 38.93	-7728 40.47
-7727 42.00	-7726 42.00	-7725 42.00	-7724 42.00	-7723 42.00	-7722 42.00	-7721 42.00	-7720 41.49

-7719 40.98	-7718 40.98	-7717 40.98	-7716 43.03	-7715 45.08	-7714 45.08	-7713 45.08	-7712 40.98
-7711 36.88	-7710 36.88	-7709 36.88	-7708 39.95	-7707 43.03	-7706 43.03	-7705 43.03	-7704 39.95
-7703 36.88	-7702 37.63	-7701 36.88	-7700 39.20	-7699 43.03	-7698 43.03	-7697 43.03	-7696 41.46
-7695 39.89	-7694 39.89	-7693 40.36	-7692 40.84	-7691 40.84	-7690 40.84	-7689 40.84	-7688 40.84
-7687 41.59	-7686 42.34	-7685 42.34	-7684 41.66	-7683 40.98	-7682 40.98	-7681 40.98	-7680 40.98
-7679 40.98	-7678 40.98	-7677 40.98	-7676 40.98	-7675 40.98	-7674 40.98	-7673 40.98	-7672 41.49
-7671 42.00	-7670 42.00	-7669 42.00	-7668 42.03	-7667 42.06	-7666 42.06	-7665 42.06	-7664 40.47
-7663 38.87	-7662 38.87	-7661 38.87	-7660 28.65	-7659 9.22	-7658 28.66	-7657 38.01	-7656 37.04
-7655 37.04	-7654 37.04	-7653 38.50	-7652 39.96	-7651 39.96	-7650 39.96	-7649 39.96	-7648 39.96
-7647 39.96	-7646 39.96	-7645 39.47	-7644 38.99	-7643 38.99	-7642 38.99	-7641 40.94	-7640 42.89
-7639 42.89	-7638 42.89	-7637 38.99	-7636 35.09	-7635 35.09	-7634 35.09	-7633 38.01	-7632 40.94
-7631 40.94	-7630 40.94	-7629 38.01	-7628 35.09	-7627 38.63	-7626 35.09	-7625 34.47	-7624 40.94
-7623 40.94	-7622 40.94	-7621 39.44	-7620 37.95	-7619 37.95	-7618 38.40	-7617 38.86	-7616 38.86
-7615 38.86	-7614 38.86	-7613 38.86	-7612 39.57	-7611 40.29	-7610 40.29	-7609 39.64	-7608 38.99
-7607 38.99	-7606 38.99	-7605 38.99	-7604 38.99	-7603 38.99	-7602 38.99	-7601 38.99	-7600 38.99
-7599 38.99	-7598 38.99	-7597 39.47	-7596 39.96	-7595 39.96	-7594 39.96	-7593 39.99	-7592 40.02
-7591 40.02	-7590 40.02	-7589 38.50	-7588 36.98	-7587 36.98	-7586 36.98	-7585 27.26	-7584 8.77
-7583 27.19	-7582 36.07	-7581 35.14	-7580 35.14	-7579 35.14	-7578 36.53	-7577 37.92	-7576 37.92
-7575 37.92	-7574 37.92	-7573 37.92	-7572 37.92	-7571 37.92	-7570 37.46	-7569 36.99	-7568 36.99
-7567 36.99	-7566 38.84	-7565 40.69	-7564 40.69	-7563 40.69	-7562 36.99	-7561 33.30	-7560 33.30
-7559 33.30	-7558 36.07	-7557 38.84	-7556 38.84	-7555 38.84	-7554 36.07	-7553 33.30	-7552 37.36
-7551 33.30	-7550 32.00	-7549 38.84	-7548 38.84	-7547 38.84	-7546 37.43	-7545 36.01	-7544 36.01
-7543 36.44	-7542 36.87	-7541 36.87	-7540 36.87	-7539 36.87	-7538 36.87	-7537 37.55	-7536 38.23
-7535 38.23	-7534 37.61	-7533 36.99	-7532 36.99	-7531 36.99	-7530 36.99	-7529 36.99	-7528 36.99
-7527 36.99	-7526 36.99	-7525 36.99	-7524 36.99	-7523 36.99	-7522 37.46	-7521 37.92	-7520 37.92
-7519 37.92	-7518 37.95	-7517 37.97	-7516 37.97	-7515 37.97	-7514 36.53	-7513 35.09	-7512 35.09
-7511 35.09	-7510 25.87	-7509 8.32	-7508 27.19	-7507 36.07	-7506 35.14	-7505 35.14	-7504 35.14
-7503 36.53	-7502 37.92	-7501 37.92	-7500 37.92	-7499 37.92	-7498 37.92	-7497 37.92	-7496 37.92
-7495 37.46	-7494 36.99	-7493 36.99	-7492 36.99	-7491 38.84	-7490 40.69	-7489 40.69	-7488 40.69
-7487 36.99	-7486 33.30	-7485 33.30	-7484 33.30	-7483 36.07	-7482 38.84	-7481 38.84	-7480 38.84
-7479 36.07	-7478 33.30	-7477 37.36	-7476 33.30	-7475 32.00	-7474 38.84	-7473 38.84	-7472 38.84
-7471 37.43	-7470 36.01	-7469 36.01	-7468 36.44	-7467 36.87	-7466 36.87	-7465 36.87	-7464 36.87
-7463 36.87	-7462 37.55	-7461 38.23	-7460 38.23	-7459 37.61	-7458 36.99	-7457 36.99	-7456 36.99
-7455 36.99	-7454 36.99	-7453 36.99	-7452 36.99	-7451 36.99	-7450 36.99	-7449 36.99	-7448 36.99
-7447 37.46	-7446 37.92	-7445 37.92	-7444 37.92	-7443 37.95	-7442 37.97	-7441 37.97	-7440 37.97
-7439 36.53	-7438 35.09	-7437 35.09	-7436 35.09	-7435 25.87	-7434 8.32	-7433 27.46	-7432 36.42
-7431 35.48	-7430 35.48	-7429 35.48	-7428 36.88	-7427 38.28	-7426 38.28	-7425 38.28	-7424 38.28
-7423 38.28	-7422 38.28	-7421 38.28	-7420 37.82	-7419 37.35	-7418 37.35	-7417 37.35	-7416 39.22
-7415 41.09	-7414 41.09	-7413 41.09	-7412 37.35	-7411 33.62	-7410 33.62	-7409 33.62	-7408 36.42
-7407 39.22	-7406 39.22	-7405 39.22	-7404 36.42	-7403 33.62	-7402 37.03	-7401 33.00	-7400 39.22
-7399 39.22	-7398 39.22	-7397 37.79	-7396 36.35	-7395 36.35	-7394 37.23	-7393 37.23	-7392 37.23
-7391 37.23	-7390 37.23	-7389 37.91	-7388 38.60	-7387 38.60	-7386 37.97	-7385 37.35	-7384 37.35
-7383 37.35	-7382 37.35	-7381 37.35	-7380 37.35	-7379 37.35	-7378 37.35	-7377 37.35	-7376 37.35
-7375 37.35	-7374 37.82	-7373 38.28	-7372 38.28	-7371 38.28	-7370 38.31	-7369 38.34	-7368 38.34
-7367 38.34	-7366 36.88	-7365 35.43	-7364 35.43	-7363 35.43	-7362 26.12	-7361 8.40	-7360 27.72
-7359 36.76	-7358 35.82	-7357 35.82	-7356 35.82	-7355 37.23	-7354 38.65	-7353 38.65	-7352 38.65
-7351 38.65	-7350 38.65	-7349 38.65	-7348 38.65	-7347 38.18	-7346 37.71	-7345 37.71	-7344 37.71
-7343 39.59	-7342 41.48	-7341 41.48	-7340 41.48	-7339 37.71	-7338 33.94	-7337 33.94	-7336 33.94
-7335 36.76	-7334 39.59	-7333 39.59	-7332 39.59	-7331 36.76	-7330 33.94	-7329 34.63	-7328 33.94
-7327 36.07	-7326 39.59	-7325 39.59	-7324 39.59	-7323 38.15	-7322 36.70	-7321 36.70	-7320 37.14
-7319 37.58	-7318 37.58	-7317 37.58	-7316 37.58	-7315 37.58	-7314 38.27	-7313 38.96	-7312 38.96
-7311 38.33	-7310 37.71	-7309 37.71	-7308 37.71	-7307 37.71	-7306 37.71	-7305 37.71	-7304 37.71
-7303 37.71	-7302 37.71	-7301 37.71	-7300 37.71	-7299 38.18	-7298 38.65	-7297 38.65	-7296 38.65
-7295 38.68	-7294 38.71	-7293 38.71	-7292 38.71	-7291 37.23	-7290 35.76	-7289 35.76	-7288 35.76
-7287 26.37	-7286 8.48	-7285 27.72	-7284 36.76	-7283 35.82	-7282 35.82	-7281 35.82	-7280 37.23
-7279 38.65	-7278 38.65	-7277 38.65	-7276 38.65	-7275 38.65	-7274 38.65	-7273 38.65	-7272 38.18
-7271 37.71	-7270 37.71	-7269 37.71	-7268 39.59	-7267 41.48	-7266 41.48	-7265 41.48	-7264 37.71
-7263 33.94	-7262 33.94	-7261 33.94	-7260 36.76	-7259 39.59	-7258 39.59	-7257 39.59	-7256 36.76
-7255 33.94	-7254 33.94	-7253 33.94	-7252 36.76	-7251 39.59	-7250 39.59	-7249 39.59	-7248 38.15
-7247 36.70	-7246 36.70	-7245 37.14	-7244 37.58	-7243 37.58	-7242 37.58	-7241 37.58	-7240 37.58
-7239 38.27	-7238 38.96	-7237 38.96	-7236 38.33	-7235 37.71	-7234 37.71	-7233 37.71	-7232 37.71
-7231 37.71	-7230 37.71	-7229 37.71	-7228 37.71	-7227 37.71	-7226 37.71	-7225 37.71	-7224 38.18
-7223 38.65	-7222 38.65	-7221 38.65	-7220 38.68	-7219 38.71	-7218 38.71	-7217 38.71	-7216 37.23
-7215 35.76	-7214 35.76	-7213 35.76	-7212 26.37	-7211 8.48	-7210 23.27	-7209 30.87	-7208 30.08
-7207 30.08	-7206 30.08	-7205 31.26	-7204 32.45	-7203 32.45	-7202 32.45	-7201 32.45	-7200 32.45
-7199 32.45	-7198 32.45	-7197 33.76	-7196 31.66	-7195 31.66	-7194 31.66	-7193 33.24	-7192 34.82
-7191 34.82	-7190 34.82	-7189 31.66	-7188 28.49	-7187 28.49	-7186 28.49	-7185 32.42	-7184 30.33
-7183 30.33	-7182 30.33	-7181 28.17	-7180 26.00	-7179 26.00	-7178 26.00	-7177 28.17	-7176 30.33
-7175 30.33	-7174 30.33	-7173 33.58	-7172 30.81	-7171 30.81	-7170 31.18	-7169 31.55	-7168 31.55
-7167 31.55	-7166 31.55	-7165 31.55	-7164 32.13	-7163 32.71	-7162 32.71	-7161 33.89	-7160 31.66
-7159 31.66	-7158 31.66	-7157 31.66	-7156 31.66	-7155 31.66	-7154 31.66	-7153 31.66	-7152 31.66
-7151 31.66	-7150 31.66	-7149 33.76	-7148 32.45	-7147 32.45	-7146 32.45	-7145 32.47	-7144 32.50
-7143 32.50	-7142 32.50	-7141 31.26	-7140 30.03	-7139 30.03	-7138 30.03	-7137 22.27	-7136 4.24
-7135 29.72	-7134 42.30	-7133 41.22	-7132 41.22	-7131 41.22	-7130 42.84	-7129 44.47	-7128 44.47
-7127 44.47	-7126 44.47	-7125 44.47	-7124 44.47	-7123 44.47	-7122 48.48	-7121 43.39	-7120 43.39
-7119 43.39	-7118 45.56	-7117 47.73	-7116 47.73	-7115 47.73	-7114 43.39	-7113 39.05	-7112 39.05
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-7087 43.39	-7086 43.39	-7085 48.48	-7084 44.47	-7083 44.47	-7082 44.47	-7081 44.50	-7080 44.54
-7079 44.54	-7078 44.54	-7077 42.84	-7076 41.15	-7075 41.15	-7074 41.15	-7073 28.60	-7072 10.03
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-6999 38.89	-6998 40.62	-6997 40.62	-6996 40.62	-6995 40.62	-6994 40.62	-6993 40.62	-6992 40.62
-6991 40.62	-6990 40.62	-6989 40.62	-6988 40.62	-6987 43.97	-6986 41.63	-6985 41.63	-6984 41.63
-6983 41.66	-6982 41.69	-6981 41.69	-6980 41.69	-6979 40.11	-6978 38.52	-6977 38.52	-6976 38.52
-6975 24.28	-6974 7.02	-6973 15.05	-6972 15.05	-6971 15.05	-6970 17.16	-6969 19.27	-6968 19.27
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-6666 20.07	-6665 11.37	-6664 11.37	-6663 20.07	-6662 20.07	-6661 11.37	-6660 20.07	-6659 20.07
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-6311 19.57	-6310 21.07	-6309 21.07	-6308 21.07	-6307 16.56	-6306 3.41	-6305 3.41	-6304 6.02
-6303 16.06	-6302 9.10	-6301 16.06	-6300 16.06	-6299 9.10	-6298 9.10	-6297 16.06	-6296 20.07
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-6223 23.50	-6222 20.07	-6221 20.07	-6220 20.07	-6219 20.07	-6218 20.07	-6217 20.07	-6216 20.07
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-5738 11.37	-5737 11.37	-5736 11.37	-5735 11.37	-5734 11.37	-5733 11.37	-5732 11.37	-5731 11.37
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-5520 11.37	-5519 11.37	-5518 11.37	-5517 11.37	-5516 11.37	-5515 11.37	-5514 11.37	-5513 11.37
-5512 11.37	-5511 11.37	-5510 11.37	-5509 11.37	-5508 11.37	-5507 11.37	-5506 11.37	-5505 11.37
-5504 11.37	-5503 11.37	-5502 11.37	-5501 11.37	-5500 11.37	-5499 11.37	-5498 11.37	-5497 11.37
-5496 11.37	-5495 11.37	-5494 11.37	-5493 11.37	-5492 11.37	-5491 11.37	-5490 11.37	-5489 11.37
-5488 11.37	-5487 11.37	-5486 11.37	-5485 11.37	-5484 11.37	-5483 11.37	-5482 11.37	-5481 11.37
-5480 11.37	-5479 11.37	-5478 11.37	-5477 11.37	-5476 11.37	-5475 11.37	-5474 11.37	-5473 11.37
-5472 11.37	-5471 11.37	-5470 11.37	-5469 11.37	-5468 11.37	-5467 11.37	-5466 11.37	-5465 11.37
-5464 11.37	-5463 11.37	-5462 11.37	-5461 11.37	-5460 11.37	-5459 11.37	-5458 11.37	-5457 11.37
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-5448 11.37	-5447 11.37	-5446 11.37	-5445 11.37	-5444 11.37	-5443 11.37	-5442 11.37	-5441 11.37
-5440 11.37	-5439 11.37	-5438 11.37	-5437 11.37	-5436 11.37	-5435 11.37	-5434 11.37	-5433 11.37
-5432 11.37	-5431 11.37	-5430 11.37	-5429 11.37	-5428 11.37	-5427 11.37	-5426 11.37	-5425 11.37
-5424 11.37	-5423 11.37	-5422 11.37	-5421 11.37	-5420 11.37	-5419 11.37	-5418 11.37	-5417 11.37
-5416 11.37	-5415 11.37	-5414 11.37	-5413 11.37	-5412 11.37	-5411 11.37	-5410 11.37	-5409 11.37
-5408 11.37	-5407 11.37	-5406 11.37	-5405 11.37	-5404 11.37	-5403 11.37	-5402 11.37	-5401 11.37
-5400 11.37	-5399 11.37	-5398 11.37	-5397 11.37	-5396 11.37	-5395 11.37	-5394 11.37	-5393 11.37
-5392 11.37	-5391 11.37	-5390 11.37	-5389 11.37	-5388 11.37	-5387 11.37	-5386 11.37	-5385 11.37
-5384 11.37	-5383 11.37	-5382 11.37	-5381 11.37	-5380 11.37	-5379 11.37		

Per. = Periodo
 Diff. = Minima differenza percentuale dagli altri periodi
 Φ_x = Coefficiente di partecipazione in dir. X
 Φ_y = Coefficiente di partecipazione in dir. Y
 Φ_z = Coefficiente di partecipazione in dir. Z
 %Mx = Percentuale massa partecipante in dir. X
 %My = Percentuale massa partecipante in dir. Y
 %Mz = Percentuale massa partecipante in dir. Z
 %Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φ_x	Φ_y	Φ_z	%Mx	%My	%Mz	%Jpz
1	*	0.06	25.21	185.52	24.74	0.00	66.92	1.19	0.00	0.00
2	*	0.05	9.50	-46.08	176.63	0.00	4.13	60.66	0.00	0.00
3	*	0.05	2.66	3.92	-18.82	0.00	0.03	0.69	0.00	0.00
4		0.04	2.66	2.91	9.88	0.00	0.02	0.19	0.00	0.00
5	*	0.04	3.33	22.20	73.91	0.00	0.96	10.62	0.00	0.00
6	*	0.04	4.08	16.28	38.35	0.00	0.52	2.86	0.00	0.00
7		0.04	4.08	6.39	1.05	0.00	0.08	0.00	0.00	0.00
8	*	0.04	5.34	-5.37	-23.80	0.00	0.06	1.10	0.00	0.00
9	*	0.03	10.89	-26.75	-46.85	0.00	1.39	4.27	0.00	0.00
10	*	0.03	11.59	-27.48	-7.34	0.00	1.47	0.10	0.00	0.00
11		0.02	10.46	-4.54	-1.54	0.00	0.04	0.00	0.00	0.00
12		0.02	4.03	-4.30	-6.18	0.00	0.04	0.07	0.00	0.00
13		0.02	4.03	-12.36	-0.19	0.00	0.30	0.00	0.00	0.00
14		0.02	2.36	-0.15	4.07	0.00	0.00	0.03	0.00	0.00
15		0.02	2.36	-6.21	-1.37	0.00	0.08	0.00	0.00	0.00
16		0.02	1.34	5.49	5.35	0.00	0.06	0.06	0.00	0.00
17		0.02	0.81	6.86	-3.08	0.00	0.09	0.02	0.00	0.00
18		0.02	0.81	-3.15	-0.42	0.00	0.02	0.00	0.00	0.00
19		0.02	2.55	-9.99	14.60	0.00	0.19	0.41	0.00	0.00
20	*	0.02	4.28	6.20	-25.72	0.00	0.07	1.29	0.00	0.00
21		0.01	6.78	-8.05	8.68	0.00	0.13	0.15	0.00	0.00
22		0.01	1.72	-2.57	-7.94	0.00	0.01	0.12	0.00	0.00
23	*	0.01	0.46	-12.82	-16.19	0.00	0.32	0.51	0.00	0.00
24		0.01	0.46	5.86	-14.24	0.00	0.07	0.39	0.00	0.00
25	*	0.01	0.36	-7.89	19.51	0.00	0.12	0.74	0.00	0.00
26		0.01	0.36	3.61	13.45	0.00	0.03	0.35	0.00	0.00
27	*	0.01	0.53	25.73	-2.19	0.00	1.29	0.01	0.00	0.00
28		0.01	0.71	-3.50	-2.56	0.00	0.02	0.01	0.00	0.00
29	*	0.01	0.71	22.09	4.59	0.00	0.95	0.04	0.00	0.00
30		0.01	2.22	15.40	-10.88	0.00	0.46	0.23	0.00	0.00
31		0.01	3.71	6.17	5.63	0.00	0.07	0.06	0.00	0.00
32	*	0.01	3.21	-2.82	-20.96	0.00	0.02	0.85	0.00	0.00
33		0.01	1.71	-0.05	6.09	0.00	0.00	0.07	0.00	0.00
34		0.01	0.07	6.47	6.30	0.00	0.08	0.08	0.00	0.00
35		0.01	0.07	2.29	-11.19	0.00	0.01	0.24	0.00	0.00
36		0.01	0.29	-2.51	-0.28	0.00	0.01	0.00	0.00	0.00
37		0.01	0.29	-4.53	0.48	0.00	0.04	0.00	0.00	0.00
38		0.01	0.67	-6.57	9.96	0.00	0.08	0.19	0.00	0.00
39		0.01	0.67	-2.24	4.96	0.00	0.01	0.05	0.00	0.00
40	*	0.01	0.46	5.46	22.89	0.00	0.06	1.02	0.00	0.00
41		0.01	0.46	-8.59	-7.88	0.00	0.14	0.12	0.00	0.00
42		0.01	0.27	-11.16	1.17	0.00	0.24	0.00	0.00	0.00
43	*	0.01	0.27	0.90	-33.04	0.00	0.00	2.12	0.00	0.00
44		0.01	2.60	-5.63	6.55	0.00	0.06	0.08	0.00	0.00
45		0.01	1.55	-2.13	12.33	0.00	0.01	0.30	0.00	0.00
46		0.01	0.04	-7.84	-0.03	0.00	0.12	0.00	0.00	0.00
47		0.01	0.04	-1.81	-0.60	0.00	0.01	0.00	0.00	0.00
48		0.01	0.42	1.69	-4.35	0.00	0.01	0.04	0.00	0.00
49		0.01	2.11	-8.65	-8.87	0.00	0.15	0.15	0.00	0.00
50		0.01	1.16	-14.00	7.48	0.00	0.38	0.11	0.00	0.00
51		0.01	1.16	-5.34	8.95	0.00	0.06	0.16	0.00	0.00
52		0.01	1.83	2.16	0.05	0.00	0.01	0.00	0.00	0.00
53		0.01	0.84	10.12	4.69	0.00	0.20	0.04	0.00	0.00
54		0.01	0.60	-4.01	-1.79	0.00	0.03	0.01	0.00	0.00
55		0.01	0.60	-0.19	-1.14	0.00	0.00	0.00	0.00	0.00
56		0.01	0.02	-9.95	-2.39	0.00	0.19	0.01	0.00	0.00
57		0.01	0.02	4.07	2.64	0.00	0.03	0.01	0.00	0.00
58		0.01	0.30	14.36	2.39	0.00	0.40	0.01	0.00	0.00
59		0.01	0.61	6.57	0.46	0.00	0.08	0.00	0.00	0.00
60		0.01	0.61	5.58	0.79	0.00	0.06	0.00	0.00	0.00
61	*	0.01	1.44	34.92	2.11	0.00	2.37	0.01	0.00	0.00
62		0.01	1.20	-9.04	0.57	0.00	0.16	0.00	0.00	0.00
63	*	0.01	1.20	37.63	-0.49	0.00	2.75	0.00	0.00	0.00
64	*	0.01	1.20	45.38	-1.23	0.00	4.00	0.00	0.00	0.00
65		0.01	1.20	0.66	-0.39	0.00	0.00	0.00	0.00	0.00
66	*	0.01	1.86	-17.62	1.47	0.00	0.60	0.00	0.00	0.00
67		0.01	0.20	2.29	0.64	0.00	0.01	0.00	0.00	0.00
68	*	0.01	0.20	-16.09	-7.20	0.00	0.50	0.10	0.00	0.00
69		0.01	1.15	7.34	-1.15	0.00	0.10	0.00	0.00	0.00
70		0.01	0.40	5.93	-5.05	0.00	0.07	0.05	0.00	0.00
71		0.01	0.40	-8.73	5.11	0.00	0.15	0.05	0.00	0.00
72	*	0.01	0.47	21.40	-3.76	0.00	0.89	0.03	0.00	0.00
73		0.01	0.47	1.78	15.43	0.00	0.01	0.46	0.00	0.00
74		0.01	0.63	-1.81	1.34	0.00	0.01	0.00	0.00	0.00
75	*	0.01	0.63	2.18	16.22	0.00	0.01	0.51	0.00	0.00
76		0.01	0.86	5.81	-6.43	0.00	0.07	0.08	0.00	0.00
77		0.01	0.24	-11.26	2.08	0.00	0.25	0.01	0.00	0.00
78		0.01	0.14	-0.60	8.89	0.00	0.00	0.15	0.00	0.00
79	*	0.01	0.14	-1.05	19.68	0.00	0.00	0.75	0.00	0.00
80		0.01	0.26	-4.67	1.89	0.00	0.04	0.01	0.00	0.00
81		0.01	0.26	-6.14	-5.50	0.00	0.07	0.06	0.00	0.00
82		0.01	0.61	9.82	-4.79	0.00	0.19	0.04	0.00	0.00
83		0.01	0.61	4.83	6.65	0.00	0.05	0.09	0.00	0.00
84		0.01	1.16	-2.81	3.04	0.00	0.02	0.02	0.00	0.00
85		0.01	0.34	1.56	-4.24	0.00	0.00	0.03	0.00	0.00
86		0.01	0.34	3.27	4.45	0.00	0.02	0.04	0.00	0.00

87	0.01	0.43	1.02	3.50	0.00	0.00	0.02	0.00	0.00
88	0.01	0.17	-4.36	4.11	0.00	0.04	0.03	0.00	0.00
89	0.01	0.17	0.66	1.07	0.00	0.00	0.00	0.00	0.00
90	0.01	0.99	-1.42	-1.21	0.00	0.00	0.00	0.00	0.00
91	0.01	0.99	-4.09	0.17	0.00	0.03	0.00	0.00	0.00
92	0.01	0.40	-8.51	3.89	0.00	0.14	0.03	0.00	0.00
93	0.01	0.40	-2.14	-2.34	0.00	0.01	0.01	0.00	0.00
94	0.01	0.03	6.22	1.54	0.00	0.08	0.00	0.00	0.00
95	0.01	0.03	-8.21	-5.86	0.00	0.13	0.07	0.00	0.00
96	0.01	0.51	4.06	8.93	0.00	0.03	0.15	0.00	0.00
97	0.01	0.22	-3.86	2.13	0.00	0.03	0.01	0.00	0.00
98	0.01	0.22	4.67	-0.37	0.00	0.04	0.00	0.00	0.00
99	0.01	0.48	4.17	2.26	0.00	0.03	0.01	0.00	0.00
100	0.01	0.48	1.10	0.43	0.00	0.00	0.00	0.00	0.00
101	0.01	1.09	2.15	7.93	0.00	0.01	0.12	0.00	0.00
102	0.00	0.56	2.33	-2.19	0.00	0.01	0.01	0.00	0.00
103	0.00	0.23	-1.74	2.31	0.00	0.01	0.01	0.00	0.00
104	0.00	0.23	2.90	2.96	0.00	0.02	0.02	0.00	0.00
105	0.00	0.17	-5.60	0.47	0.00	0.06	0.00	0.00	0.00
106	0.00	0.17	2.57	2.37	0.00	0.01	0.01	0.00	0.00
107	0.00	0.38	3.56	5.13	0.00	0.02	0.05	0.00	0.00
108	0.00	0.33	-2.35	3.22	0.00	0.01	0.02	0.00	0.00
109	0.00	0.33	-0.96	0.24	0.00	0.00	0.00	0.00	0.00
110	0.00	0.18	-0.31	0.41	0.00	0.00	0.00	0.00	0.00
111	0.00	0.18	-1.78	-0.61	0.00	0.01	0.00	0.00	0.00
112	0.00	0.21	1.04	1.21	0.00	0.00	0.00	0.00	0.00
113	0.00	0.21	0.45	-2.46	0.00	0.00	0.01	0.00	0.00
114	0.00	0.39	-3.19	2.65	0.00	0.02	0.01	0.00	0.00
115	0.00	0.39	0.59	-0.74	0.00	0.00	0.00	0.00	0.00
116	0.00	0.28	0.15	0.41	0.00	0.00	0.00	0.00	0.00
117	0.00	0.28	-3.11	5.62	0.00	0.02	0.06	0.00	0.00
118	0.00	0.20	0.74	0.52	0.00	0.00	0.00	0.00	0.00
119	0.00	0.20	2.65	0.33	0.00	0.01	0.00	0.00	0.00
120	0.00	0.05	3.87	-2.19	0.00	0.03	0.01	0.00	0.00
121	0.00	0.05	-0.01	1.73	0.00	0.00	0.01	0.00	0.00
122	0.00	0.39	-0.82	1.39	0.00	0.00	0.00	0.00	0.00
123	0.00	0.39	0.36	-1.53	0.00	0.00	0.00	0.00	0.00
124	0.00	0.37	0.29	-7.34	0.00	0.00	0.10	0.00	0.00
125	0.00	0.27	-2.11	-4.23	0.00	0.01	0.03	0.00	0.00
126	0.00	0.27	4.78	0.36	0.00	0.04	0.00	0.00	0.00
127	0.00	0.29	-4.39	-0.60	0.00	0.04	0.00	0.00	0.00
128	0.00	0.98	2.37	1.82	0.00	0.01	0.01	0.00	0.00
129	0.00	0.46	-1.53	3.43	0.00	0.00	0.02	0.00	0.00
130	0.00	0.46	-0.64	0.74	0.00	0.00	0.00	0.00	0.00
131	0.00	0.65	-0.51	-0.46	0.00	0.00	0.00	0.00	0.00
132	0.00	0.65	-3.26	-2.48	0.00	0.02	0.01	0.00	0.00
133	0.00	0.47	-1.53	1.69	0.00	0.00	0.01	0.00	0.00
134	0.00	0.47	0.49	-9.18	0.00	0.00	0.16	0.00	0.00
135	0.00	0.01	-0.26	3.95	0.00	0.00	0.03	0.00	0.00
136	0.00	0.01	0.46	-2.07	0.00	0.00	0.01	0.00	0.00
137	0.00	0.66	4.52	5.17	0.00	0.04	0.05	0.00	0.00
138	0.00	0.66	-0.59	-3.57	0.00	0.00	0.02	0.00	0.00
139	0.00	0.37	-4.28	3.22	0.00	0.04	0.02	0.00	0.00
140	0.00	0.37	-1.35	3.22	0.00	0.00	0.02	0.00	0.00
141	0.00	0.58	3.03	3.65	0.00	0.02	0.03	0.00	0.00
142	0.00	0.55	-2.19	0.93	0.00	0.01	0.00	0.00	0.00
143	0.00	0.17	1.78	-0.52	0.00	0.01	0.00	0.00	0.00
144	0.00	0.17	-2.26	0.66	0.00	0.01	0.00	0.00	0.00
145	0.00	0.21	0.25	-1.55	0.00	0.00	0.00	0.00	0.00
146	0.00	0.21	0.12	8.01	0.00	0.00	0.12	0.00	0.00
147	0.00	0.06	0.01	-0.03	0.00	0.00	0.00	0.00	0.00
148	0.00	0.02	0.21	7.45	0.00	0.00	0.11	0.00	0.00
149	0.00	0.02	0.10	8.81	0.00	0.00	0.15	0.00	0.00
150	*	0.00	0.08	0.36	-16.25	0.00	0.00	0.51	0.00
151	0.00	0.30	0.20	-2.84	0.00	0.00	0.02	0.00	0.00
152	0.00	0.30	-1.20	-3.55	0.00	0.00	0.02	0.00	0.00
153	0.00	0.77	-0.65	-0.15	0.00	0.00	0.00	0.00	0.00
154	0.00	0.77	-1.72	2.19	0.00	0.01	0.01	0.00	0.00
155	0.00	0.40	6.12	-1.87	0.00	0.07	0.01	0.00	0.00
156	0.00	0.28	-2.09	-5.88	0.00	0.01	0.07	0.00	0.00
157	0.00	0.28	2.70	-3.47	0.00	0.01	0.02	0.00	0.00
158	0.00	0.33	-0.95	-3.49	0.00	0.00	0.02	0.00	0.00
159	0.00	0.62	3.52	2.38	0.00	0.02	0.01	0.00	0.00
160	0.00	0.20	1.58	3.73	0.00	0.00	0.03	0.00	0.00
161	0.00	0.18	-1.34	2.14	0.00	0.00	0.01	0.00	0.00
162	0.00	0.18	-0.94	-1.24	0.00	0.00	0.00	0.00	0.00
163	0.00	0.27	-0.85	-1.37	0.00	0.00	0.00	0.00	0.00
164	0.00	0.32	-1.25	1.98	0.00	0.00	0.01	0.00	0.00
165	0.00	0.32	2.34	-2.14	0.00	0.01	0.01	0.00	0.00
166	0.00	0.20	-2.32	1.40	0.00	0.01	0.00	0.00	0.00
167	0.00	0.08	2.26	-1.96	0.00	0.01	0.01	0.00	0.00
168	0.00	0.08	-0.30	-0.51	0.00	0.00	0.00	0.00	0.00
169	0.00	0.27	-0.50	-0.17	0.00	0.00	0.00	0.00	0.00
170	0.00	0.24	-0.73	-0.61	0.00	0.00	0.00	0.00	0.00
171	0.00	0.23	-1.57	1.70	0.00	0.00	0.01	0.00	0.00
172	0.00	0.11	-0.64	0.72	0.00	0.00	0.00	0.00	0.00
173	0.00	0.11	-1.34	1.37	0.00	0.00	0.00	0.00	0.00
174	0.00	0.14	2.02	-2.09	0.00	0.01	0.01	0.00	0.00
175	0.00	0.43	-1.26	1.49	0.00	0.00	0.00	0.00	0.00
176	0.00	0.39	-2.54	-1.04	0.00	0.01	0.00	0.00	0.00
177	0.00	0.39	-4.58	-1.29	0.00	0.04	0.00	0.00	0.00
178	0.00	0.37	0.42	0.94	0.00	0.00	0.00	0.00	0.00
179	0.00	0.20	0.79	2.01	0.00	0.00	0.01	0.00	0.00
180	0.00	0.20	0.90	-3.86	0.00	0.00	0.03	0.00	0.00
181	0.00	0.23	-1.98	-0.81	0.00	0.01	0.00	0.00	0.00
182	0.00	0.22	-0.04	3.29	0.00	0.00	0.02	0.00	0.00
183	0.00	0.22	-4.12	-1.82	0.00	0.03	0.01	0.00	0.00
184	0.00	0.45	3.29	0.66	0.00	0.02	0.00	0.00	0.00

185	0,00	0,21	2,09	0,68	0,00	0,01	0,00	0,00	0,00
186	0,00	0,21	-2,07	0,39	0,00	0,01	0,00	0,00	0,00
187	0,00	0,31	2,54	-1,43	0,00	0,01	0,00	0,00	0,00
188	0,00	0,31	-0,11	2,11	0,00	0,00	0,01	0,00	0,00
189	0,00	0,21	5,48	1,34	0,00	0,06	0,00	0,00	0,00
190	0,00	0,21	-1,38	0,36	0,00	0,00	0,00	0,00	0,00
191	0,00	0,23	-1,30	-4,69	0,00	0,00	0,04	0,00	0,00
192	0,00	0,27	1,32	-6,35	0,00	0,00	0,08	0,00	0,00
193	0,00	0,07	-2,91	-2,70	0,00	0,02	0,01	0,00	0,00
194	0,00	0,07	-5,99	1,42	0,00	0,07	0,00	0,00	0,00
195	0,00	0,36	4,24	3,73	0,00	0,03	0,03	0,00	0,00
196	0,00	0,36	-4,53	2,37	0,00	0,04	0,01	0,00	0,00
197	0,00	0,37	-3,37	3,53	0,00	0,02	0,02	0,00	0,00
198	0,00	0,05	-1,56	4,90	0,00	0,00	0,05	0,00	0,00
199	0,00	0,05	-0,13	-1,30	0,00	0,00	0,00	0,00	0,00
200	0,00	0,10	-0,27	2,59	0,00	0,00	0,01	0,00	0,00
201	0,00	0,02	3,57	-0,98	0,00	0,02	0,00	0,00	0,00
202	0,00	0,02	-3,29	3,68	0,00	0,02	0,03	0,00	0,00
203	0,00	0,17	-1,62	-1,25	0,00	0,01	0,00	0,00	0,00
204	0,00	0,20	3,13	3,73	0,00	0,02	0,03	0,00	0,00
205	0,00	0,27	2,58	-0,17	0,00	0,01	0,00	0,00	0,00
206	0,00	0,27	3,42	0,33	0,00	0,02	0,00	0,00	0,00
207	0,00	0,02	-2,08	-4,64	0,00	0,01	0,04	0,00	0,00
208	0,00	0,02	0,58	-1,24	0,00	0,00	0,00	0,00	0,00
209	0,00	0,03	-2,29	-1,90	0,00	0,01	0,01	0,00	0,00
210	0,00	0,03	0,18	-0,18	0,00	0,00	0,00	0,00	0,00
211	0,00	0,55	1,02	-0,26	0,00	0,00	0,00	0,00	0,00
212	0,00	0,21	-1,43	2,22	0,00	0,00	0,01	0,00	0,00
213	0,00	0,21	-0,48	-0,58	0,00	0,00	0,00	0,00	0,00
214	0,00	0,08	2,93	2,91	0,00	0,02	0,02	0,00	0,00
215	0,00	0,08	-1,90	1,67	0,00	0,01	0,01	0,00	0,00
216	0,00	0,62	-1,57	-0,04	0,00	0,00	0,00	0,00	0,00
217	0,00	0,39	1,69	-2,64	0,00	0,01	0,01	0,00	0,00
218	0,00	0,39	2,62	0,13	0,00	0,01	0,00	0,00	0,00
219	0,00	0,41	3,25	0,06	0,00	0,02	0,00	0,00	0,00
220	0,00	0,35	-3,40	-0,52	0,00	0,02	0,00	0,00	0,00
221	0,00	0,35	-0,09	-2,64	0,00	0,00	0,01	0,00	0,00
222	0,00	0,40	-1,17	0,16	0,00	0,00	0,00	0,00	0,00
223	0,00	0,18	-3,34	0,29	0,00	0,02	0,00	0,00	0,00
224	0,00	0,18	-1,93	-3,71	0,00	0,01	0,03	0,00	0,00
225	0,00	0,36	-3,08	0,80	0,00	0,02	0,00	0,00	0,00
226	0,00	0,46	-0,51	0,46	0,00	0,00	0,00	0,00	0,00
227	0,00	0,39	-0,04	-0,64	0,00	0,00	0,00	0,00	0,00
228	0,00	0,11	-3,04	-1,25	0,00	0,02	0,00	0,00	0,00
229	0,00	0,11	-5,73	0,61	0,00	0,06	0,00	0,00	0,00
230	0,00	0,16	0,75	-0,39	0,00	0,00	0,00	0,00	0,00
231	0,00	0,32	0,73	-0,74	0,00	0,00	0,00	0,00	0,00
232	0,00	0,02	5,21	-1,17	0,00	0,05	0,00	0,00	0,00
233	0,00	0,02	-2,82	2,85	0,00	0,02	0,02	0,00	0,00
234	0,00	0,11	1,07	-2,21	0,00	0,00	0,01	0,00	0,00
235	0,00	0,11	2,19	1,53	0,00	0,01	0,00	0,00	0,00
236	0,00	0,15	2,54	-0,58	0,00	0,01	0,00	0,00	0,00
237	0,00	0,15	-1,31	1,46	0,00	0,00	0,00	0,00	0,00
238	0,00	0,15	1,10	0,44	0,00	0,00	0,00	0,00	0,00
239	0,00	0,15	-1,13	-1,61	0,00	0,00	0,01	0,00	0,00
240	0,00	0,24	-0,10	-1,08	0,00	0,00	0,00	0,00	0,00

Tot.cons.

89.43 90.00 0.00 0.00

Elenco coefficienti di risposta**Simbologia**

Modo = Numero del modo di vibrare

Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X

Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di operatività

Modo	Sx	Sy
1	13.20	13.20
2	12.10	12.10
3	11.72	11.72
4	11.62	11.62
5	11.50	11.50
6	11.31	11.31
7	11.17	11.17
8	11.00	11.00
9	10.68	10.68
10	10.37	10.37
11	9.83	9.83
12	9.63	9.63
13	9.56	9.56
14	9.48	9.48
15	9.44	9.44
16	9.39	9.39
17	9.37	9.37
18	9.35	9.35
19	9.31	9.31
20	9.25	9.25
21	9.04	9.04
22	8.96	8.96
23	8.94	8.94
24	8.94	8.94
25	8.93	8.93

26	8.92	8.92
27	8.92	8.92
28	8.83	8.83
29	8.82	8.82
30	8.80	8.80
31	8.76	8.76
32	8.72	8.72
33	8.69	8.69
34	8.67	8.67
35	8.67	8.67
36	8.67	8.67
37	8.67	8.67
38	8.66	8.66
39	8.65	8.65
40	8.64	8.64
41	8.64	8.64
42	8.63	8.63
43	8.63	8.63
44	8.61	8.61
45	8.57	8.57
46	8.55	8.55
47	8.55	8.55
48	8.55	8.55
49	8.53	8.53
50	8.48	8.48
51	8.47	8.47
52	8.46	8.46
53	8.44	8.44
54	8.43	8.43
55	8.43	8.43

56	8.42	8.42
57	8.42	8.42
58	8.42	8.42
59	8.41	8.41
60	8.41	8.41
61	8.40	8.40
62	8.39	8.39
63	8.38	8.38
64	8.37	8.37
65	8.36	8.36
66	8.35	8.35
67	8.33	8.33
68	8.33	8.33
69	8.33	8.33
70	8.31	8.31
71	8.31	8.31
72	8.30	8.30
73	8.30	8.30
74	8.29	8.29
75	8.29	8.29
76	8.28	8.28
77	8.28	8.28
78	8.28	8.28
79	8.28	8.28
80	8.27	8.27
81	8.27	8.27
82	8.26	8.26
83	8.26	8.26
84	8.25	8.25
85	8.25	8.25

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Stato limite di danno

Modo Sx	Sy
1	15.45 15.45
2	14.18 14.18
3	13.74 13.74
4	13.63 13.63
5	13.48 13.48
6	13.27 13.27
7	13.11 13.11
8	12.91 12.91
9	12.54 12.54
10	12.19 12.19
11	11.56 11.56
12	11.33 11.33
13	11.25 11.25
14	11.16 11.16
15	11.11 11.11
16	11.05 11.05
17	11.03 11.03
18	11.01 11.01
19	10.97 10.97
20	10.89 10.89
21	10.65 10.65
22	10.56 10.56
23	10.54 10.54
24	10.53 10.53
25	10.52 10.52
26	10.52 10.52
27	10.51 10.51
28	10.40 10.40
29	10.39 10.39
30	10.37 10.37
31	10.32 10.32
32	10.28 10.28
33	10.25 10.25
34	10.23 10.23
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Stato limite di salvaguardia della vita

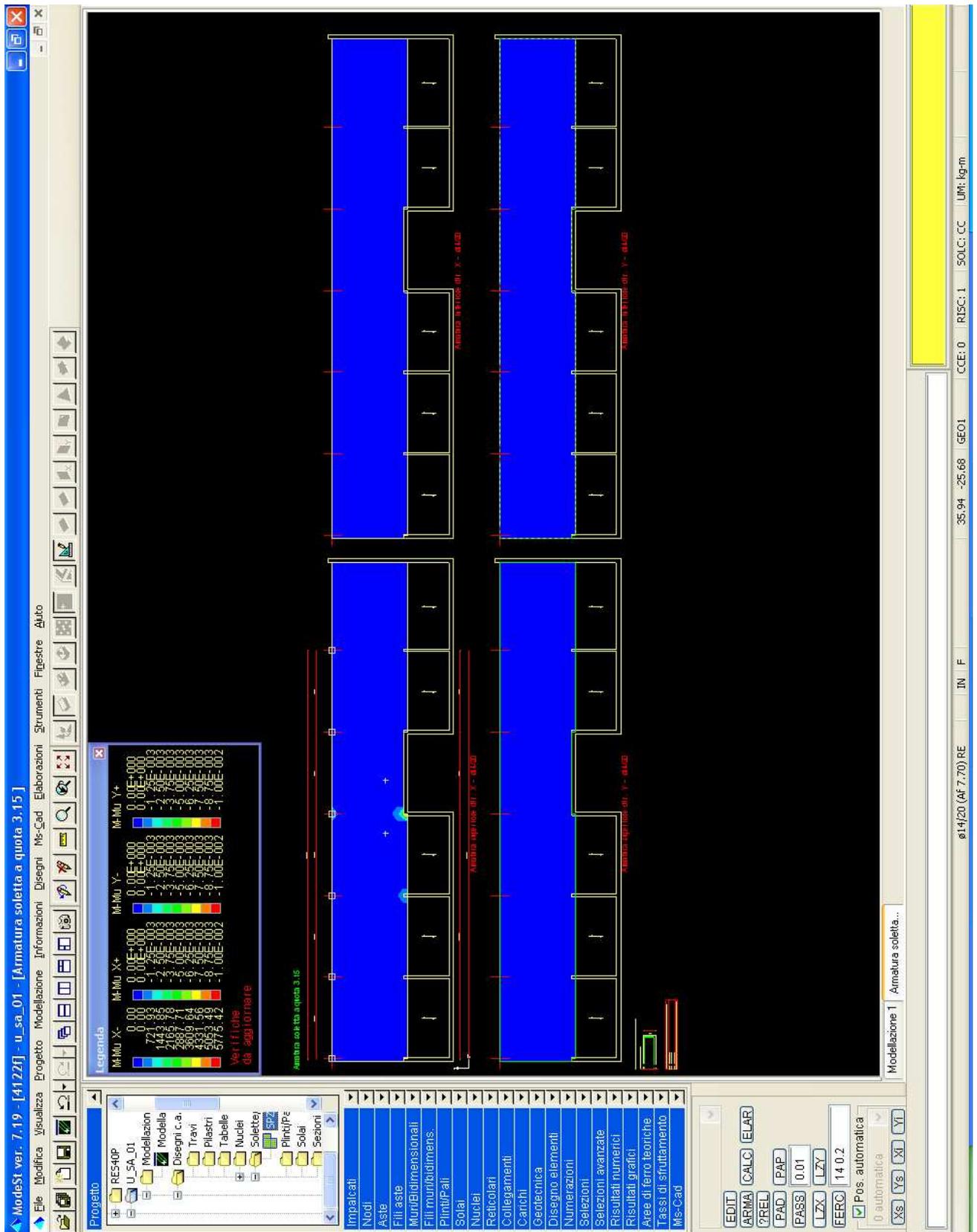
Modo Sx Sy

1 26.65 26.65
 2 25.62 25.62
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184	21.84	21.84	203	21.82	21.82	222	21.80	21.80
185	21.84	21.84	204	21.82	21.82	223	21.80	21.80
186	21.84	21.84	205	21.82	21.82	224	21.80	21.80
187	21.83	21.83	206	21.82	21.82	225	21.80	21.80
188	21.83	21.83	207	21.82	21.82	226	21.80	21.80
189	21.83	21.83	208	21.82	21.82	227	21.80	21.80
190	21.83	21.83	209	21.82	21.82	228	21.80	21.80
191	21.83	21.83	210	21.82	21.82	229	21.80	21.80
192	21.83	21.83	211	21.81	21.81	230	21.80	21.80
193	21.83	21.83	212	21.81	21.81	231	21.79	21.79
194	21.83	21.83	213	21.81	21.81	232	21.79	21.79
195	21.83	21.83	214	21.81	21.81	233	21.79	21.79
196	21.83	21.83	215	21.81	21.81	234	21.79	21.79
197	21.82	21.82	216	21.81	21.81	235	21.79	21.79
198	21.82	21.82	217	21.81	21.81	236	21.79	21.79
199	21.82	21.82	218	21.81	21.81	237	21.79	21.79
200	21.82	21.82	219	21.80	21.80	238	21.79	21.79
201	21.82	21.82	220	21.80	21.80	239	21.79	21.79
202	21.82	21.82	221	21.80	21.80	240	21.79	21.79

3.2. MAPPE D'ARMATURA SOLETTA SUPERIORE BLOCCO A



ModeSt ver. 7.19 [4122] - u_sa_01 - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto Impalcati Nodi Aste Fili aste Muribidimensionali Fili muribidimens. Plinti/Pali Soletti Nuclei Reticolari Collegamenti Carichi Geotecnica Disegno elementi Numerazioni Selezioni avanzate Risultati numerici Risultati grafici Aree di ferro teoriche Tassi di sfruttamento Ms-Cad

Legenda

ATXS	ATXI	ATYs	ATYI
0,00	0,00	0,00	0,00
3,72	2,22	2,06	2,07
7,44	4,44	4,13	4,14
11,07	6,66	6,20	6,21
14,70	8,88	8,26	8,27
18,33	11,11	10,33	10,34
21,96	13,33	12,39	12,41
25,59	15,56	14,45	14,48
29,22	17,78	16,52	16,55

Verifiche da aggiornare

Armatura soletta a quota 3.15

Armatura soletta dir. X - at10

Armatura soletta dir. Y - at10

Armatura soletta dir. X - at10

Armatura soletta dir. Y - at10

Modellazione 1 Armatura soletta...

[SELE] - Attendevvo una selezione di entità grafiche

EDIT ARMA CALC ELAR
 ?REL
 PAD PAP
 PASS 0.01
 LZX LZZ
 FEREC 14.0.2
 Pos. automatica
 automatica
 XS YS XI YI
 TZRE TZCP TZCF
 AAZ AGGZ ELIZ
 UNIP ASSX
 DAFB
 XS XI YS YI
 DX DX+ DY DY+
 DX DY
 DPUN LPV DAD

914/20 (At 7.70) RE IN F 52.93 -24.76 GEO1 CCE:0 RISC:1 SOLC:CC UM: kg-m

ModeSt ver. 7.19 [4122] - u_sa_01 - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto Impalcati Nodi Aste Fili aste Mur/Bidimensionali Fili mur/bidimens. Solai Nuclei Reticolari Collegamenti Carichi Geotecnica Disegno elementi Numerazioni Selezioni avanzate Risultati numerici Risultati grafici Aree di ferro teoriche Tassi di sfruttamento Ms-Cad

Legend

ATXs	ATXl	ATXs	ATXl
0.00	0.00	0.00	0.00
3.72	2.22	2.22	2.07
7.44	4.44	4.44	4.14
11.07	6.66	6.66	6.21
14.70	8.88	8.88	8.28
18.33	11.11	11.11	10.35
21.96	13.33	13.33	12.41
25.59	15.56	15.56	14.48
29.22	17.78	17.78	16.55

Verifiche da aggiornare

Armatura soletta a quota 3.15

Armatura soletta dir. X - Ø50

Armatura soletta dir. Y - Ø40

Armatura soletta dir. Z - Ø50

Armatura soletta dir. X - Ø50

Armatura soletta dir. Y - Ø40

Armatura soletta dir. Z - Ø50

Modellazione 1 Armatura soletta...

AAZ - Il punto indicato non individua una zona
Selezionare la zona

Selezionare la zona di armatura (diffusa o concentrata) alla quale assegnare l'armatura corrente

CCE: 0 RISC: 1 SOLC: CC UM: kg-m AAZ

36.00 -30.07 GEO1

Ø18/20 (AF 12.72) RE IN F

EDIT ARMA CALC ELAR
PREL
PAD PAP
PASS 0.01
LZX LZ
FERC 18.0.2
 Pos. automatica
 automatica
XS YS XI YI
TZRE TZCP TZCF
AAZ AGGZ ELIZ
UNIP ASSX
- DAFB
XS XI YS YI
DX DX+ DY DY+
DX DY
DPUN LDPV DAD

ModeSt ver. 7.19 - [4122] - u_sa_01 - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto Impalcati Nodi Aste Fili aste Muribidimensionali Fili muribidimens. Plinti/Pali Soletti Nuclei Rettilinei Collegamenti Carichi Geotecnica Disegno elementi Numerazioni Selezioni avanzate Risultati numerici Risultati grafici Aree di ferro teoriche Tassi di sfruttamento Ms-Cad

Legenda

ATXs	ATXl	ATXs	ATXl
0.00	0.00	0.00	0.00
3.72	2.22	2.06	2.07
7.44	4.44	4.13	4.14
11.07	6.66	6.19	6.21
14.70	8.89	8.26	8.28
18.33	11.11	10.33	10.37
21.96	13.33	12.40	12.47
25.59	15.55	14.47	14.58
29.22	17.78	16.54	16.55

Verifiche da aggiornare

Armatura soletta a quota 3.15

Armatura soletta dir. X - Ø50

Armatura soletta dir. Y - Ø50

Armatura soletta dir. Z - Ø50

Armatura soletta dir. X - Ø50

Armatura soletta dir. Y - Ø50

Armatura soletta dir. Z - Ø50

EDIT ARMA CALC ELAR ?REL PAD PAP PASS 0.01 LZL LZV FEREC 18.0.2 Pos. automatica automatica XS YS XI YI TZRE TZCP TZCF AAZ AGGZ ELIZ UNIP ASSX DAFB XS XI YS YI DX DX+ DY DY+ DX DY DPUN LPV DAD

Modellazione 1 Armatura soletta...

Selezionare la zona

Selezionare la zona di armatura (diffusa o concentrata) alla quale assegnare l'armatura corrente

CCE: 0 RISC: 1 SOLC: CC UM: kg-m AAZ

Ø18/20 (Af.12.72) RE IN F 33.89 -28.44 GEO1

ModeSt ver. 7.19 [4122] - u_sa_01 - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Legenda

ATXs	ATXl	ATXs	ATXl
0,00	0,00	0,00	0,00
0,00	2,72	0,00	2,07
3,72	4,44	2,06	4,13
7,44	8,06	4,13	6,21
11,17	11,69	6,21	8,29
14,90	15,31	8,29	10,36
18,63	18,94	10,36	12,44
22,35	22,57	12,44	14,51
26,08	26,20	14,51	16,59
29,78	29,83	16,59	18,66

Verifiche
non soddisfatte

Armatura soletta a quota 3.15

Progetto Impalcati Nodi Aste Fili aste Muri/Dimensionali Fili muribidimens. Pilastri/Pali Soletti Nuclei Rettilinei Collegamenti Carichi Geotecnica Disegno elementi Numerazioni Selezioni avanzate Risultati numerici Risultati grafici Area di ferro teoriche Tassi di sfruttamento Ms-Cad

SNAP 10 FINE INTE CENT VICI GRID 1 ORTO PERP LC SL LINE LCERC QUOT TEST CANG CORI SPOS TAGL SPEZI RACC STIR ESTE OFFS GAMB ESPL BLOC SELE ESSEL INSE

Report complessivi EDIT ARMA CALC ELAR ?REL ?PAD ?PAP PASS 0.01 LZX LZY EERC 18.01

Pos. automatica in automatica

Modellazione 1 Armatura soletta...

CCE: 0 RISC: 1 SOLC: CC UM: kg-m
 GEO1 28,94 -27,45
 ø18/10 (AF 25.45) RE IN F

4. MODELLAZIONE C

4.1. FATTORE DI STRUTTURA

Si assume un fattore di struttura $q=1.5$, valore assunto come minimo che non richiede adeguate giustificazioni da parte del progettista; paragrafo 7.4.3.2 DM08.

4.2. PARAMETRI DI CALCOLO SCALE IN CA

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con: ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti: Xfinest ver. 8.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08

Tipo di calcolo: analisi sismica dinamica

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <kg/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: ISOSHELL
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per Buckling: No
- Trascura Buckling torsionale: No

Dati struttura

- Zona sismica: zona 3
- Sito di costruzione: LON. 11.18250 LAT. 43.75800
- Contenuto tra ID reticolo: 20058 20057 20280 20279

simbologia

TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 Ag = Accelerazione orizzontale massima al sito
 FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

TCC	Ag	FO	TC*
SLO	0.4462	2.57	0.25
SLD	0.5363	2.60	0.26
SLV	1.2629	2.39	0.30

- Tipo di opera: Opera ordinaria
- Vita nominale V_N : 50.00
- Classe d'uso: classe II
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 41.96 <m>
- Numero piani edificio: 0
- Coefficiente θ : 0
- Edificio regolare in altezza: no
- Edificio regolare in pianta: no
- Forze orizzontali convenzionali per stati limite non sismici: no

Dati di calcolo

- Categoria del suolo di fondazione: C

Coeff. C_1 0.075
 Fattore di struttura (q) 1.50

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica: 1.00
- Modi da calcolare: 180
- Modi da considerare: con singola massa superiore a 1.00%
- Smorzamento spettro: 5.00

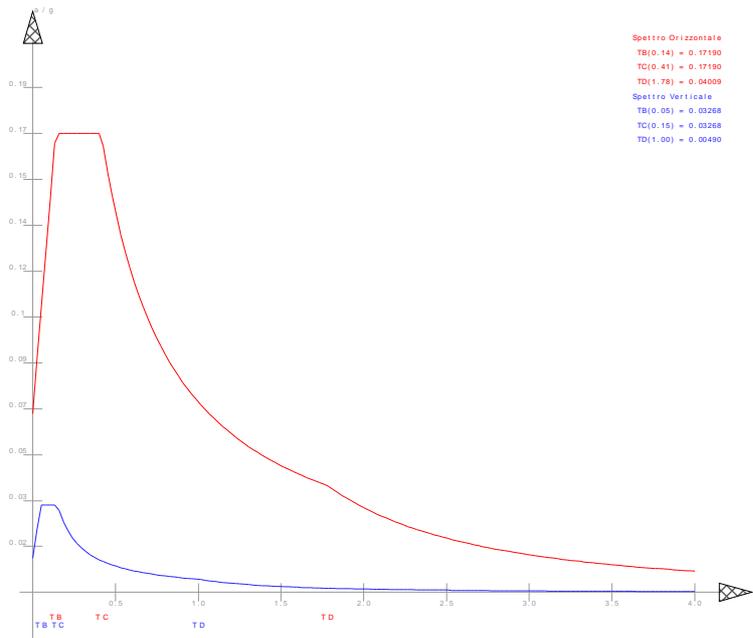


Figura numero 1: Spettro allo SLO

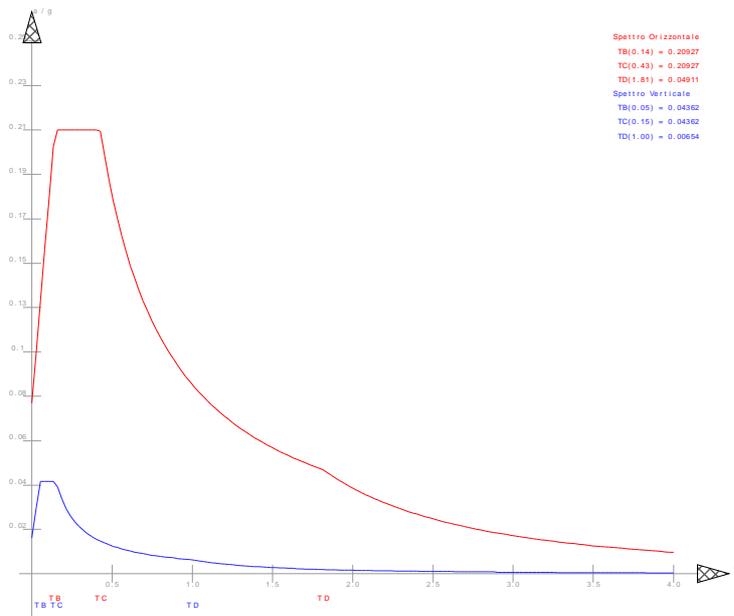


Figura numero 2: Spettro allo SLD

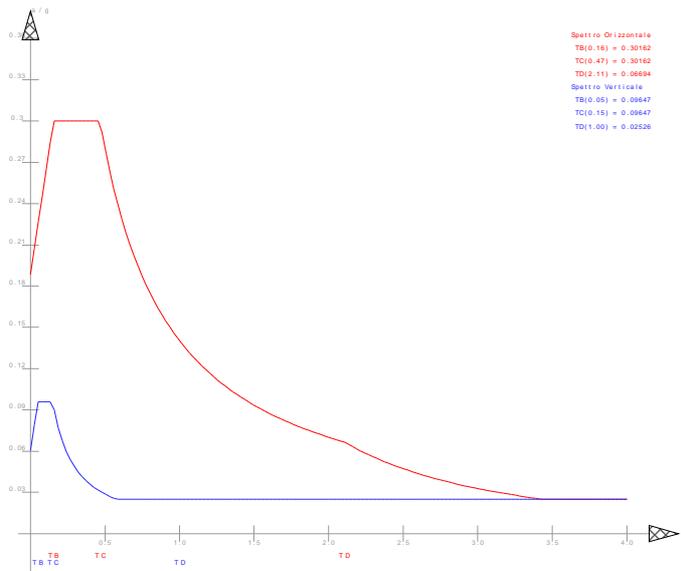


Figura numero 3: Spettro allo SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Condizioni di carico elementari

Simbologia

- CCE = Numero della condizione di carico elementare
- Comm. = Commento
- s = Coeff. di riduzione
- Mx = Moltiplicatore della massa in dir. X
- My = Moltiplicatore della massa in dir. Y
- Mz = Moltiplicatore della massa in dir. Z
- Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
- Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
- Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	s	Mx	My	Mz	Jpx	Jpy	Jpz
1	pp e perm	1.00	1.00	1.00	0.00	0.00	0.00	1.00
2	tamponamenti	1.00	1.00	1.00	0.00	0.00	0.00	1.00
3	permanente solette	1.00	1.00	1.00	0.00	0.00	0.00	1.00
4	carrabile	1.00	1.00	1.00	0.00	0.00	0.00	1.00
5	copertura (5 6 9)	1.00	1.00	1.00	0.00	0.00	0.00	1.00
6	scale (1 7 8)	1.00	1.00	1.00	0.00	0.00	0.00	1.00
7	permanenti non strutturali solai	1.00	1.00	1.00	0.00	0.00	0.00	1.00
8	grigliati esterni (10)	1.00	1.00	1.00	0.00	0.00	0.00	1.00
9	spinta della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
10	spinta accidentale della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
11	variazione termica uniforme	1.00	0.00	0.00	0.00	0.00	0.00	0.00
12	vento	1.00	0.00	0.00	0.00	0.00	0.00	0.00
13	Sisma dir. X - SLO	--	--	--	--	--	--	--
14	Sisma dir. Y - SLO	--	--	--	--	--	--	--
15	Sisma dir. X - SLD	--	--	--	--	--	--	--
16	Sisma dir. Y - SLD	--	--	--	--	--	--	--
17	Sisma dir. X - SLV	--	--	--	--	--	--	--
18	Sisma dir. Y - SLV	--	--	--	--	--	--	--

Combinazioni delle cce

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
 - SLU = Stato limite ultimo
 - SLU S = Stato limite ultimo (azione sismica)
 - SLE R = Stato limite d'esercizio, combinazione rara
 - SLE F = Stato limite d'esercizio, combinazione frequente
 - SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 - SLD = Stato limite di danno
 - SLV = Stato limite di salvaguardia della vita
 - SLC = Stato limite di prevenzione del collasso
 - SLO = Stato limite di operatività
- An. = Tipo di analisi
 - L = Lineare
 - NL = Non lineare
- Bk = Buckling
 - S = Si

194 CC 194 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.15	0.20	0.70	1.00	0.15	1.00	0.17	0.00	0.00	0.00	0.00
195 CC 195 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.17	0.00	0.70	1.00	0.15	1.00	0.17	0.00	0.00	0.00	0.00
196 CC 196 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.15	0.00	0.70	1.00	0.15	1.00	0.17	0.00	0.00	0.00	0.00
197 CC 197 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.17	0.20	0.70	1.00	0.17	1.00	0.15	0.00	0.00	0.00	0.00
198 CC 198 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.15	0.20	0.70	1.00	0.17	1.00	0.15	0.00	0.00	0.00	0.00
199 CC 199 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.17	0.00	0.70	1.00	0.17	1.00	0.15	0.00	0.00	0.00	0.00
200 CC 200 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.15	0.00	0.70	1.00	0.17	1.00	0.15	0.00	0.00	0.00	0.00
201 CC 201 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.17	0.20	0.70	1.00	0.15	1.00	0.15	0.00	0.00	0.00	0.00
202 CC 202 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.15	0.20	0.70	1.00	0.15	1.00	0.15	0.00	0.00	0.00	0.00
203 CC 203 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.17	0.00	0.70	1.00	0.15	1.00	0.15	0.00	0.00	0.00	0.00
204 CC 204 - Amb. 2 (SLE F)	SLE F L N	1.00	1.00	1.00	0.15	0.00	0.70	1.00	0.15	1.00	0.15	0.00	0.00	0.00	0.00
205 CC 205 - Amb. 2 (SLE Q)	SLE Q L N	1.00	1.00	1.00	0.15	0.00	0.60	1.00	0.15	1.00	0.15	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia

Nodo = Numero del nodo
Mo = Massa orizzontale

Nodo	Mo												
<KG>	<KG>												
-14513	63.26	-14512	50.31	-14511	49.41	-14510	45.25	-14509	48.50	-14508	55.65	-14507	47.21
-14506	48.74	-14505	46.95	-14504	52.74	-14503	50.23	-14502	39.95	-14501	39.23	-14500	35.93
-14499	38.51	-14498	96.67	-14497	75.40	-14496	72.90	-14495	65.55	-14494	11.22	-14493	17.80
-14492	15.62	-14491	18.06	-14490	19.73	-14489	17.47	-14488	9.95	-14487	15.79	-14486	13.86
-14485	16.02	-14484	17.17	-14483	17.93	-14482	7.94	-14481	12.60	-14480	11.05	-14479	12.78
-14478	13.57	-14477	13.53	-14476	8.06	-14475	12.79	-14474	11.22	-14473	12.97	-14472	13.90
-14471	14.52	-14470	8.02	-14469	12.72	-14468	11.16	-14467	12.91	-14466	13.58	-14465	12.90
-14464	7.88	-14463	12.51	-14462	10.98	-14461	12.69	-14460	13.60	-14459	14.20	-14458	11.65
-14457	18.50	-14456	16.23	-14455	18.77	-14454	18.92	-14453	13.83	-14452	18.36	-14451	11.35
-14450	18.01	-14449	15.80	-14448	18.27	-14447	19.23	-14446	24.79	-14445	9.78	-14444	15.53
-14443	13.62	-14442	15.75	-14441	18.06	-14440	11.37	-14439	18.05	-14438	15.83	-14437	18.31
-14436	19.96	-14435	17.52	-14434	11.46	-14433	18.20	-14432	15.97	-14431	18.46	-14430	19.78
-14429	22.86	-14428	17.55	-14427	13.12	-14426	14.21	-14425	12.38	-14424	13.90	-14423	12.38
-14422	17.64	-14421	25.43	-14420	11.46	-14419	18.20	-14418	15.97	-14417	18.46	-14416	19.78
-14415	22.87	-14414	11.46	-14413	18.20	-14412	15.97	-14411	18.46	-14410	19.78	-14409	22.86
-14408	17.55	-14407	13.12	-14406	14.21	-14405	12.38	-14404	13.90	-14403	12.38	-14402	17.64
-14401	25.43	-14400	11.46	-14399	18.20	-14398	15.97	-14397	18.46	-14396	19.78	-14395	22.87
-14394	10.97	-14393	17.41	-14392	15.27	-14391	17.66	-14390	18.92	-14389	21.87	-14388	16.79
-14387	12.55	-14386	10.70	-14385	6.19	-14384	6.95	-14383	6.19	-14382	14.80	-14381	24.32
-14380	10.97	-14379	17.41	-14378	15.27	-14377	17.66	-14376	18.92	-14375	21.87	-14374	10.47
-14373	16.62	-14372	14.58	-14371	16.86	-14370	18.06	-14369	20.87	-14368	16.02	-14367	11.98
-14366	7.19	-14365	11.97	-14364	23.22	-14363	10.47	-14362	16.62	-14361	14.58	-14360	16.86
-14359	18.06	-14358	20.88	-14357	10.47	-14356	16.62	-14355	14.58	-14354	16.86	-14353	18.06
-14352	20.87	-14351	16.02	-14350	11.98	-14349	7.19	-14348	11.97	-14347	23.22	-14346	10.47
-14345	16.62	-14344	14.58	-14343	16.86	-14342	18.06	-14341	20.88	-14340	10.47	-14339	16.62
-14338	14.58	-14337	16.86	-14336	18.06	-14335	20.87	-14334	16.02	-14333	11.98	-14332	7.19
-14331	11.97	-14330	23.22	-14329	10.47	-14328	16.62	-14327	14.58	-14326	16.86	-14325	18.06
-14324	20.88	-14323	10.47	-14322	16.62	-14321	14.58	-14320	16.86	-14319	18.06	-14318	20.87
-14316	16.02	-14314	11.98	-14312	7.19	-14308	11.97	-14306	23.22	-14304	10.47	-14303	16.62
-14302	14.58	-14301	16.86	-14300	18.06	-14299	20.88	-14298	10.47	-14297	16.62	-14296	14.58
-14295	16.86	-14294	18.06	-14293	20.87	-14291	16.02	-14289	11.98	-14287	7.19	-14283	11.97
-14281	23.22	-14279	10.47	-14278	16.62	-14277	14.58	-14276	16.86	-14275	18.06	-14274	20.88
-14273	33.27	-14272	26.11	-14271	22.91	-14270	26.49	-14269	28.77	-14268	27.91	-14267	40.47
-14266	15.79	-14265	13.86	-14264	16.02	-14263	17.17	-14262	25.94	-14261	32.28	-14260	12.60
-14259	11.05	-14258	12.78	-14257	13.57	-14256	19.52	-14255	32.76	-14254	12.79	-14253	11.22
-14252	12.97	-14251	13.90	-14250	18.11	-14249	32.60	-14248	12.72	-14247	11.16	-14246	12.91
-14245	13.58	-14244	12.90	-14243	37.79	-14242	21.61	-14241	18.96	-14240	21.92	-14239	23.49
-14238	19.48	-14237	47.40	-14236	18.50	-14235	16.23	-14234	18.77	-14233	18.92	-14232	13.83
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-9932 10.84	-9931 17.21	-9930 15.10	-9929 17.46	-9928 18.71	-9927 21.62	-9926 16.60
-9925 10.74	-9924 13.44	-9923 13.37	-9922 10.84	-9921 17.21	-9920 15.10	-9919 17.46
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-9903 18.14	-9902 17.92	-9901 18.14	-9900 17.92	-9899 19.93	-9898 21.95	-9897 25.31
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-8444	56.52	-8443	58.67	-8442	58.67	-8441	58.67	-8440	58.67	-8439	58.67	-8438	58.67
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-8416	57.24	-8415	66.20	-8414	58.69	-8413	58.69	-8412	58.69	-8411	58.71	-8410	58.73
-8409	58.73	-8408	58.73	-8407	56.51	-8406	54.29	-8405	54.29	-8404	54.29	-8403	48.26
-8402	12.88	-8401	101.27	-8400	86.48	-8399	76.67	-8398	88.66	-8397	94.00	-8396	140.45
-8395	57.02	-8394	55.01	-8393	52.93	-8392	52.56	-8391	50.79	-8390	143.76	-8389	74.46
-8388	51.80	-8387	72.07	-8386	36.78	-8385	55.69	-8384	54.26	-8383	54.26	-8382	54.26
-8381	56.40	-8380	58.55	-8379	58.55	-8378	58.55	-8377	58.55	-8376	58.55	-8375	58.55
-8374	58.55	-8373	66.05	-8372	57.12	-8371	57.12	-8370	57.12	-8369	59.97	-8368	62.83
-8367	62.83	-8366	56.72	-8365	50.93	-8364	62.36	-8363	58.64	-8362	61.83	-8361	61.07
-8360	67.94	-8359	74.81	-8358	80.14	-8357	67.17	-8356	50.39	-8355	51.91	-8354	58.62
-8353	51.60	-8352	49.71	-8351	56.74	-8350	55.21	-8349	54.41	-8348	57.12	-8347	59.83
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-8339	58.56	-8338	58.56	-8337	58.56	-8336	58.59	-8335	58.61	-8334	58.61	-8333	58.61
-8332	56.39	-8331	54.18	-8330	54.18	-8329	54.18	-8328	48.16	-8327	12.85	-8326	29.46
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-8318	46.89	-8317	46.89	-8316	46.89	-8315	46.89	-8314	46.89	-8313	49.86	-8312	45.74
-8311	45.74	-8310	45.74	-8309	48.03	-8308	50.32	-8307	50.32	-8306	49.29	-8305	44.84
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-8269	45.74	-8268	45.74	-8267	45.74	-8266	45.74	-8265	49.86	-8264	46.90	-8263	46.90
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-8234	22.19	-8233	23.25	-8232	23.25	-8231	23.25	-8230	20.44	-8229	19.03	-8228	21.13
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-8206	20.08	-8205	17.43	-8204	21.13	-8203	20.43	-8202	21.13	-8201	21.13	-8200	21.13
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-8124	10.12	-8123	30.30	-8122	22.20	-8121	16.80	-8120	28.99	-8119	8.91	-8118	10.24
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-8110	11.37	-8109	11.37	-8108	11.37	-8107	11.52	-8106	11.66	-8105	11.66	-8104	11.66
-8103	11.67	-8102	11.67	-8101	11.67	-8100	11.67	-8099	11.23	-8098	10.79	-8097	10.79
-8096	10.79	-8095	5.39	-8094	5.41	-8093	5.03	-8092	19.47	-8091	5.03	-8090	5.03
-8089	16.14	-8088	16.14	-8087	13.37	-8086	32.77	-8085	20.77	-8084	18.22	-8083	21.07
-8082	22.58	-8081	31.73	-8080	10.83	-8079	10.86	-8078	10.86	-8077	10.86	-8076	19.11
-8075	19.04	-8074	10.83	-8073	11.21	-8072	18.22	-8071	11.21	-8070	11.21	-8069	21.95
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-8061	12.49	-8060	19.33	-8059	25.77	-8058	22.40	-8057	21.20	-8056	39.31	-8055	25.59
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-7997	22.08	-7996	14.55	-7995	17.06	-7994	20.07	-7993	27.51	-7992	27.01	-7991	5.40
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-5899	7.08	-5898	7.08	-5897	6.08	-5896	24.12	-5895	20.77	-5894	18.22	-5893	21.07
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-5878	20.32	-5877	20.07	-5876	22.33	-5875	24.58	-5874	28.35	-5873	22.08	-5872	14.55
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-5815	19.47	-5814	5.41	-5813	5.41	-5812	16.14	-5811	16.14	-5810	32.77	-5809	20.77
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-5780	39.31	-5779	25.59	-5778	29.10	-5777	20.32	-5776	16.06	-5775	20.32	-5774	20.07
-5773	22.33	-5772	24.58	-5771	28.35	-5770	22.08	-5769	14.55	-5768	17.06	-5767	20.07
-5766	22.10	-5765	24.12	-5764	26.10	-5763	26.10	-5762	14.72	-5761	16.44	-5760	16.44
-5759	16.44	-5758	16.44	-5757	13.17	-5756	7.08	-5755	7.08	-5754	7.08	-5753	6.08
-1	69.00	45	138.19	46	279.93	47	164.87	48	73.44	49	279.54	50	88.51
51	138.33	52	279.70	53	67.18	54	133.53	55	279.91	56	169.46	57	138.52
58	279.79	59	67.33	60	138.15	61	279.91	62	169.46	63	138.15	64	279.91
65	169.46	163	17.61	164	21.40	165	19.19						

Totali masse nodi

Mo
<KG>
137941.00

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione**Simbologia**

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi
 ϕ_x = Coefficiente di partecipazione in dir. X
 ϕ_y = Coefficiente di partecipazione in dir. Y
 ϕ_z = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	ϕ_x	ϕ_y	ϕ_z	%Mx	%My	%Mz	%Jpz
1	*	1.08	82.60	-0.85	-210.71	0.00	0.00	32.19	0.00	0.00
2	*	0.59	49.33	-9.37	-156.34	0.00	0.06	17.72	0.00	0.00
3	*	0.40	10.15	248.79	-14.80	0.00	44.87	0.16	0.00	0.00
4	*	0.36	4.69	-23.29	-85.86	0.00	0.39	5.34	0.00	0.00
5		0.34	0.02	18.89	-0.96	0.00	0.26	0.00	0.00	0.00
6		0.34	0.00	11.93	0.22	0.00	0.10	0.00	0.00	0.00
7		0.34	0.00	0.10	0.03	0.00	0.00	0.00	0.00	0.00
8		0.34	0.01	-2.71	0.23	0.00	0.01	0.00	0.00	0.00
9		0.34	0.01	8.31	-0.24	0.00	0.05	0.00	0.00	0.00
10		0.34	0.03	-9.36	0.05	0.00	0.06	0.00	0.00	0.00

11	*	0.34	1.88	60.91	5.02	0.00	2.69	0.02	0.00	0.00
12	*	0.23	12.56	4.13	-49.93	0.00	0.01	1.81	0.00	0.00
13	*	0.20	12.56	0.82	82.98	0.00	0.00	4.99	0.00	0.00
14	*	0.16	15.62	-1.64	-36.75	0.00	0.00	0.98	0.00	0.00
15	*	0.14	15.62	4.23	70.27	0.00	0.01	3.58	0.00	0.00
16	*	0.12	11.58	10.11	35.21	0.00	0.07	0.90	0.00	0.00
17	*	0.11	3.85	9.28	-33.21	0.00	0.06	0.80	0.00	0.00
18	*	0.10	3.85	116.87	-1.56	0.00	9.90	0.00	0.00	0.00
19		0.09	4.04	-4.16	-0.64	0.00	0.01	0.00	0.00	0.00
20	*	0.09	1.69	7.00	-49.58	0.00	0.04	1.78	0.00	0.00
21		0.09	1.09	0.90	-8.59	0.00	0.00	0.05	0.00	0.00
22		0.09	0.14	-0.25	15.65	0.00	0.00	0.18	0.00	0.00
23		0.09	0.14	-1.22	11.16	0.00	0.00	0.09	0.00	0.00
24		0.08	3.75	4.01	-17.22	0.00	0.01	0.21	0.00	0.00
25		0.08	2.85	2.77	-0.21	0.00	0.01	0.00	0.00	0.00
26		0.08	1.06	0.53	11.67	0.00	0.00	0.10	0.00	0.00
27		0.08	0.86	-0.19	12.62	0.00	0.00	0.12	0.00	0.00
28		0.08	0.86	-0.10	2.58	0.00	0.00	0.00	0.00	0.00
29		0.07	3.73	-8.28	-16.00	0.00	0.05	0.19	0.00	0.00
30		0.07	2.51	2.60	-7.69	0.00	0.00	0.04	0.00	0.00
31		0.07	1.66	6.73	24.16	0.00	0.03	0.42	0.00	0.00
32		0.07	1.66	-1.58	0.08	0.00	0.00	0.00	0.00	0.00
33		0.06	2.73	-5.15	0.73	0.00	0.02	0.00	0.00	0.00
34	*	0.06	1.40	-32.06	22.82	0.00	0.75	0.38	0.00	0.00
35	*	0.06	0.89	68.11	-9.40	0.00	3.36	0.06	0.00	0.00
36	*	0.06	0.89	-89.14	-7.60	0.00	5.76	0.04	0.00	0.00
37		0.06	1.75	6.36	4.51	0.00	0.03	0.01	0.00	0.00
38		0.06	1.75	-0.51	-2.13	0.00	0.00	0.00	0.00	0.00
39		0.06	0.80	-4.68	8.05	0.00	0.02	0.05	0.00	0.00
40		0.05	0.80	-4.68	5.80	0.00	0.02	0.02	0.00	0.00
41		0.05	0.34	1.11	26.51	0.00	0.00	0.51	0.00	0.00
42		0.05	0.34	-4.74	3.01	0.00	0.02	0.01	0.00	0.00
43		0.05	3.96	-5.33	15.01	0.00	0.02	0.16	0.00	0.00
44		0.05	3.26	-0.15	15.72	0.00	0.00	0.18	0.00	0.00
45		0.05	0.68	0.20	-2.45	0.00	0.00	0.00	0.00	0.00
46		0.05	0.68	-0.72	-1.65	0.00	0.00	0.00	0.00	0.00
47		0.05	2.29	1.22	6.02	0.00	0.00	0.03	0.00	0.00
48		0.04	0.93	2.67	-4.16	0.00	0.01	0.01	0.00	0.00
49		0.04	0.93	5.28	-25.58	0.00	0.02	0.47	0.00	0.00
50		0.04	3.13	0.91	-27.51	0.00	0.00	0.55	0.00	0.00
51		0.04	1.58	-0.66	-19.61	0.00	0.00	0.28	0.00	0.00
52		0.04	0.86	-0.24	7.97	0.00	0.00	0.05	0.00	0.00
53		0.04	0.86	1.35	-13.51	0.00	0.00	0.13	0.00	0.00
54		0.04	1.18	0.13	6.59	0.00	0.00	0.03	0.00	0.00
55		0.04	0.56	-0.73	-3.21	0.00	0.00	0.01	0.00	0.00
56		0.04	0.56	1.74	16.28	0.00	0.00	0.19	0.00	0.00
57		0.04	1.22	-7.24	7.98	0.00	0.04	0.05	0.00	0.00
58		0.04	1.22	3.25	-6.71	0.00	0.01	0.03	0.00	0.00
59	*	0.04	0.98	-27.78	89.28	0.00	0.56	5.78	0.00	0.00
60		0.04	0.96	15.23	11.19	0.00	0.17	0.09	0.00	0.00
61		0.03	0.96	10.61	-1.43	0.00	0.08	0.00	0.00	0.00
62	*	0.03	2.01	-58.43	4.00	0.00	2.48	0.01	0.00	0.00
63		0.03	1.16	-10.71	-1.44	0.00	0.08	0.00	0.00	0.00
64	*	0.03	0.52	-30.68	19.97	0.00	0.68	0.29	0.00	0.00
65	*	0.03	0.52	77.17	32.95	0.00	4.32	0.79	0.00	0.00
66		0.03	0.59	19.11	23.77	0.00	0.26	0.41	0.00	0.00
67	*	0.03	0.59	-26.12	60.16	0.00	0.49	2.62	0.00	0.00
68	*	0.03	0.07	-22.44	38.14	0.00	0.36	1.05	0.00	0.00
69	*	0.03	0.07	2.95	-50.17	0.00	0.01	1.82	0.00	0.00
70	*	0.03	1.15	43.30	14.56	0.00	1.36	0.15	0.00	0.00
71		0.03	1.15	12.29	6.99	0.00	0.11	0.04	0.00	0.00
72		0.03	0.55	-4.86	-11.46	0.00	0.02	0.10	0.00	0.00
73	*	0.03	0.55	14.19	33.64	0.00	0.15	0.82	0.00	0.00
74		0.03	1.15	-11.68	26.20	0.00	0.10	0.50	0.00	0.00
75		0.03	0.68	2.88	0.10	0.00	0.01	0.00	0.00	0.00
76		0.03	0.68	2.61	1.81	0.00	0.00	0.00	0.00	0.00
77		0.03	0.71	-5.40	9.92	0.00	0.02	0.07	0.00	0.00
78		0.03	0.80	-1.68	0.64	0.00	0.00	0.00	0.00	0.00
79	*	0.03	0.21	-9.29	-35.24	0.00	0.06	0.90	0.00	0.00
80		0.03	0.21	3.66	12.26	0.00	0.01	0.11	0.00	0.00
81		0.03	1.83	-10.25	6.75	0.00	0.08	0.03	0.00	0.00
82	*	0.03	1.02	47.43	20.02	0.00	1.63	0.29	0.00	0.00
83	*	0.03	1.02	70.10	36.27	0.00	3.56	0.95	0.00	0.00
84	*	0.03	1.50	29.30	17.68	0.00	0.62	0.23	0.00	0.00
85		0.03	1.50	3.58	24.94	0.00	0.01	0.45	0.00	0.00
86	*	0.02	2.07	22.85	4.46	0.00	0.38	0.01	0.00	0.00
87		0.02	1.03	11.48	-25.10	0.00	0.10	0.46	0.00	0.00
88		0.02	0.41	-3.83	-6.29	0.00	0.01	0.03	0.00	0.00
89		0.02	0.41	11.51	-18.38	0.00	0.10	0.24	0.00	0.00
90		0.02	0.65	-5.35	2.28	0.00	0.02	0.00	0.00	0.00
91		0.02	0.38	13.42	-16.81	0.00	0.13	0.20	0.00	0.00
92		0.02	0.34	10.97	-0.36	0.00	0.09	0.00	0.00	0.00
93	*	0.02	0.34	28.93	-28.05	0.00	0.61	0.57	0.00	0.00
94	*	0.02	0.34	23.16	-10.48	0.00	0.39	0.08	0.00	0.00
95		0.02	0.34	18.23	8.58	0.00	0.24	0.05	0.00	0.00
96		0.02	0.73	0.40	1.74	0.00	0.00	0.00	0.00	0.00
97		0.02	0.73	0.27	3.29	0.00	0.00	0.01	0.00	0.00
98		0.02	0.74	2.10	-26.37	0.00	0.00	0.50	0.00	0.00
99		0.02	1.01	11.04	6.21	0.00	0.09	0.03	0.00	0.00
100		0.02	0.55	-3.82	-5.97	0.00	0.01	0.03	0.00	0.00
101		0.02	0.55	-2.27	0.88	0.00	0.00	0.00	0.00	0.00
102		0.02	0.06	1.94	3.93	0.00	0.00	0.01	0.00	0.00
103		0.02	0.06	-0.69	-12.23	0.00	0.00	0.11	0.00	0.00
104		0.02	0.65	0.16	-4.48	0.00	0.00	0.01	0.00	0.00
105		0.02	0.46	-0.31	-8.15	0.00	0.00	0.05	0.00	0.00
106		0.02	0.46	-6.83	-7.60	0.00	0.03	0.04	0.00	0.00
107		0.02	0.23	1.17	-14.05	0.00	0.00	0.14	0.00	0.00
108		0.02	0.23	-1.57	4.51	0.00	0.00	0.01	0.00	0.00

109	0.02	0.41	-11.19	3.78	0.00	0.09	0.01	0.00	0.00
110	0.02	0.03	1.96	2.28	0.00	0.00	0.00	0.00	0.00
111	0.02	0.03	-2.73	0.46	0.00	0.01	0.00	0.00	0.00
112	0.02	0.83	5.59	-0.87	0.00	0.02	0.00	0.00	0.00
113	0.02	0.67	-6.01	-5.03	0.00	0.03	0.02	0.00	0.00
114	*	0.02	0.67	20.48	0.32	0.00	0.30	0.00	0.00
115	0.02	0.60	1.85	-6.17	0.00	0.00	0.03	0.00	0.00
116	0.02	0.60	-5.80	0.82	0.00	0.02	0.00	0.00	0.00
117	0.02	0.34	0.50	7.19	0.00	0.00	0.04	0.00	0.00
118	0.02	0.34	-5.25	4.59	0.00	0.02	0.02	0.00	0.00
119	0.02	0.59	-3.37	3.30	0.00	0.01	0.01	0.00	0.00
120	0.02	0.60	6.79	0.17	0.00	0.03	0.00	0.00	0.00
121	0.02	0.30	4.61	4.73	0.00	0.02	0.02	0.00	0.00
122	0.02	0.30	-0.39	2.56	0.00	0.00	0.00	0.00	0.00
123	0.02	0.33	-10.21	2.95	0.00	0.08	0.01	0.00	0.00
124	0.02	0.33	-1.51	4.21	0.00	0.00	0.01	0.00	0.00
125	0.02	0.38	-0.30	-1.76	0.00	0.00	0.00	0.00	0.00
126	0.02	0.49	-8.82	0.17	0.00	0.06	0.00	0.00	0.00
127	0.02	0.49	0.86	-5.63	0.00	0.00	0.02	0.00	0.00
128	0.02	0.43	6.00	-5.58	0.00	0.03	0.02	0.00	0.00
129	0.02	0.43	-7.16	-3.15	0.00	0.04	0.01	0.00	0.00
130	0.02	0.59	-6.43	-0.08	0.00	0.03	0.00	0.00	0.00
131	0.02	0.33	9.24	2.02	0.00	0.06	0.00	0.00	0.00
132	0.02	0.33	7.54	-7.46	0.00	0.04	0.04	0.00	0.00
133	0.02	0.80	5.53	2.13	0.00	0.02	0.00	0.00	0.00
134	0.02	0.10	0.88	-13.39	0.00	0.00	0.13	0.00	0.00
135	0.02	0.10	-4.60	-2.01	0.00	0.02	0.00	0.00	0.00
136	0.02	0.30	-1.03	-10.53	0.00	0.00	0.08	0.00	0.00
137	0.02	0.30	6.86	0.55	0.00	0.03	0.00	0.00	0.00
138	0.02	0.43	4.17	4.28	0.00	0.01	0.01	0.00	0.00
139	0.02	0.16	-2.35	-4.02	0.00	0.00	0.01	0.00	0.00
140	0.02	0.16	-8.02	-1.49	0.00	0.05	0.00	0.00	0.00
141	0.02	0.30	2.20	-9.54	0.00	0.00	0.07	0.00	0.00
142	0.02	0.21	-0.61	-0.11	0.00	0.00	0.00	0.00	0.00
143	0.02	0.21	0.37	-4.18	0.00	0.00	0.01	0.00	0.00
144	0.02	0.26	-5.95	-4.22	0.00	0.03	0.01	0.00	0.00
145	0.02	0.26	-0.21	3.51	0.00	0.00	0.01	0.00	0.00
146	0.02	0.30	-10.50	3.44	0.00	0.08	0.01	0.00	0.00
147	0.02	0.22	-3.73	7.61	0.00	0.01	0.04	0.00	0.00
148	0.02	0.22	-4.19	1.65	0.00	0.01	0.00	0.00	0.00
149	0.02	0.13	6.22	-8.59	0.00	0.03	0.05	0.00	0.00
150	0.02	0.13	7.54	7.60	0.00	0.04	0.04	0.00	0.00
151	0.02	0.37	1.73	-5.66	0.00	0.00	0.02	0.00	0.00
152	0.02	0.37	5.88	1.03	0.00	0.03	0.00	0.00	0.00
153	0.02	0.84	-12.46	-0.64	0.00	0.11	0.00	0.00	0.00
154	0.02	0.23	-10.92	-2.36	0.00	0.09	0.00	0.00	0.00
155	0.02	0.23	15.43	-0.95	0.00	0.17	0.00	0.00	0.00
156	0.02	0.26	-1.94	-4.79	0.00	0.00	0.02	0.00	0.00
157	0.02	0.26	-19.02	2.61	0.00	0.26	0.00	0.00	0.00
158	0.02	0.60	-13.07	-3.77	0.00	0.12	0.01	0.00	0.00
159	*	0.01	0.44	24.03	4.67	0.00	0.42	0.02	0.00
160	0.01	0.44	-4.13	4.02	0.00	0.01	0.01	0.00	0.00
161	0.01	0.09	4.79	2.84	0.00	0.02	0.01	0.00	0.00
162	0.01	0.09	-8.25	2.41	0.00	0.05	0.00	0.00	0.00
163	0.01	0.27	-6.17	-6.01	0.00	0.03	0.03	0.00	0.00
164	0.01	0.21	-6.24	3.47	0.00	0.03	0.01	0.00	0.00
165	0.01	0.21	4.12	-1.57	0.00	0.01	0.00	0.00	0.00
166	0.01	0.30	-4.00	1.28	0.00	0.01	0.00	0.00	0.00
167	0.01	0.38	2.72	0.79	0.00	0.01	0.00	0.00	0.00
168	0.01	0.38	3.19	12.61	0.00	0.01	0.12	0.00	0.00
169	0.01	0.47	0.38	-2.76	0.00	0.00	0.01	0.00	0.00
170	0.01	0.66	0.09	-1.36	0.00	0.00	0.00	0.00	0.00
171	0.01	0.66	-1.70	5.43	0.00	0.00	0.02	0.00	0.00
172	0.01	0.17	3.76	-1.46	0.00	0.01	0.00	0.00	0.00
173	0.01	0.17	-0.52	1.61	0.00	0.00	0.00	0.00	0.00
174	0.01	0.38	2.77	1.84	0.00	0.01	0.00	0.00	0.00
175	0.01	0.38	6.23	-0.09	0.00	0.03	0.00	0.00	0.00
176	0.01	0.82	17.85	-8.87	0.00	0.23	0.06	0.00	0.00
177	0.01	0.07	17.61	3.74	0.00	0.22	0.01	0.00	0.00
178	0.01	0.07	-0.67	-11.09	0.00	0.00	0.09	0.00	0.00
179	0.01	0.28	-1.48	11.30	0.00	0.00	0.09	0.00	0.00
180	0.01	0.32	0.73	-1.69	0.00	0.00	0.00	0.00	0.00

Tot.cons. 86.37 87.15 0.00 0.00

Elenco coefficienti di risposta

Simbologia

Modo = Numero del modo di vibrare

Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X

Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di operatività

Modo	Sx	Sy			
1	6.59	6.59	10	17.19	17.19
2	12.03	12.03	11	17.19	17.19
3	17.19	17.19	12	17.19	17.19
4	17.19	17.19	13	17.19	17.19
5	17.19	17.19	14	17.19	17.19
6	17.19	17.19	15	17.19	17.19
7	17.19	17.19	16	15.84	15.84
8	17.19	17.19	17	14.89	14.89
9	17.19	17.19	18	14.59	14.59
			19	13.77	13.77
			20	13.50	13.50
			21	13.38	13.38
			22	13.31	13.31
			23	13.30	13.30
			24	12.94	12.94
			25	12.71	12.71
			26	12.54	12.54
			27	12.48	12.48
			28	12.43	12.43
			29	12.03	12.03
			30	11.84	11.84
			31	11.71	11.71
			32	11.63	11.63
			33	11.50	11.50
			34	11.35	11.35
			35	11.29	11.29
			36	11.25	11.25
			37	11.07	11.07

38	11.00	11.00
39	10.90	10.90
40	10.86	10.86
41	10.72	10.72
42	10.71	10.71
43	10.55	10.55
44	10.40	10.40
45	10.28	10.28
46	10.26	10.26
47	10.18	10.18
48	10.09	10.09
49	10.06	10.06
50	9.96	9.96
51	9.83	9.83
52	9.79	9.79
53	9.76	9.76
54	9.72	9.72
55	9.59	9.59
56	9.57	9.57
57	9.49	9.49
58	9.46	9.46
59	9.38	9.38
60	9.36	9.36
61	9.33	9.33
62	9.23	9.23
63	9.18	9.18
64	9.15	9.15
65	9.14	9.14
66	9.12	9.12
67	9.11	9.11
68	9.09	9.09
69	9.09	9.09
70	9.06	9.06
71	9.03	9.03
72	8.98	8.98
73	8.97	8.97
74	8.94	8.94
75	8.91	8.91
76	8.90	8.90
77	8.88	8.88
78	8.86	8.86
79	8.82	8.82
80	8.81	8.81
81	8.76	8.76
82	8.73	8.73
83	8.70	8.70
84	8.65	8.65
85	8.63	8.63
86	8.59	8.59
87	8.54	8.54
88	8.52	8.52
89	8.51	8.51
90	8.47	8.47
91	8.46	8.46
92	8.45	8.45
93	8.44	8.44
94	8.41	8.41
95	8.41	8.41
96	8.38	8.38
97	8.37	8.37
98	8.35	8.35
99	8.34	8.34
100	8.31	8.31
101	8.30	8.30
102	8.28	8.28
103	8.28	8.28
104	8.26	8.26
105	8.25	8.25
106	8.25	8.25
107	8.24	8.24
108	8.23	8.23
109	8.23	8.23
110	8.21	8.21
111	8.21	8.21
112	8.20	8.20
113	8.17	8.17
114	8.16	8.16
115	8.14	8.14
116	8.13	8.13
117	8.12	8.12
118	8.11	8.11
119	8.10	8.10
120	8.09	8.09
121	8.08	8.08
122	8.08	8.08
123	8.07	8.07
124	8.07	8.07
125	8.06	8.06
126	8.05	8.05
127	8.05	8.05
128	8.04	8.04
129	8.03	8.03
130	8.02	8.02
131	8.01	8.01
132	8.01	8.01
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134	7.99	7.99
135	7.98	7.98

136	7.98	7.98
137	7.97	7.97
138	7.96	7.96
139	7.96	7.96
140	7.96	7.96
141	7.95	7.95
142	7.95	7.95
143	7.94	7.94
144	7.92	7.92
145	7.92	7.92
146	7.90	7.90
147	7.90	7.90
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150	7.88	7.88
151	7.88	7.88
152	7.87	7.87
153	7.86	7.86
154	7.85	7.85
155	7.85	7.85
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157	7.84	7.84
158	7.83	7.83
159	7.82	7.82
160	7.82	7.82
161	7.81	7.81
162	7.81	7.81
163	7.80	7.80
164	7.79	7.79
165	7.79	7.79
166	7.79	7.79
167	7.78	7.78
168	7.78	7.78
169	7.77	7.77
170	7.76	7.76
171	7.75	7.75
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174	7.74	7.74
175	7.73	7.73
176	7.72	7.72
177	7.71	7.71
178	7.71	7.71
179	7.71	7.71
180	7.71	7.71

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53	11.71	11.71
54	11.67	11.67
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56	11.49	11.49
57	11.39	11.39
58	11.35	11.35
59	11.26	11.26
60	11.23	11.23
61	11.20	11.20
62	11.08	11.08
63	11.02	11.02
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66	10.95	10.95
67	10.93	10.93
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69	10.91	10.91
70	10.87	10.87
71	10.84	10.84
72	10.78	10.78
73	10.77	10.77
74	10.73	10.73
75	10.70	10.70
76	10.68	10.68
77	10.66	10.66
78	10.64	10.64
79	10.58	10.58
80	10.58	10.58
81	10.52	10.52
82	10.47	10.47
83	10.45	10.45
84	10.39	10.39
85	10.36	10.36
86	10.31	10.31
87	10.25	10.25
88	10.23	10.23
89	10.22	10.22
90	10.17	10.17
91	10.15	10.15
92	10.15	10.15
93	10.14	10.14
94	10.10	10.10
95	10.10	10.10
96	10.06	10.06
97	10.04	10.04
98	10.03	10.03
99	10.01	10.01
100	9.98	9.98
101	9.97	9.97
102	9.94	9.94
103	9.94	9.94
104	9.92	9.92
105	9.91	9.91
106	9.90	9.90
107	9.89	9.89
108	9.88	9.88
109	9.88	9.88
110	9.86	9.86
111	9.86	9.86
112	9.85	9.85
113	9.81	9.81
114	9.79	9.79
115	9.77	9.77
116	9.76	9.76
117	9.75	9.75
118	9.74	9.74
119	9.73	9.73
120	9.72	9.72
121	9.71	9.71
122	9.70	9.70
123	9.69	9.69
124	9.69	9.69
125	9.68	9.68
126	9.67	9.67
127	9.66	9.66
128	9.65	9.65
129	9.65	9.65
130	9.63	9.63
131	9.63	9.63
132	9.62	9.62
133	9.60	9.60
134	9.59	9.59
135	9.59	9.59
136	9.58	9.58
137	9.58	9.58
138	9.56	9.56
139	9.56	9.56
140	9.55	9.55
141	9.55	9.55
142	9.54	9.54
143	9.54	9.54
144	9.51	9.51
145	9.51	9.51
146	9.49	9.49
147	9.49	9.49

Stato limite di danno

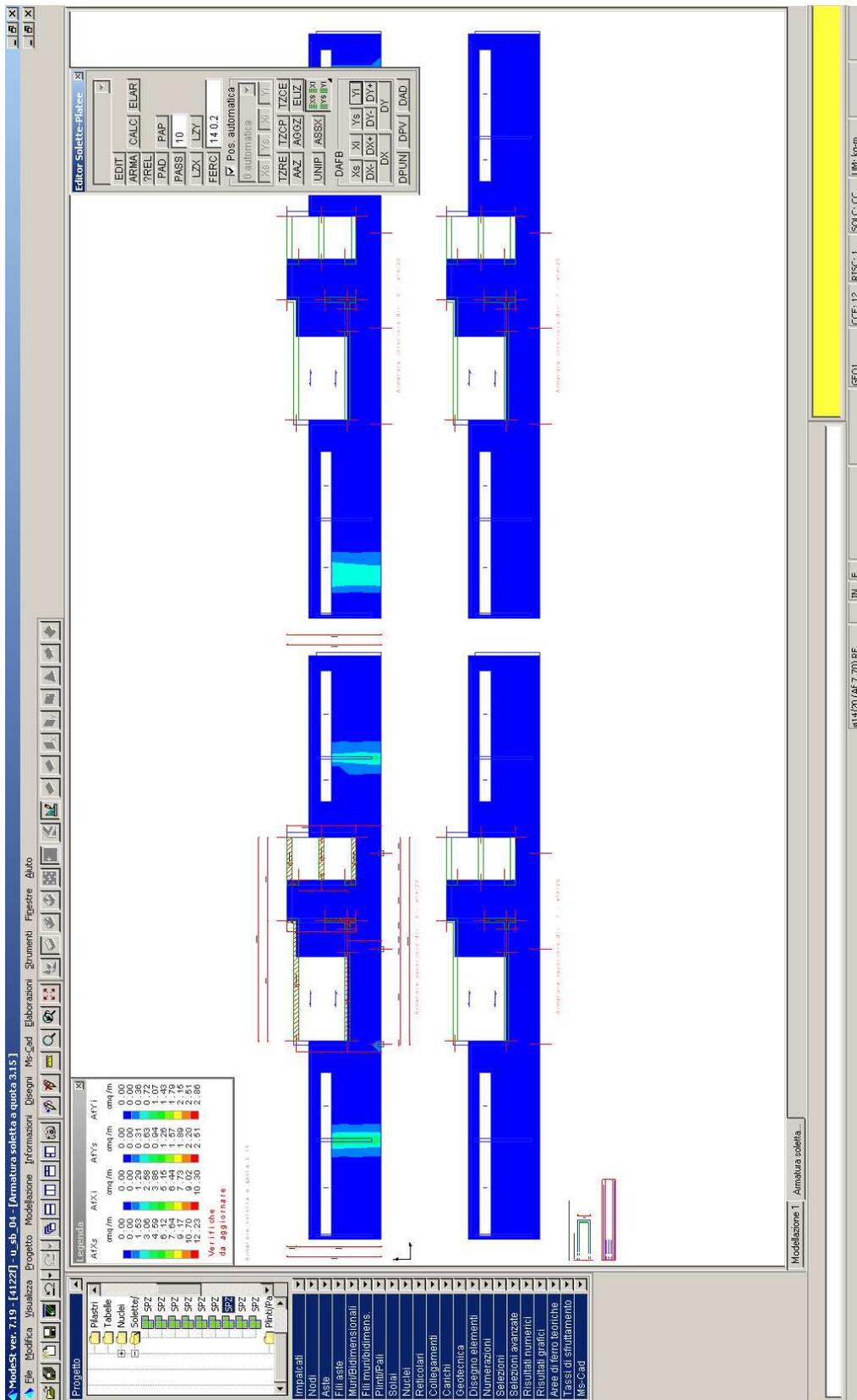
Modo Sx	Sy
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4	20.93 20.93
5	20.93 20.93
6	20.93 20.93
7	20.93 20.93
8	20.93 20.93
9	20.93 20.93
10	20.93 20.93
11	20.93 20.93
12	20.93 20.93
13	20.93 20.93
14	20.93 20.93
15	20.77 20.77
16	18.98 18.98
17	17.85 17.85
18	17.48 17.48
19	16.51 16.51
20	16.18 16.18
21	16.04 16.04
22	15.96 15.96
23	15.95 15.95
24	15.51 15.51
25	15.24 15.24
26	15.04 15.04
27	14.97 14.97
28	14.91 14.91
29	14.42 14.42
30	14.19 14.19
31	14.04 14.04
32	13.94 13.94
33	13.79 13.79
34	13.62 13.62
35	13.54 13.54
36	13.49 13.49
37	13.28 13.28
38	13.19 13.19
39	13.07 13.07
40	13.03 13.03
41	12.86 12.86
42	12.84 12.84
43	12.65 12.65
44	12.48 12.48
45	12.34 12.34
46	12.31 12.31
47	12.21 12.21
48	12.10 12.10
49	12.07 12.07

148	9.49	9.49	35	23.31	23.31	108	20.40	20.40
149	9.47	9.47	36	23.27	23.27	109	20.40	20.40
150	9.47	9.47	37	23.10	23.10	110	20.39	20.39
151	9.46	9.46	38	23.03	23.03	111	20.39	20.39
152	9.46	9.46	39	22.93	22.93	112	20.38	20.38
153	9.44	9.44	40	22.90	22.90	113	20.34	20.34
154	9.43	9.43	41	22.77	22.77	114	20.33	20.33
155	9.42	9.42	42	22.75	22.75	115	20.32	20.32
156	9.42	9.42	43	22.60	22.60	116	20.31	20.31
157	9.42	9.42	44	22.46	22.46	117	20.29	20.29
158	9.41	9.41	45	22.35	22.35	118	20.29	20.29
159	9.40	9.40	46	22.33	22.33	119	20.28	20.28
160	9.39	9.39	47	22.25	22.25	120	20.27	20.27
161	9.38	9.38	48	22.17	22.17	121	20.26	20.26
162	9.38	9.38	49	22.14	22.14	122	20.26	20.26
163	9.36	9.36	50	22.04	22.04	123	20.25	20.25
164	9.36	9.36	51	21.92	21.92	124	20.25	20.25
165	9.36	9.36	52	21.88	21.88	125	20.24	20.24
166	9.35	9.35	53	21.85	21.85	126	20.24	20.24
167	9.35	9.35	54	21.82	21.82	127	20.23	20.23
168	9.34	9.34	55	21.69	21.69	128	20.22	20.22
169	9.34	9.34	56	21.67	21.67	129	20.21	20.21
170	9.32	9.32	57	21.60	21.60	130	20.21	20.21
171	9.31	9.31	58	21.57	21.57	131	20.20	20.20
172	9.31	9.31	59	21.50	21.50	132	20.19	20.19
173	9.30	9.30	60	21.47	21.47	133	20.18	20.18
174	9.29	9.29	61	21.45	21.45	134	20.17	20.17
175	9.29	9.29	62	21.35	21.35	135	20.17	20.17
176	9.28	9.28	63	21.30	21.30	136	20.16	20.16
177	9.27	9.27	64	21.28	21.28	137	20.16	20.16
178	9.27	9.27	65	21.26	21.26	138	20.15	20.15
179	9.26	9.26	66	21.25	21.25	139	20.14	20.14
180	9.26	9.26	67	21.24	21.24	140	20.14	20.14
			68	21.22	21.22	141	20.14	20.14
			69	21.22	21.22	142	20.13	20.13
			70	21.19	21.19	143	20.13	20.13
			71	21.16	21.16	144	20.11	20.11
			72	21.11	21.11	145	20.10	20.10
			73	21.10	21.10	146	20.09	20.09
			74	21.08	21.08	147	20.09	20.09
			75	21.05	21.05	148	20.09	20.09
			76	21.03	21.03	149	20.07	20.07
			77	21.02	21.02	150	20.07	20.07
			78	21.00	21.00	151	20.07	20.07
			79	20.96	20.96	152	20.06	20.06
			80	20.95	20.95	153	20.05	20.05
			81	20.91	20.91	154	20.04	20.04
			82	20.87	20.87	155	20.04	20.04
			83	20.85	20.85	156	20.04	20.04
			84	20.80	20.80	157	20.03	20.03
			85	20.78	20.78	158	20.03	20.03
			86	20.74	20.74	159	20.02	20.02
			87	20.69	20.69	160	20.01	20.01
			88	20.67	20.67	161	20.00	20.00
			89	20.67	20.67	162	20.00	20.00
			90	20.63	20.63	163	19.99	19.99
			91	20.62	20.62	164	19.99	19.99
			92	20.61	20.61	165	19.98	19.98
			93	20.61	20.61	166	19.98	19.98
			94	20.58	20.58	167	19.98	19.98
			95	20.57	20.57	168	19.97	19.97
			96	20.54	20.54	169	19.97	19.97
			97	20.53	20.53	170	19.96	19.96
			98	20.52	20.52	171	19.95	19.95
			99	20.50	20.50	172	19.94	19.94
			100	20.48	20.48	173	19.94	19.94
			101	20.47	20.47	174	19.93	19.93
			102	20.45	20.45	175	19.93	19.93
			103	20.45	20.45	176	19.92	19.92
			104	20.43	20.43	177	19.91	19.91
			105	20.42	20.42	178	19.91	19.91
			106	20.42	20.42	179	19.91	19.91
			107	20.41	20.41	180	19.91	19.91

Stato limite di salvaguardia della vita

Modo	Sx	Sy
1	13.02	13.02
2	23.78	23.78
3	30.16	30.16
4	30.16	30.16
5	30.16	30.16
6	30.16	30.16
7	30.16	30.16
8	30.16	30.16
9	30.16	30.16
10	30.16	30.16
11	30.16	30.16
12	30.16	30.16
13	30.16	30.16
14	30.16	30.16
15	29.04	29.04
16	27.62	27.62
17	26.72	26.72
18	26.44	26.44
19	25.66	25.66
20	25.40	25.40
21	25.29	25.29
22	25.22	25.22
23	25.22	25.22
24	24.87	24.87
25	24.65	24.65
26	24.50	24.50
27	24.44	24.44
28	24.39	24.39
29	24.01	24.01
30	23.82	23.82
31	23.70	23.70
32	23.63	23.63
33	23.50	23.50
34	23.37	23.37

4.4. MAPPE D'ARMATURA SOLETTA SUPERIORE BLOCCO B



Modest ver.7.19 - u_sb_04 - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni MS-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto

- Tabella
- Modelli
- Solette/SPZ
- SPZ
- SPZ
- SPZ
- SPZ
- SPZ
- Plinti/Pg

Leggenda

M-Mu X-	M-Mu Y-	M-Mu X+	M-Mu Y+
0.00E+000	0.00E+000	0.00E+000	0.00E+000
-1.25E-003	-1.25E-003	-1.25E-003	-1.25E-003
-3.75E-003	-3.75E-003	-3.75E-003	-3.75E-003
-6.00E-003	-6.00E-003	-6.00E-003	-6.00E-003
-7.50E-003	-7.50E-003	-7.50E-003	-7.50E-003
-8.75E-003	-8.75E-003	-8.75E-003	-8.75E-003
-1.00E-002	-1.00E-002	-1.00E-002	-1.00E-002

da aggiornare

Editor Solette-Place

EDIT ARMA CALC ELAR
 SREL
 PAD PAP
 PASS 10
 LZL LZL

FERC 14 0.2

Pos automatica

TZRE TZCP TZCE
 AAZ AGGZ ELZ
 UNIP ASSX
 DAFB
 XS XI XS YI
 DX DX4 DX DY4
 DX
 DPUN DPV DAD

Modellazione 1 Armatura soletta...

18.89 6.35 GEO1 CCE.12 RISC.11 SOLC.CC UNI-hgm

5. MODELLAZIONE D

5.1. PARAMETRI DI CALCOLO

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con: ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti: Xfinest ver. 8.1, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08

Tipo di calcolo: analisi sismica dinamica

Schematizzazione piani rigidi: metodo Master-Slave

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <kg/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: ISOSHELL
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per Buckling: No
- Trascura Buckling torsionale: No

Dati struttura

- Zona sismica: zona 3
- Sito di costruzione: SCANDICCI LON. 11.18240 LAT. 43.75800
Contenuto tra ID reticolo: 20058 20057 20280 20279

Simbologia

TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 Ag = Accelerazione orizzontale massima al sito
 FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale

TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

TCC Ag FO TC*
 SLO 0.5163 2.59 0.26
 SLD 0.6103 2.63 0.28
 SLV 1.4446 2.39 0.30

- Tipo di opera: Opera ordinaria
- Vita nominale V_N : 50.00
- Classe d'uso: classe III
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 41.96 <m>
- Numero piani edificio: 9
- Coefficiente θ : 0
- Edificio regolare in altezza: no
- Edificio regolare in pianta: no
- Forze orizzontali convenzionali per stati limite non sismici: no

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. o prefabbricato a telaio a più piani e più campate

Coeff. C_1	0.075
Periodo T_1	1.23648
Coeff. λ SLO	1.00
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovrarigidità (α_s/α_1)	1.15
Valore di riferimento del fattore di struttura (q_0)	3.45
Fattore riduttivo (K_w)	1.00
Fattore di struttura (q)	1.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica: 1.00
- Modi da calcolare: 240
- Modi da considerare: con singola massa superiore a 1.00%
- Smorzamento spettro: 5.00

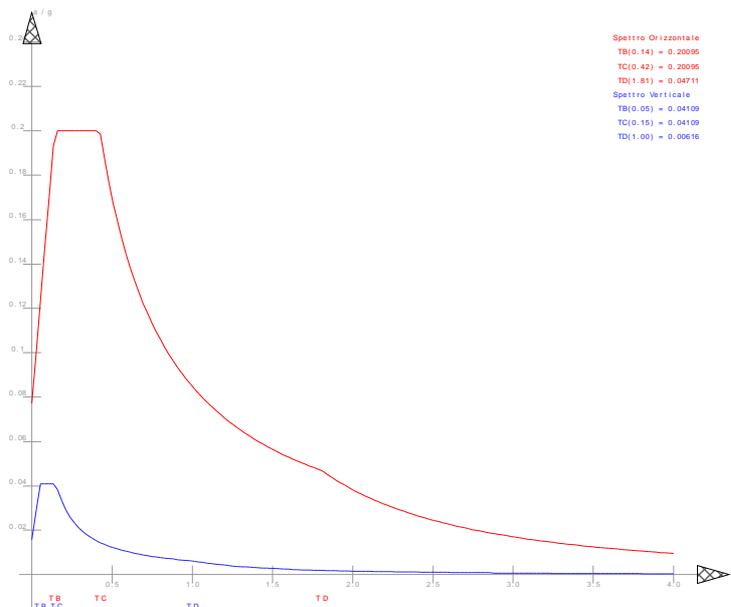


Figura numero 1: Spettro allo SLO

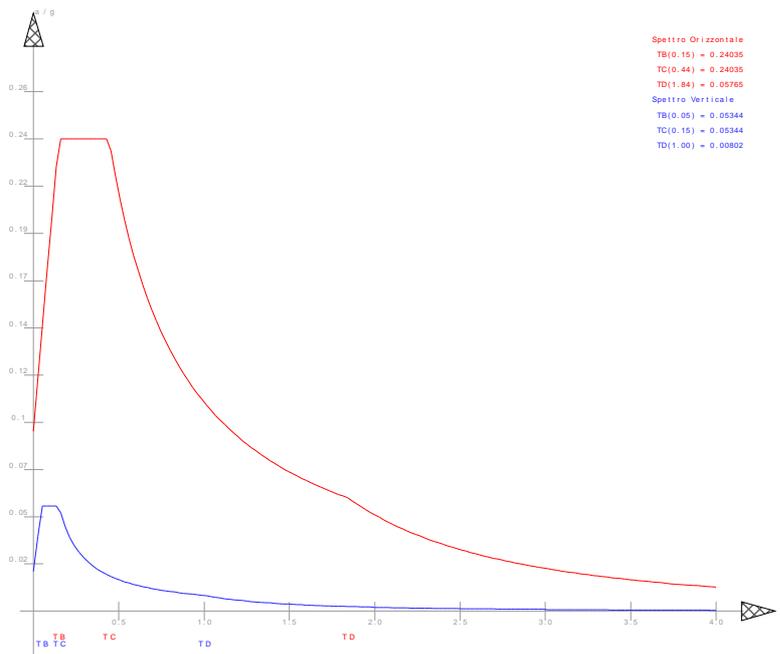


Figura numero 2: Spettro allo SLD

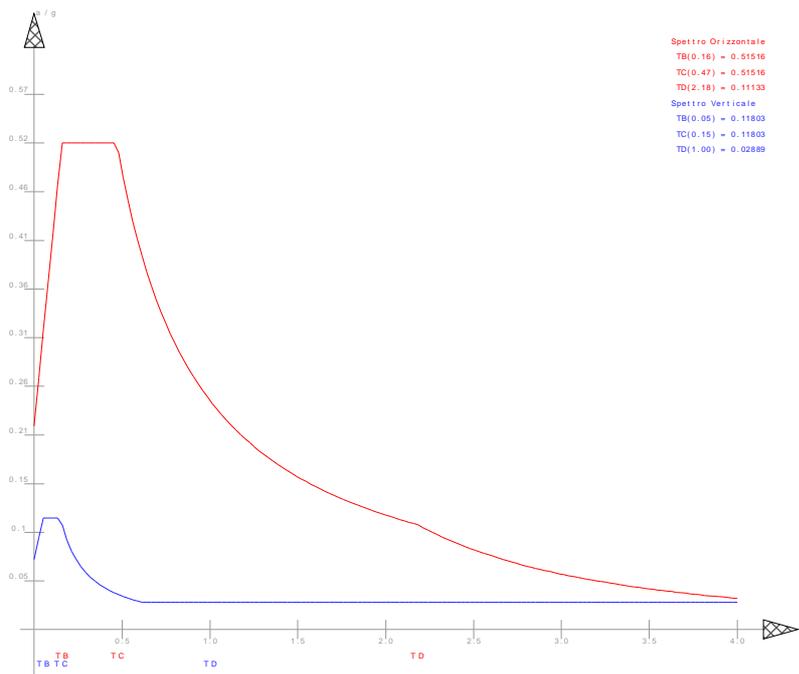


Figura numero 3: Spettro allo SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Dati di piano

Simbologia

Imp. = Numero dell'impalcato
 Lx = Dimensione del piano in dir. X
 Ly = Dimensione del piano in dir. Y
 Ex = Eccentricità in dir. X

Ey = Eccentricità in dir. Y
Ea = Eccentricità complessiva

Imp.	Lx	Ly	Ex	Ey	Ea
<m>	<m>	<m>	<m>	<m>	<m>
1	36.00	15.90	1.80	0.80	1.97
2	6.00	3.35	0.30	0.17	0.34
3	36.00	21.44	1.80	1.07	2.10
4	36.00	21.44	1.80	1.07	2.10
5	36.00	21.44	1.80	1.07	2.10
6	36.00	21.44	1.80	1.07	2.10
7	36.00	21.44	1.80	1.07	2.10
8	36.00	21.44	1.80	1.07	2.10
9	36.00	21.44	1.80	1.07	2.10

Condizioni di carico elementari

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
s = Coeff. di riduzione
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	s	Mx	My	Mz	Jpx	Jpy	Jpz
1	pp e perm	1.00	1.00	1.00	1.00	0.00	0.00	1.00
2	tamponamenti	1.00	1.00	1.00	1.00	0.00	0.00	1.00
3	permanente solette	1.00	1.00	1.00	1.00	0.00	0.00	1.00
4	parcheggio	1.00	1.00	1.00	1.00	0.00	0.00	1.00
5	negozi (2)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
6	carrabile	1.00	1.00	1.00	1.00	0.00	0.00	1.00
7	mezzanino (4)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
8	uffici (3)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
9	copertura (5 6 9)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
10	scale (1 7 8)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
11	permanenti non strutturali solai	1.00	1.00	1.00	1.00	0.00	0.00	1.00
12	grigliati esterni (10)	1.00	1.00	1.00	1.00	0.00	0.00	1.00
13	spinta della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
14	spinta accidentale della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
15	variazione termica uniforme	1.00	0.00	0.00	0.00	0.00	0.00	0.00
16	Momento torcente - SLO	--	--	--	--	--	--	--
17	Sisma dir. X - SLO	--	--	--	--	--	--	--
18	Sisma dir. Y - SLO	--	--	--	--	--	--	--
19	Sisma dir. Z - SLO	--	--	--	--	--	--	--
20	Momento torcente - SLD	--	--	--	--	--	--	--
21	Sisma dir. X - SLD	--	--	--	--	--	--	--
22	Sisma dir. Y - SLD	--	--	--	--	--	--	--
23	Sisma dir. Z - SLD	--	--	--	--	--	--	--
24	Momento torcente - SLV	--	--	--	--	--	--	--
25	Sisma dir. X - SLV	--	--	--	--	--	--	--
26	Sisma dir. Y - SLV	--	--	--	--	--	--	--
27	Sisma dir. Z - SLV	--	--	--	--	--	--	--

Ambienti di carico

Simbologia

N Numero
Comm. Commento
1 pp e perm
2 tamponamenti
3 permanente solette
4 parcheggio
5 negozi (2)
6 carrabile
7 mezzanino (4)
8 uffici (3)
9 copertura (5 6 9)
10 scale (1 7 8)
11 permanenti non strutturali solai
12 grigliati esterni (10)
13 spinta della terra
14 spinta accidentale della terra
15 variazione termica uniforme

Fazioni orizzontali convenzionali

- SLU Stato limite ultimo
- SLR Stato limite per combinazioni rare
- SLF Stato limite per combinazioni frequenti
- SLQ Stato limite per combinazioni quasi permanenti o di danno

N Comm.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	S	SLU	SLR	SLF	SLQ
1 Calcolo sismico	si	no	no	no	no															
2 Calcolo statico	si	no	si	si	si	si														

Combinazioni delle cce

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLU S = Stato limite ultimo (azione sismica)
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SLV = Stato limite di salvaguardia della vita
- SLC = Stato limite di prevenzione del collasso
- SLO = Stato limite di operatività
- An. = Tipo di analisi
- L = Lineare
- NL = Non lineare
- Bk = Buckling
- S = Si
- N = No

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Mt	±S X	±S Y	±S Z
1	CC 1 - Amb. 1 (SLU S) S Mt+X+0.3Y+0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	0.30	0.30
2	CC 2 - Amb. 1 (SLU S) S Mt+X+0.3Y+0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	0.30	0.30
3	CC 3 - Amb. 1 (SLU S) S Mt+X+0.3Y+0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	0.30	0.30
4	CC 4 - Amb. 1 (SLU S) S Mt+X+0.3Y-0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	0.30	-0.30
5	CC 5 - Amb. 1 (SLU S) S Mt+X+0.3Y-0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	0.30	-0.30
6	CC 6 - Amb. 1 (SLU S) S Mt+X+0.3Y-0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	0.30	-0.30
7	CC 7 - Amb. 1 (SLU S) S Mt+X-0.3Y+0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	-0.30	0.30
8	CC 8 - Amb. 1 (SLU S) S Mt+X-0.3Y+0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	-0.30	0.30
9	CC 9 - Amb. 1 (SLU S) S Mt+X-0.3Y+0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	-0.30	0.30
10	CC 10 - Amb. 1 (SLU S) S Mt+X-0.3Y-0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30
11	CC 11 - Amb. 1 (SLU S) S Mt+X-0.3Y-0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30
12	CC 12 - Amb. 1 (SLU S) S Mt+X-0.3Y-0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30
13	CC 13 - Amb. 1 (SLU S) S Mt+0.3X+Y+0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	1.00	0.30
14	CC 14 - Amb. 1 (SLU S) S Mt+0.3X+Y+0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	1.00	0.30
15	CC 15 - Amb. 1 (SLU S) S Mt+0.3X+Y+0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	1.00	0.30
16	CC 16 - Amb. 1 (SLU S) S Mt+0.3X+Y-0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	1.00	-0.30
17	CC 17 - Amb. 1 (SLU S) S Mt+0.3X+Y-0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	1.00	-0.30
18	CC 18 - Amb. 1 (SLU S) S Mt+0.3X+Y-0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	1.00	-0.30
19	CC 19 - Amb. 1 (SLU S) S Mt-0.3X+Y+0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	1.00	0.30
20	CC 20 - Amb. 1 (SLU S) S Mt-0.3X+Y+0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	1.00	0.30
21	CC 21 - Amb. 1 (SLU S) S Mt-0.3X+Y+0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	1.00	0.30
22	CC 22 - Amb. 1 (SLU S) S Mt-0.3X+Y-0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	1.00	-0.30
23	CC 23 - Amb. 1 (SLU S) S Mt-0.3X+Y-0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	1.00	-0.30
24	CC 24 - Amb. 1 (SLU S) S Mt-0.3X+Y-0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	1.00	-0.30
25	CC 25 - Amb. 1 (SLU S) S Mt+0.3X+0.3Y+Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	0.30	1.00
26	CC 26 - Amb. 1 (SLU S) S Mt+0.3X+0.3Y+Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	0.30	1.00
27	CC 27 - Amb. 1 (SLU S) S Mt+0.3X+0.3Y+Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	0.30	1.00
28	CC 28 - Amb. 1 (SLU S) S Mt+0.3X-0.3Y+Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	-0.30	1.00
29	CC 29 - Amb. 1 (SLU S) S Mt+0.3X-0.3Y+Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	-0.30	1.00
30	CC 30 - Amb. 1 (SLU S) S Mt+0.3X-0.3Y+Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	0.30	-0.30	1.00
31	CC 31 - Amb. 1 (SLU S) S Mt-0.3X+0.3Y+Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	0.30	1.00
32	CC 32 - Amb. 1 (SLU S) S Mt-0.3X+0.3Y+Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	0.30	1.00
33	CC 33 - Amb. 1 (SLU S) S Mt-0.3X+0.3Y+Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	0.30	1.00
34	CC 34 - Amb. 1 (SLU S) S Mt-0.3X-0.3Y+Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	-0.30	1.00
35	CC 35 - Amb. 1 (SLU S) S Mt-0.3X-0.3Y+Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	-0.30	1.00
36	CC 36 - Amb. 1 (SLU S) S Mt-0.3X-0.3Y+Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	1.00	-0.30	-0.30	1.00
37	CC 37 - Amb. 1 (SLU S) S -Mt+X+0.3Y+0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	0.30	0.30
38	CC 38 - Amb. 1 (SLU S) S -Mt+X+0.3Y+0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	0.30	0.30
39	CC 39 - Amb. 1 (SLU S) S -Mt+X+0.3Y+0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	0.30	0.30
40	CC 40 - Amb. 1 (SLU S) S -Mt+X+0.3Y-0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	0.30	-0.30
41	CC 41 - Amb. 1 (SLU S) S -Mt+X+0.3Y-0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	0.30	-0.30
42	CC 42 - Amb. 1 (SLU S) S -Mt+X+0.3Y-0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	0.30	-0.30
43	CC 43 - Amb. 1 (SLU S) S -Mt+X-0.3Y+0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	-0.30	0.30
44	CC 44 - Amb. 1 (SLU S) S -Mt+X-0.3Y+0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	-0.30	0.30
45	CC 45 - Amb. 1 (SLU S) S -Mt+X-0.3Y+0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	-0.30	0.30
46	CC 46 - Amb. 1 (SLU S) S -Mt+X-0.3Y-0.3Z	SLV	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	-0.30	-0.30
47	CC 47 - Amb. 1 (SLU S) S -Mt+X-0.3Y-0.3Z	SLD	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30	0.00	0.60	1.00	0.60	1.00	0.15	0.00	-1.00	1.00	-0.30	-0.30
48	CC 48 - Amb. 1 (SLU S) S -Mt+X-0.3Y-0.3Z	SLO	L	N	1.00	1.00	1.00	0.15	0.60	0.15	0.60	0.30											

3	24.91	14.25	10.81	82953.40	12867300.00	4	24.90	14.38	14.66	77695.70	11841000.00
5	24.91	14.38	18.56	77563.60	11824100.00	6	24.91	14.39	22.46	77543.80	11816500.00
7	24.91	14.39	26.36	77543.80	11816500.00	8	24.91	14.39	30.26	77543.80	11816500.00
9	25.62	14.40	34.16	82580.60	10829500.00						

Totali masse impalcati

Mo	Jpz
<KG>	<KG*mq>
661767.00	97983600.00

Elenco masse nodi

Simbologia

Nodo = Numero del nodo
 Mo = Massa orizzontale
 Mz = Massa in dir. Z

Nodo	Mo	Mz												
<KG>	<KG>	<KG>												
-14878	12.51	12.51	-14877	12.51	12.51	-14876	12.51	12.51	-14875	12.51	12.51	-14874	12.51	12.51
-14873	12.51	12.51	-14872	12.51	12.51	-14871	12.51	12.51	-14870	12.51	12.51	-14869	12.51	12.51
-14868	12.51	12.51	-14867	12.51	12.51	-14866	12.51	12.51	-14865	12.51	12.51	-14864	12.51	12.51
-14863	12.51	12.51	-14862	12.51	12.51	-14861	12.51	12.51	-14860	12.51	12.51	-14859	12.51	12.51
-14858	12.51	12.51	-14857	12.51	12.51	-14856	12.51	12.51	-14855	12.51	12.51	-14854	12.51	12.51
-14853	12.51	12.51	-14852	12.51	12.51	-14851	12.51	12.51	-14850	12.51	12.51	-14849	12.51	12.51
-14848	12.51	12.51	-14847	12.51	12.51	-14846	12.51	12.51	-14845	12.51	12.51	-14844	12.51	12.51
-14843	12.51	12.51	-14842	12.51	12.51	-14841	12.51	12.51	-14840	12.51	12.51	-14839	12.51	12.51
-14838	12.51	12.51	-14837	12.51	12.51	-14836	12.51	12.51	-14835	12.51	12.51	-14834	12.51	12.51
-14833	12.51	12.51	-14832	12.51	12.51	-14831	12.51	12.51	-14830	12.51	12.51	-14829	54.63	54.63
-14828	54.63	54.63	-14827	54.63	54.63	-14826	54.63	54.63	-14825	54.63	54.63	-14824	54.63	54.63
-14823	54.63	54.63	-14822	54.63	54.63	-14821	54.63	54.63	-14820	54.63	54.63	-14819	54.63	54.63
-14818	54.63	54.63	-14817	54.63	54.63	-14816	54.63	54.63	-14815	0.00	123.58	-14814	0.00	123.58
-14813	0.00	123.58	-14812	0.00	123.58	-14811	0.00	123.58	-14810	0.00	123.58	-14809	0.00	123.58
-14808	13.04	13.04	-14807	13.04	13.04	-14806	13.04	13.04	-14805	13.04	13.04	-14804	13.04	13.04
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-14133	20.87	20.87	-14132	11.24	11.24	-14131	8.86	8.86	-14130	15.01	15.01	-14129	14.58	14.58
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-13898 32.70	32.70	-13897 32.30	32.30	-13896 32.70	32.70	-13895 32.30	32.30	-13894 35.94	35.94
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-10938 26.09 26.09	-10937 47.83 47.83	-10936 47.83 47.83	-10935 26.09 26.09	-10934 26.09 26.09
-10933 26.09 26.09	-10932 13.04 13.04	-10931 13.04 13.04	-10930 26.09 26.09	-10929 26.09 26.09
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-10683 14.58 14.58	-10682 16.86 16.86	-10681 18.06 18.06	-10680 20.88 20.88	-10679 8.83 8.83
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-10608 17.14 17.14	-10607 27.84 27.84	-10606 21.30 21.30	-10605 29.86 29.86	-10604 18.61 18.61
-10603 19.17 19.17	-10602 20.97 20.97	-10601 21.55 21.55	-10600 24.51 24.51	-10599 28.80 28.80
-10598 22.51 22.51	-10597 20.09 20.09	-10596 20.34 20.34	-10595 19.35 19.35	-10594 19.59 19.59
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-10573 59.75 59.75	-10572 29.39 29.39	-10571 26.47 26.47	-10570 26.42 26.42	-10569 24.78 24.78
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-10553 28.39 28.39	-10552 9.54 9.54	-10551 5.15 5.15	-10550 5.15 5.15	-10549 5.15 5.15
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-10533 16.14 16.14	-10532 15.68 15.68	-10531 18.13 18.13	-10530 19.42 19.42	-10529 24.01 24.01

857	0.00	380.86	858	0.00	64.22	859	0.00	64.22	860	0.00	64.22	861	0.00	64.22
862	0.00	310.91	863	0.00	315.09	901	0.00	183.66	902	0.00	185.31	903	0.00	1280.23
904	0.00	2571.69	905	0.00	2769.26	906	0.00	2238.78	907	0.00	2817.87	908	0.00	2955.49
909	0.00	1664.02	910	0.00	1674.03	913	0.00	3466.46	915	0.00	4055.14	917	0.00	3818.71
918	0.00	3818.71	920	0.00	4055.14	923	0.00	2262.71	924	0.00	1674.03	927	0.00	3466.46
929	0.00	4055.14	931	0.00	3818.71	932	0.00	3818.71	934	0.00	4055.14	937	0.00	2262.71
938	0.00	1271.46	939	0.00	2571.69	940	0.00	2955.49	941	0.00	2817.87	942	0.00	2817.87
943	0.00	2955.49	944	0.00	1655.26	945	0.00	22.70	946	0.00	83.99	947	0.00	83.99
948	0.00	22.70	949	0.00	43.86	950	0.00	45.46	951	0.00	22.70	952	0.00	83.13
953	0.00	146.29	954	0.00	88.54	955	0.00	768.04	956	0.00	203.38	957	0.00	207.57
958	0.00	64.22	959	0.00	64.22	960	0.00	64.22	961	0.00	64.22	962	0.00	137.62
963	0.00	141.79												

Totali masse nodi

Mo Mz
 <KG> <KG>
 266245.00 923680.00

Elenco forze sismiche di impalcato allo SLO**Simbologia**

Imp. = Numero dell'impalcato
 cx = Coeff. c in dir. X
 cy = Coeff. c in dir. Y
 Mz = Momento intorno all'asse Z

Imp.	cx	cy	Mz
<kgm>			
1	0.02	0.02	27284.00
2	0.00	0.00	1980.03
3	0.06	0.06	74011.10
4	0.07	0.07	94008.70
5	0.09	0.09	118815.00
6	0.11	0.11	143745.00
7	0.13	0.13	168705.00
8	0.15	0.15	193666.00
9	0.18	0.18	232827.00

Totali forze sismiche

Mz
 <kgm>
 1055040.00

Elenco forze sismiche di impalcato allo SLD

Imp.	cx	cy	Mz
<kgm>			
1	0.02	0.02	34081.60
2	0.00	0.00	2473.34
3	0.06	0.06	92450.50
4	0.07	0.07	117430.00
5	0.09	0.09	148417.00
6	0.11	0.11	179558.00
7	0.13	0.13	210737.00
8	0.15	0.15	241916.00
9	0.18	0.18	290834.00

Totali forze sismiche

Mz
 <kgm>
 1317900.00

Elenco forze sismiche di impalcato allo SLV

Imp.	cx	cy	Mz
<kgm>			
1	0.02	0.02	77732.00
2	0.00	0.00	5641.11
3	0.06	0.06	210858.00
4	0.07	0.07	267830.00
5	0.09	0.09	338504.00
6	0.11	0.11	409530.00
7	0.13	0.13	480640.00
8	0.15	0.15	551752.00
9	0.18	0.18	663323.00

Totali forze sismiche

Mz
 <kgm>
 3005810.00

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione**Simbologia**

Modo = Numero del modo di vibrare
 C = * indica che il modo è stato considerato

Per. = Periodo
 Diff. = Minima differenza percentuale dagli altri periodi
 Φ_x = Coefficiente di partecipazione in dir. X
 Φ_y = Coefficiente di partecipazione in dir. Y
 Φ_z = Coefficiente di partecipazione in dir. Z
 %Mx = Percentuale massa partecipante in dir. X
 %My = Percentuale massa partecipante in dir. Y
 %Mz = Percentuale massa partecipante in dir. Z
 %Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φ_x	Φ_y	Φ_z	%Mx	%My	%Mz	%Jpz
1	*	2.00	21.84	-709.59	2.31	-0.67	54.26	0.00	0.00	0.01
2	*	1.64	0.79	-6.55	271.88	0.17	0.00	7.97	0.00	0.25
3	*	1.63	0.77	-9.69	107.30	0.82	0.01	1.24	0.00	0.02
4	*	1.62	0.77	3.86	78.96	-0.75	0.00	0.67	0.00	0.04
5	*	1.58	2.32	-7.85	-695.33	3.62	0.01	52.10	0.00	0.45
6	*	1.25	26.31	-7.94	62.09	-0.20	0.01	0.42	0.00	70.31
7	*	0.81	33.94	-2.82	-66.42	3.31	0.00	0.48	0.00	0.00
8	*	0.61	7.14	-294.67	4.89	5.84	9.36	0.00	0.00	0.00
9		0.57	7.14	-0.11	-49.81	-0.03	0.00	0.27	0.00	0.00
10	*	0.51	0.39	9.75	-94.16	-0.23	0.01	0.96	0.00	0.00
11	*	0.51	0.39	304.69	3.23	-2.28	10.00	0.00	0.00	0.00
12	*	0.46	9.85	-0.07	-294.59	-1.69	0.00	9.35	0.00	0.02
13		0.42	2.29	-3.77	0.08	61.26	0.00	0.00	0.41	0.00
14		0.41	2.29	4.98	0.04	45.55	0.00	0.00	0.22	0.00
15		0.40	2.60	3.45	0.29	6.49	0.00	0.00	0.00	0.00
16	*	0.37	1.61	2.81	4.38	0.55	0.00	0.00	0.00	12.10
17		0.37	1.61	1.23	-0.36	-22.13	0.00	0.00	0.05	0.00
18		0.34	3.41	0.55	-0.61	-24.69	0.00	0.00	0.07	0.00
19		0.33	3.30	-1.46	-70.86	1.72	0.00	0.54	0.00	0.00
20		0.32	1.06	-0.00	-2.34	-0.05	0.00	0.00	0.00	0.01
21		0.32	0.28	46.85	0.22	0.90	0.24	0.00	0.00	0.00
22		0.32	0.28	-0.50	3.40	0.06	0.00	0.00	0.00	0.02
23		0.32	0.81	-0.05	-3.50	-0.11	0.00	0.00	0.00	0.04
24		0.29	4.18	-0.19	2.35	-0.25	0.00	0.00	0.00	0.02
25		0.28	1.20	-0.11	5.22	-0.31	0.00	0.00	0.00	0.01
26		0.28	1.20	-1.33	0.39	-20.24	0.00	0.00	0.04	0.00
27	*	0.27	1.76	-69.38	0.85	1.57	0.52	0.00	0.00	0.00
28		0.27	1.43	0.44	-11.97	0.34	0.00	0.02	0.00	0.00
29		0.27	0.33	-0.62	0.54	21.68	0.00	0.00	0.05	0.00
30		0.26	0.33	2.35	1.08	22.18	0.00	0.00	0.05	0.00
31	*	0.26	2.93	-0.04	166.21	-3.71	0.00	2.98	0.00	0.00
32		0.22	0.13	7.06	0.68	-1.29	0.01	0.00	0.00	0.08
33		0.22	0.02	2.54	-44.48	1.13	0.00	0.21	0.00	0.00
34		0.22	0.02	0.87	2.05	0.66	0.00	0.00	0.00	0.00
35	*	0.21	1.64	74.97	0.69	-5.40	0.61	0.00	0.00	1.60
36		0.21	0.35	29.55	-15.96	58.71	0.09	0.03	0.37	0.00
37	*	0.21	0.35	145.48	-0.84	3.83	2.28	0.00	0.00	0.47
38		0.20	1.38	1.18	16.72	-45.42	0.00	0.03	0.22	0.00
39		0.20	1.01	0.58	7.25	-15.42	0.00	0.01	0.03	0.00
40		0.20	0.27	1.49	2.52	-4.83	0.00	0.00	0.00	0.00
41		0.20	0.27	-6.76	-17.67	-1.77	0.00	0.03	0.00	0.19
42		0.20	0.43	-0.19	5.19	-3.89	0.00	0.00	0.00	0.01
43		0.20	0.43	-3.62	-3.89	6.27	0.00	0.00	0.00	0.01
44	*	0.18	1.61	18.59	29.18	-340.75	0.04	0.09	12.57	0.00
45		0.18	1.61	-0.46	38.03	-21.84	0.00	0.16	0.05	0.11
46		0.18	0.11	-28.01	14.67	-12.75	0.08	0.02	0.02	0.00
47	*	0.18	0.11	9.57	-120.12	181.42	0.01	1.55	3.56	0.00
48		0.18	0.12	8.57	-0.26	-2.14	0.01	0.00	0.00	0.00
49		0.18	0.05	4.77	2.64	-0.16	0.00	0.00	0.00	0.00
50		0.18	0.05	-4.54	-1.60	1.33	0.00	0.00	0.00	0.00
51		0.18	0.02	-2.16	1.36	0.78	0.00	0.00	0.00	0.00
52		0.18	0.02	2.06	-0.31	-0.54	0.00	0.00	0.00	0.00
53		0.18	0.12	4.03	-10.50	-4.65	0.00	0.01	0.00	0.00
54	*	0.18	0.57	7.31	83.39	211.41	0.01	0.75	4.84	0.00
55	*	0.17	0.57	-0.56	-59.92	239.46	0.00	0.39	6.21	0.00
56	*	0.17	2.29	-1.73	-25.10	-676.77	0.00	0.07	49.59	0.00
57	*	0.17	1.34	-67.72	-105.58	-44.69	0.49	1.20	0.22	0.01
58	*	0.16	1.34	-12.14	-3.85	-233.60	0.02	0.00	5.91	0.00
59		0.16	0.65	-4.02	-10.72	74.32	0.00	0.01	0.60	0.00
60		0.16	0.52	-1.87	-31.08	10.44	0.00	0.10	0.01	0.00
61	*	0.16	0.52	1.38	-103.65	39.82	0.00	1.16	0.17	0.00
62		0.16	0.54	-2.80	-39.68	-38.45	0.00	0.17	0.16	0.00
63		0.15	0.54	-0.02	-0.29	0.08	0.00	0.00	0.00	0.00
64	*	0.15	0.66	-10.42	27.78	122.72	0.01	0.08	1.63	0.00
65		0.15	0.66	4.79	8.91	-79.21	0.00	0.01	0.68	0.01
66	*	0.15	0.78	5.82	12.21	120.44	0.00	0.02	1.57	0.00
67	*	0.15	0.51	-8.30	-25.58	-103.72	0.01	0.07	1.16	0.02
68		0.15	0.35	0.02	0.07	0.51	0.00	0.00	0.00	0.00
69		0.15	0.35	7.95	14.69	-28.18	0.01	0.02	0.09	0.01
70		0.14	1.34	-24.86	14.17	-20.05	0.07	0.02	0.04	0.00
71		0.14	1.15	-11.98	-2.71	-47.77	0.02	0.00	0.25	0.01
72		0.14	0.11	-22.38	-1.84	20.78	0.05	0.00	0.05	0.17
73		0.14	0.11	28.20	0.43	10.82	0.09	0.00	0.01	0.00
74		0.14	0.38	-24.51	5.80	45.64	0.06	0.00	0.23	0.18
75		0.14	1.28	-11.49	3.42	-12.08	0.01	0.00	0.02	0.80
76	*	0.13	0.31	97.57	-50.48	-33.87	1.03	0.27	0.12	0.05
77		0.13	0.14	-45.75	-14.30	33.00	0.23	0.02	0.12	0.01
78		0.13	0.14	-63.46	9.21	8.49	0.43	0.01	0.01	0.00
79		0.13	1.53	-29.63	-1.67	-2.94	0.09	0.00	0.00	0.00
80		0.13	0.54	14.40	-16.84	-26.47	0.02	0.03	0.08	0.02
81		0.13	0.16	0.67	-24.82	-19.48	0.00	0.07	0.04	0.00
82		0.13	0.16	0.68	-0.30	0.80	0.00	0.00	0.00	0.00
83		0.13	0.09	18.48	57.28	57.93	0.04	0.35	0.36	0.00
84		0.13	0.09	-36.95	16.73	20.32	0.15	0.03	0.04	0.02
85		0.12	0.51	-41.32	20.89	18.16	0.18	0.05	0.04	0.00
86		0.12	0.15	-1.22	-4.04	-0.09	0.00	0.00	0.00	0.00

87	0.12	0.15	-0.55	-0.79	0.53	0.00	0.00	0.00	0.00
88	0.12	0.52	7.87	-42.29	-8.90	0.01	0.19	0.01	0.00
89	* 0.12	1.00	2.35	4.37	-123.91	0.00	0.00	1.66	0.00
90	0.12	0.92	-0.44	-2.41	-4.20	0.00	0.00	0.00	0.00
91	0.12	0.83	43.96	3.25	9.68	0.21	0.00	0.01	0.01
92	0.12	0.83	0.36	-14.78	-8.45	0.00	0.02	0.01	0.00
93	0.11	0.10	25.19	1.38	12.54	0.07	0.00	0.02	0.00
94	0.11	0.10	5.67	10.63	31.77	0.00	0.01	0.11	0.00
95	0.11	0.21	-6.64	6.93	9.20	0.00	0.01	0.01	0.00
96	* 0.11	0.09	-80.23	0.62	-4.05	0.69	0.00	0.00	0.00
97	* 0.11	0.06	-71.92	1.13	-0.18	0.56	0.00	0.00	0.00
98	* 0.11	0.06	80.78	2.02	11.55	0.70	0.00	0.01	0.00
99	0.11	0.54	1.22	7.21	7.55	0.00	0.01	0.01	0.00
100	0.11	0.16	8.69	7.11	20.33	0.01	0.01	0.04	0.00
101	0.11	0.16	-35.37	11.46	29.97	0.13	0.01	0.10	0.00
102	0.11	0.25	-11.61	31.78	81.14	0.01	0.11	0.71	0.00
103	0.11	0.50	-7.14	-2.20	-1.87	0.01	0.00	0.00	0.00
104	0.11	0.52	-64.08	-5.29	0.95	0.44	0.00	0.00	0.00
105	0.11	0.40	-23.83	3.18	57.80	0.06	0.00	0.36	0.00
106	0.11	0.40	-5.06	75.35	11.01	0.00	0.61	0.01	0.00
107	0.11	0.57	-0.51	1.59	1.14	0.00	0.00	0.00	0.00
108	0.11	1.16	-28.94	6.66	3.44	0.09	0.00	0.00	0.00
109	0.10	1.16	-2.39	-10.04	-10.31	0.00	0.01	0.01	0.00
110	0.10	0.44	-18.50	-22.64	24.44	0.04	0.06	0.06	0.00
111	* 0.10	0.44	73.60	-2.23	51.52	0.58	0.00	0.29	0.00
112	0.10	0.68	-61.78	7.79	-10.96	0.41	0.01	0.01	0.01
113	0.10	0.62	-1.00	0.51	-0.35	0.00	0.00	0.00	0.00
114	0.10	0.62	-4.36	62.73	26.90	0.00	0.42	0.08	0.00
115	0.10	0.01	-10.36	1.82	17.21	0.01	0.00	0.03	0.00
116	0.10	0.01	-11.99	1.50	17.91	0.02	0.00	0.03	0.00
117	0.10	0.29	-1.84	-3.81	-4.70	0.00	0.00	0.00	0.05
118	0.10	0.29	1.57	-6.50	8.13	0.00	0.00	0.01	0.20
119	0.10	1.23	4.23	-0.17	9.13	0.00	0.00	0.01	0.00
120	0.10	0.30	1.75	8.38	13.07	0.00	0.01	0.02	0.01
121	0.09	0.30	2.38	4.81	3.82	0.00	0.00	0.00	0.07
122	0.09	0.13	-2.47	2.61	-16.15	0.00	0.00	0.03	0.00
123	0.09	0.13	0.63	4.30	0.35	0.00	0.00	0.00	0.00
124	0.09	0.08	1.48	-3.51	14.45	0.00	0.00	0.02	0.00
125	0.09	0.08	2.61	2.57	-7.24	0.00	0.00	0.01	0.00
126	0.09	0.26	-1.09	-6.72	-1.34	0.00	0.00	0.00	0.00
127	0.09	0.26	-1.10	-1.11	3.85	0.00	0.00	0.00	0.00
128	0.09	0.16	-1.65	-7.73	-1.65	0.00	0.01	0.00	0.00
129	0.09	0.16	0.00	-0.69	-1.25	0.00	0.00	0.00	0.00
130	0.09	0.34	-2.78	1.73	0.91	0.00	0.00	0.00	0.00
131	0.09	0.34	3.68	-5.62	-0.86	0.00	0.00	0.00	0.00
132	0.09	0.39	-1.02	73.24	-0.43	0.00	0.58	0.00	0.16
133	0.09	0.39	1.93	-7.90	-1.44	0.00	0.01	0.00	0.00
134	0.09	0.06	7.20	-5.26	-16.34	0.01	0.00	0.03	0.00
135	0.09	0.06	-0.66	22.23	0.69	0.00	0.05	0.00	0.05
136	0.09	0.21	5.78	-11.61	-12.46	0.00	0.01	0.02	0.01
137	0.09	0.15	-0.85	-3.89	5.79	0.00	0.00	0.00	0.00
138	0.09	0.10	1.17	46.71	-2.96	0.00	0.24	0.00	0.53
139	0.09	0.10	0.78	3.56	1.51	0.00	0.00	0.00	0.00
140	0.09	0.13	4.06	2.03	-9.53	0.00	0.00	0.01	0.00
141	0.09	0.11	2.47	-1.45	-6.93	0.00	0.00	0.01	0.01
142	0.09	0.03	-0.85	0.25	-0.03	0.00	0.00	0.00	0.00
143	0.09	0.03	-1.09	0.39	1.57	0.00	0.00	0.00	0.03
144	0.08	0.02	0.16	0.26	-0.98	0.00	0.00	0.00	0.00
145	0.08	0.02	1.81	-4.30	-10.87	0.00	0.00	0.01	0.00
146	0.08	0.22	-2.78	12.47	3.15	0.00	0.02	0.00	0.00
147	0.08	0.22	0.02	3.29	0.76	0.00	0.00	0.00	0.00
148	0.08	1.04	2.46	6.28	4.14	0.00	0.00	0.00	0.00
149	0.08	0.24	0.13	-1.36	1.93	0.00	0.00	0.00	0.00
150	0.08	0.17	2.22	-17.57	-0.17	0.00	0.03	0.00	0.00
151	0.08	0.17	-1.39	-30.87	3.43	0.00	0.10	0.00	0.01
152	0.08	0.25	-7.76	38.75	8.40	0.01	0.16	0.01	0.00
153	0.08	0.25	-5.86	4.21	-11.76	0.00	0.00	0.01	0.01
154	0.08	0.27	1.77	9.12	2.48	0.00	0.01	0.00	0.00
155	0.08	0.78	16.11	-5.12	7.58	0.03	0.00	0.01	0.00
156	0.08	0.78	-0.24	-74.35	-1.26	0.00	0.60	0.00	0.00
157	0.08	0.28	-1.70	-14.01	32.49	0.00	0.02	0.11	0.00
158	0.08	0.21	18.43	-36.31	-2.78	0.04	0.14	0.00	0.00
159	0.08	0.21	-9.59	-13.43	14.52	0.01	0.02	0.02	0.00
160	0.08	0.61	-15.73	13.76	0.04	0.03	0.02	0.00	0.00
161	0.07	0.09	3.74	-20.35	-0.47	0.00	0.04	0.00	0.00
162	0.07	0.07	13.58	35.55	30.12	0.02	0.14	0.10	0.00
163	0.07	0.07	-6.74	-6.53	-31.11	0.00	0.00	0.10	0.01
164	0.07	0.45	-1.58	2.41	-0.63	0.00	0.00	0.00	0.00
165	0.07	0.45	2.12	-5.79	-0.84	0.00	0.00	0.00	0.01
166	* 0.07	1.03	145.43	6.60	0.30	2.28	0.00	0.00	0.01
167	0.07	0.34	16.63	-6.32	-0.11	0.03	0.00	0.00	0.06
168	0.07	0.06	4.74	-8.86	-4.04	0.00	0.01	0.00	0.02
169	0.07	0.06	7.32	13.61	-19.20	0.01	0.02	0.04	0.14
170	0.07	0.24	1.84	5.60	18.91	0.00	0.00	0.04	0.14
171	0.07	0.22	-0.85	-1.81	-2.14	0.00	0.00	0.00	0.00
172	0.07	0.15	-2.24	-11.88	2.33	0.00	0.02	0.00	0.04
173	0.07	0.10	39.09	-37.97	5.87	0.16	0.16	0.00	0.00
174	0.07	0.10	17.05	2.71	6.62	0.03	0.00	0.00	0.00
175	0.07	0.50	-35.70	4.15	2.98	0.14	0.00	0.00	0.00
176	0.07	0.09	-20.64	11.96	-10.64	0.05	0.02	0.01	0.00
177	0.07	0.09	29.56	20.90	-11.39	0.09	0.05	0.01	0.00
178	0.07	0.20	-19.49	-50.49	-11.89	0.04	0.27	0.02	0.00
179	0.07	0.26	-51.16	9.59	-15.45	0.28	0.01	0.03	0.00
180	0.07	0.26	-20.54	-11.70	-9.08	0.05	0.01	0.01	0.00
181	0.07	0.08	-24.63	1.77	-9.48	0.07	0.00	0.01	0.00
182	0.07	0.02	14.75	-0.37	-8.28	0.02	0.00	0.01	0.00
183	0.07	0.02	4.94	13.96	2.32	0.00	0.02	0.00	0.00
184	0.07	0.06	40.32	-0.76	-12.14	0.18	0.00	0.02	0.00

185	0.07	0.06	-1.03	-6.06	6.71	0.00	0.00	0.00	0.00
186	0.07	0.32	2.05	-5.54	-2.22	0.00	0.00	0.00	0.00
187	0.07	0.37	-5.34	-9.50	25.28	0.00	0.01	0.07	0.00
188	0.07	0.37	-20.45	-10.53	-2.24	0.05	0.01	0.00	0.00
189	0.07	0.15	9.68	20.40	-27.02	0.01	0.04	0.08	0.00
190	0.07	0.05	-21.96	7.64	-2.16	0.05	0.01	0.00	0.00
191	0.07	0.05	-0.34	-6.88	2.39	0.00	0.01	0.00	0.00
192	0.07	0.10	5.98	5.39	-2.79	0.00	0.00	0.00	0.00
193	0.07	0.10	0.41	9.58	0.37	0.00	0.01	0.00	0.00
194	0.07	0.26	-1.19	13.38	6.09	0.00	0.02	0.00	0.00
195	0.07	0.20	0.23	-2.72	7.51	0.00	0.00	0.01	0.00
196	0.07	0.20	-0.43	0.64	1.11	0.00	0.00	0.00	0.00
197	0.06	0.20	51.99	24.90	-1.21	0.29	0.07	0.00	0.00
198	0.06	0.28	-1.19	-5.50	-1.88	0.00	0.00	0.00	0.00
199	0.06	0.05	3.61	13.29	-3.56	0.00	0.02	0.00	0.00
200	* 0.06	0.05	-20.36	-89.34	-5.58	0.04	0.86	0.00	0.01
201	* 0.06	0.17	-71.71	15.99	-3.83	0.55	0.03	0.00	0.00
202	0.06	0.17	-58.08	-6.00	7.38	0.36	0.00	0.01	0.00
203	0.06	0.33	-15.47	-2.31	-6.82	0.03	0.00	0.01	0.00
204	0.06	0.45	-8.74	3.91	7.12	0.01	0.00	0.01	0.00
205	0.06	0.28	-3.59	2.42	-19.28	0.00	0.00	0.04	0.01
206	0.06	0.28	0.46	18.74	1.49	0.00	0.04	0.00	0.00
207	0.06	0.15	-6.82	-34.42	-0.81	0.01	0.13	0.00	0.01
208	0.06	0.15	5.56	57.29	0.81	0.00	0.35	0.00	0.01
209	0.06	0.10	-15.73	66.06	8.44	0.03	0.47	0.01	0.01
210	0.06	0.10	-5.41	-9.33	9.29	0.00	0.01	0.01	0.00
211	0.06	0.80	11.11	-15.19	-1.11	0.01	0.02	0.00	0.00
212	0.06	0.29	-6.29	0.54	2.18	0.00	0.00	0.00	0.00
213	0.06	0.29	4.69	0.80	-1.29	0.00	0.00	0.00	0.00
214	0.06	0.20	-3.00	-5.85	-0.61	0.00	0.00	0.00	0.00
215	0.06	0.20	17.54	0.79	0.28	0.03	0.00	0.00	0.01
216	0.06	0.10	14.62	-22.99	-10.25	0.02	0.06	0.01	0.05
217	0.06	0.10	5.52	7.66	0.98	0.00	0.01	0.00	0.00
218	0.06	0.22	7.44	-0.66	9.49	0.01	0.00	0.01	0.01
219	0.06	0.22	0.68	-1.17	-0.11	0.00	0.00	0.00	0.01
220	0.06	0.36	2.52	-11.50	-1.97	0.00	0.01	0.00	0.88
221	0.06	0.22	5.32	-1.85	0.36	0.00	0.00	0.00	0.00
222	0.06	0.22	6.74	6.03	-1.04	0.00	0.00	0.00	0.00
223	0.06	0.39	31.35	1.11	-7.00	0.11	0.00	0.01	0.00
224	* 0.06	0.11	108.51	-1.90	-5.34	1.27	0.00	0.00	0.00
225	* 0.06	0.11	82.62	-23.60	-7.62	0.74	0.06	0.01	0.01
226	0.06	0.07	4.73	-0.35	-0.96	0.00	0.00	0.00	0.00
227	0.06	0.07	-3.25	0.88	-6.32	0.00	0.00	0.00	0.00
228	* 0.06	0.23	-30.95	-76.16	-13.56	0.10	0.63	0.02	0.02
229	* 0.06	0.56	-0.38	-138.23	-2.62	0.00	2.06	0.00	0.17
230	0.06	0.07	-6.25	3.29	7.76	0.00	0.00	0.01	0.00
231	0.06	0.07	-7.28	-32.31	15.41	0.01	0.11	0.03	0.12
232	0.06	0.54	-35.19	1.82	5.64	0.13	0.00	0.00	0.00
233	0.06	0.05	-12.04	-2.22	41.36	0.02	0.00	0.19	0.00
234	0.06	0.05	-12.79	-3.52	19.11	0.02	0.00	0.04	0.00
235	0.06	0.42	3.57	0.32	-5.29	0.00	0.00	0.00	0.00
236	0.06	0.42	-0.97	-0.01	0.51	0.00	0.00	0.00	0.00
237	0.05	0.41	10.19	-2.41	2.41	0.01	0.00	0.00	0.00
238	0.05	0.41	10.68	-8.70	14.20	0.01	0.01	0.02	0.02
239	0.05	0.57	12.33	1.58	51.77	0.02	0.00	0.29	0.00
240	0.05	0.57	3.71	1.20	3.05	0.00	0.00	0.00	0.01

Tot.cons.

86.20 85.45 89.57 85.60

Elenco coefficienti di risposta**Simbologia**

Modo = Numero del modo di vibrare

Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X

Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Sz = Coefficiente di risposta (moltiplicato per 100) in dir. Z

Stato limite di operatività

Modo	Sx	Sy	Sz
1	3.84	3.84	0.15
2	5.18	5.18	0.23
3	5.22	5.22	0.23
4	5.26	5.26	0.24
5	5.38	5.38	0.25
6	6.80	6.80	0.39
7	10.47	10.47	0.76
8	14.03	14.03	1.02
9	15.03	15.03	1.09
10	16.65	16.65	1.21
11	16.72	16.72	1.21
12	18.51	18.51	1.34
13	20.09	20.09	1.47
14	20.09	20.09	1.51
15	20.09	20.09	1.55
16	20.09	20.09	1.66
17	20.09	20.09	1.69
18	20.09	20.09	1.79
19	20.09	20.09	1.85
20	20.09	20.09	1.91
21	20.09	20.09	1.93
22	20.09	20.09	1.94
23	20.09	20.09	1.95
24	20.09	20.09	2.09

25	20.09	20.09	2.18
26	20.09	20.09	2.21
27	20.09	20.09	2.24
28	20.09	20.09	2.29
29	20.09	20.09	2.32
30	20.09	20.09	2.33
31	20.09	20.09	2.39
32	20.09	20.09	2.84
33	20.09	20.09	2.84
34	20.09	20.09	2.84
35	20.09	20.09	2.91
36	20.09	20.09	2.96
37	20.09	20.09	2.97
38	20.09	20.09	3.03
39	20.09	20.09	3.07
40	20.09	20.09	3.10
41	20.09	20.09	3.11
42	20.09	20.09	3.13
43	20.09	20.09	3.15
44	20.09	20.09	3.33
45	20.09	20.09	3.39
46	20.09	20.09	3.45
47	20.09	20.09	3.45
48	20.09	20.09	3.46
49	20.09	20.09	3.47
50	20.09	20.09	3.47
51	20.09	20.09	3.47
52	20.09	20.09	3.47
53	20.09	20.09	3.47

54	20.09	20.09	3.50
55	20.09	20.09	3.52
56	20.09	20.09	3.61
57	20.09	20.09	3.69
58	20.09	20.09	3.74
59	20.09	20.09	3.81
60	20.09	20.09	3.84
61	20.09	20.09	3.86
62	20.09	20.09	3.96
63	20.09	20.09	3.98
64	20.09	20.09	4.02
65	20.09	20.09	4.04
66	20.09	20.09	4.07
67	20.09	20.09	4.11
68	20.09	20.09	4.11
69	20.09	20.09	4.11
70	20.09	20.09	4.11
71	20.00	20.00	4.11
72	19.86	19.86	4.11
73	19.85	19.85	4.11
74	19.81	19.81	4.11
75	19.65	19.65	4.11
76	19.42	19.42	4.11
77	19.38	19.38	4.11
78	19.37	19.37	4.11
79	19.19	19.19	4.11
80	18.99	18.99	4.11
81	18.93	18.93	4.11
82	18.92	18.92	4.11

181	34.47	34.47	11.80	201	33.79	33.79	11.80	221	32.73	32.73	11.80
182	34.46	34.46	11.80	202	33.77	33.77	11.80	222	32.71	32.71	11.80
183	34.45	34.45	11.80	203	33.73	33.73	11.80	223	32.66	32.66	11.80
184	34.41	34.41	11.80	204	33.50	33.50	11.80	224	32.62	32.62	11.80
185	34.40	34.40	11.80	205	33.45	33.45	11.80	225	32.61	32.61	11.80
186	34.36	34.36	11.80	206	33.41	33.41	11.80	226	32.58	32.58	11.80
187	34.30	34.30	11.80	207	33.36	33.36	11.80	227	32.57	32.57	11.80
188	34.25	34.25	11.80	208	33.35	33.35	11.80	228	32.55	32.55	11.80
189	34.18	34.18	11.80	209	33.29	33.29	11.80	229	32.45	32.45	11.80
190	34.16	34.16	11.80	210	33.28	33.28	11.80	230	32.39	32.39	11.80
191	34.16	34.16	11.80	211	33.19	33.19	11.80	231	32.38	32.38	11.80
192	34.10	34.10	11.80	212	33.06	33.06	11.80	232	32.32	32.32	11.80
193	34.08	34.08	11.80	213	33.02	33.02	11.80	233	32.26	32.26	11.80
194	34.05	34.05	11.80	214	32.98	32.98	11.80	234	32.26	32.26	11.80
195	34.00	34.00	11.80	215	32.95	32.95	11.80	235	32.18	32.18	11.80
196	33.98	33.98	11.80	216	32.88	32.88	11.80	236	32.14	32.14	11.80
197	33.95	33.95	11.80	217	32.87	32.87	11.80	237	32.03	32.03	11.80
198	33.91	33.91	11.80	218	32.84	32.84	11.80	238	31.98	31.98	11.80
199	33.87	33.87	11.80	219	32.81	32.81	11.80	239	31.91	31.91	11.80
200	33.87	33.87	11.80	220	32.77	32.77	11.80	240	31.85	31.85	11.80

5.2. PRESSIONI SUL TERRENO

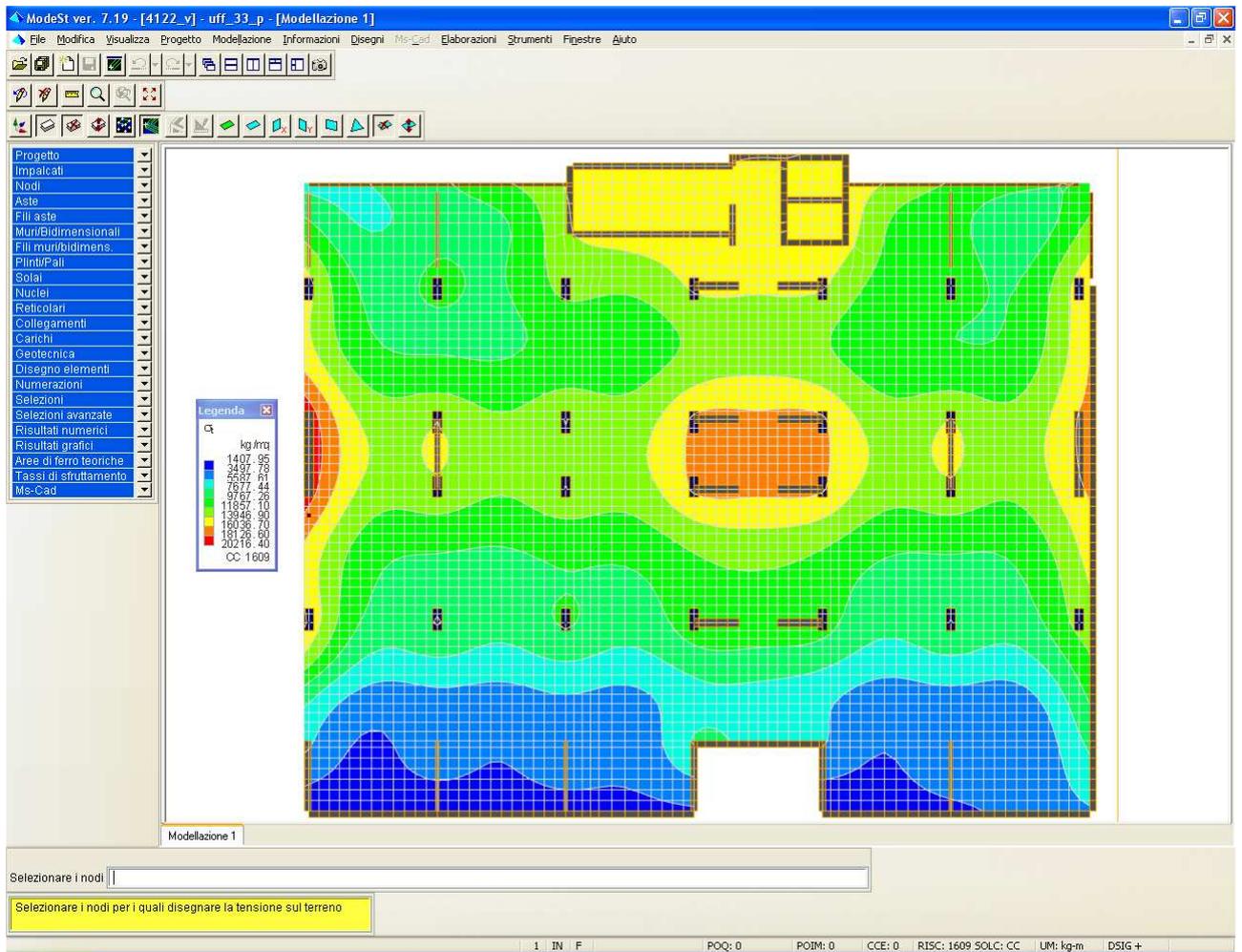
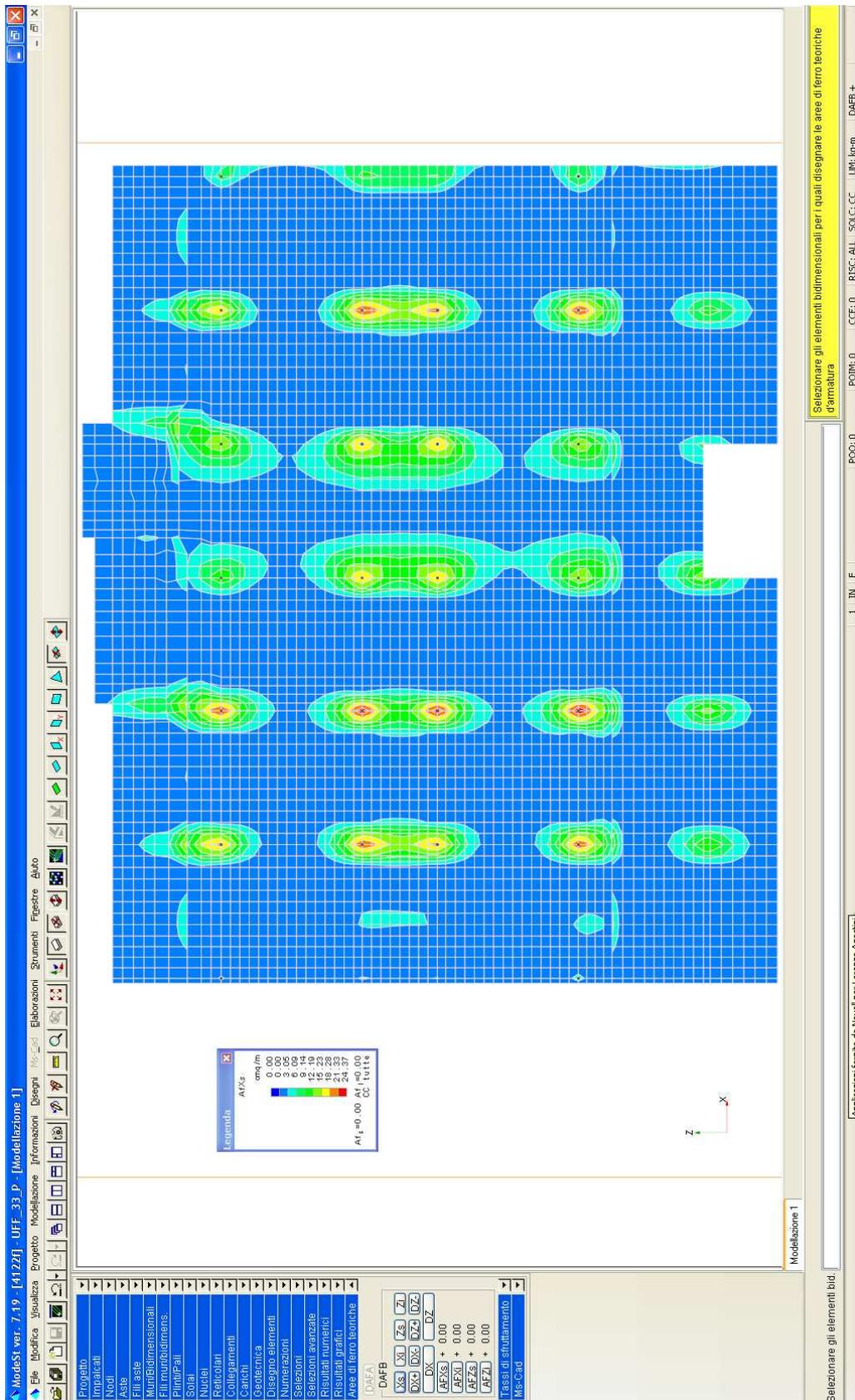
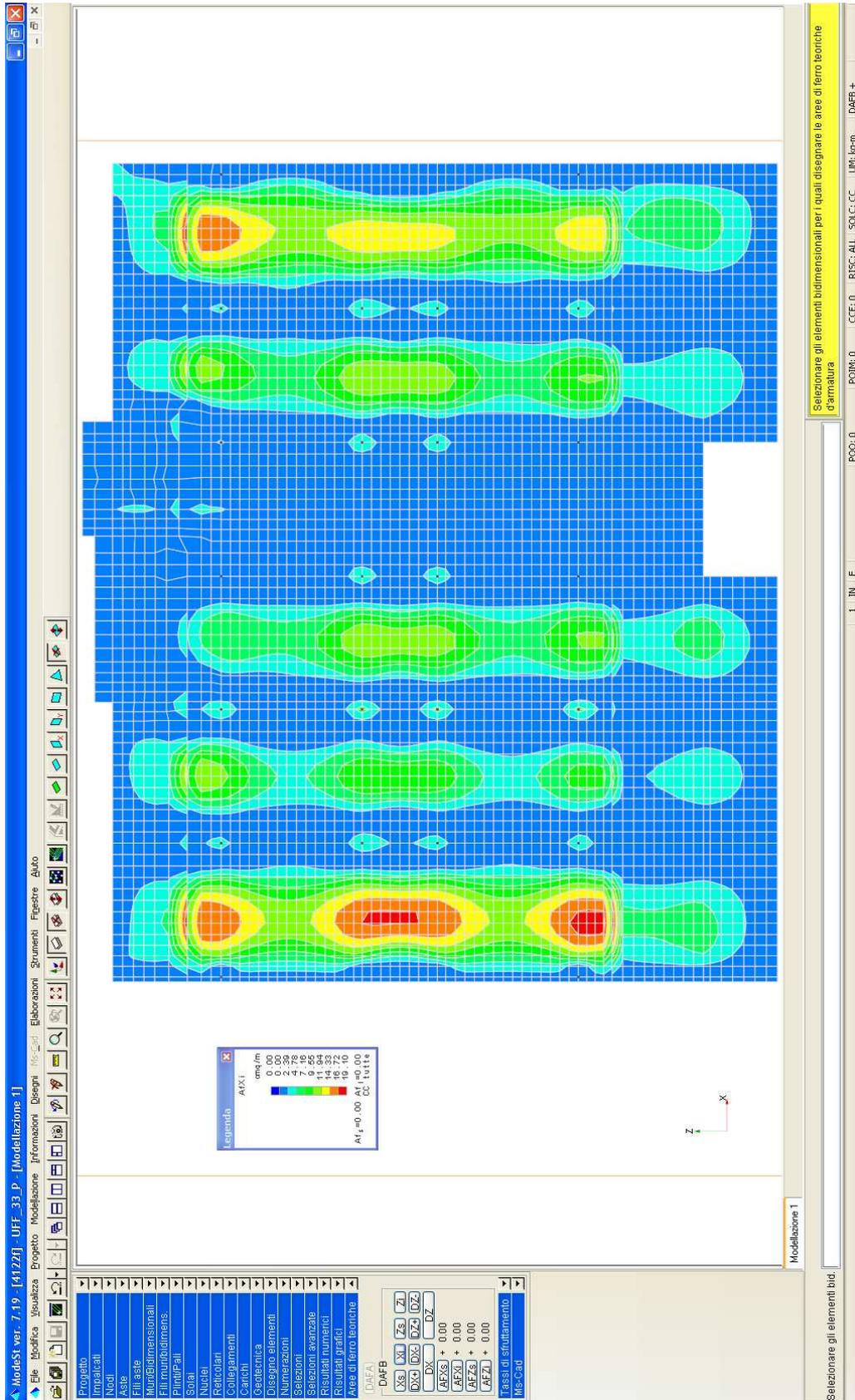
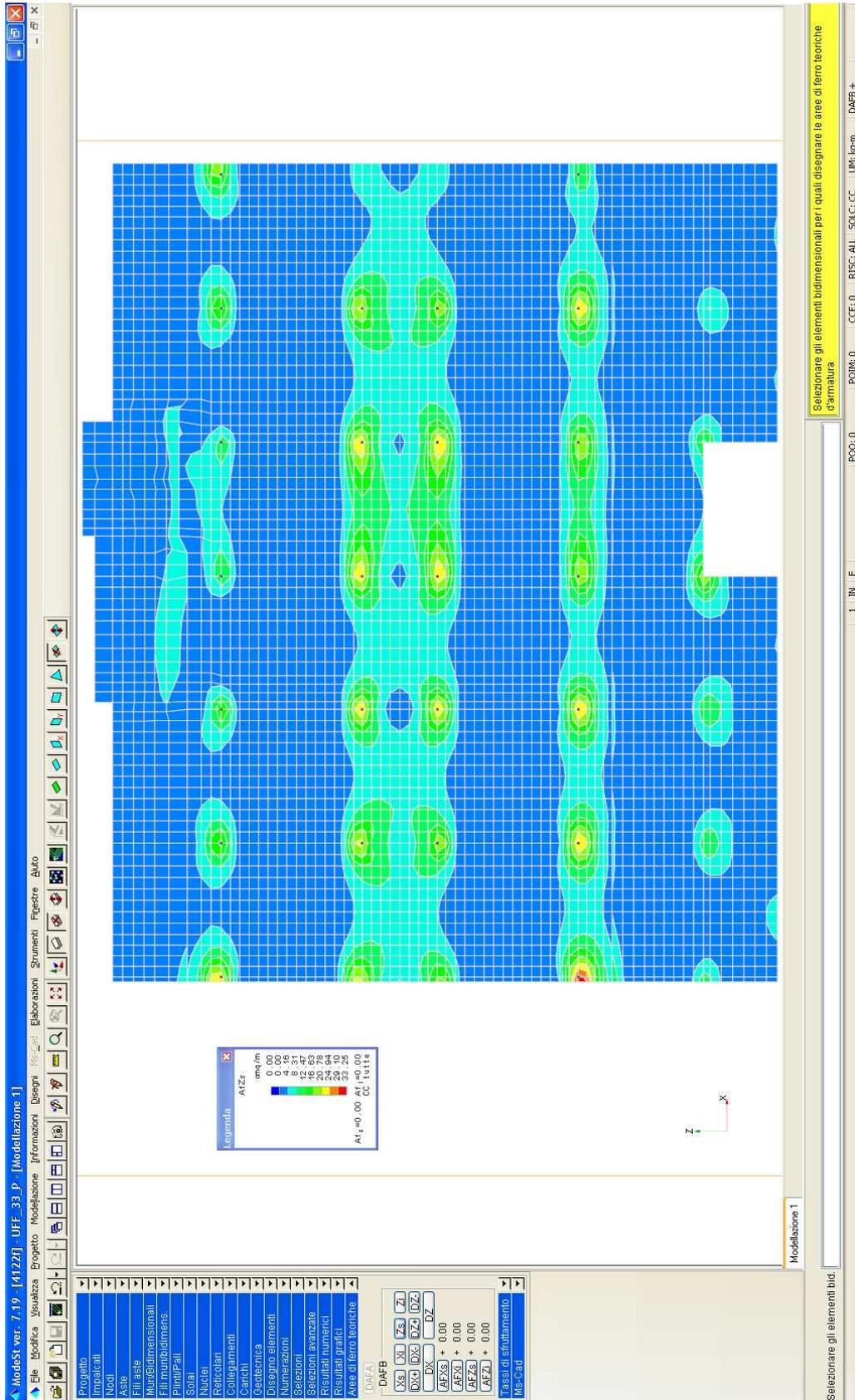


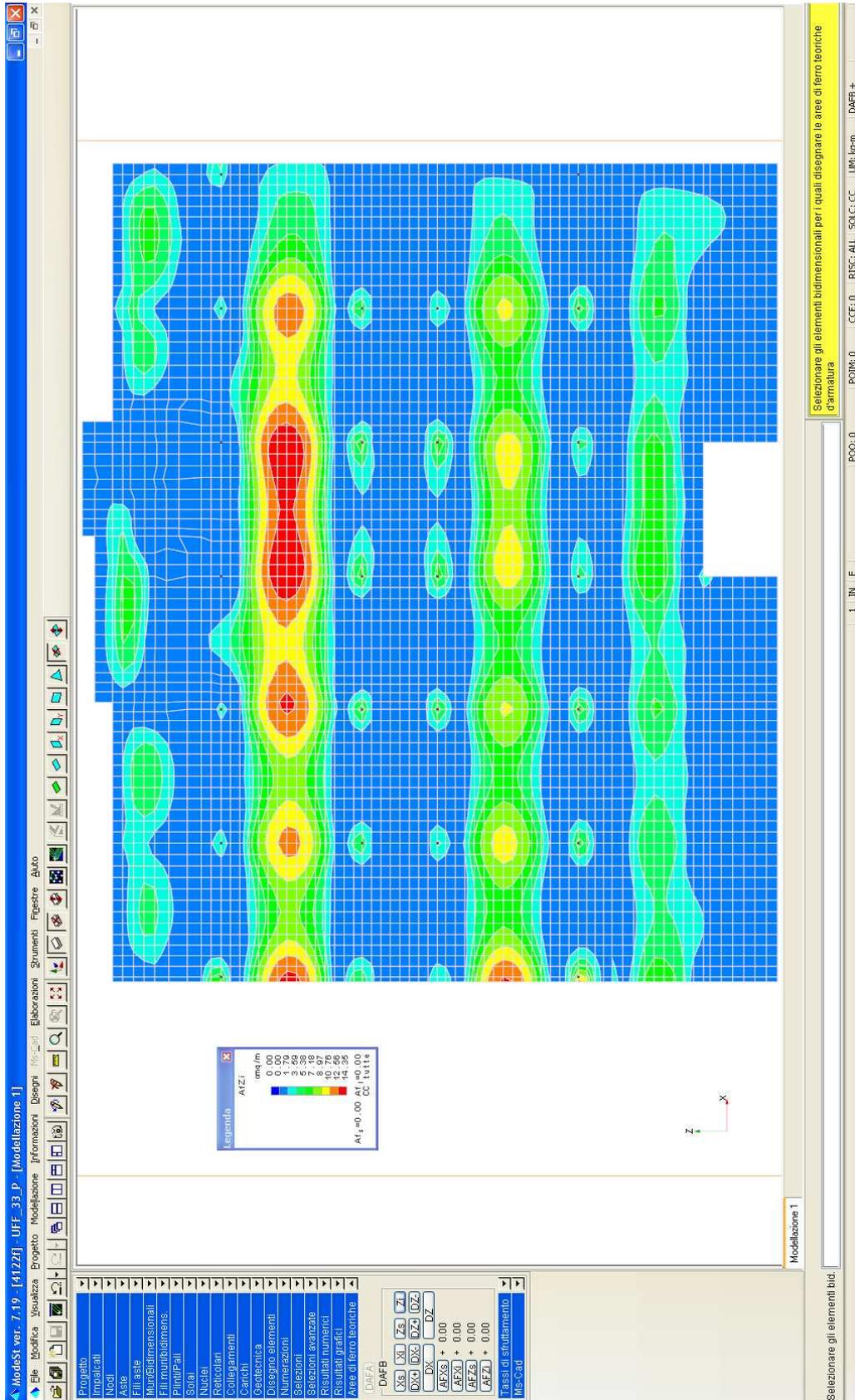
Figura 18 – pressioni sul terreno in sle qp

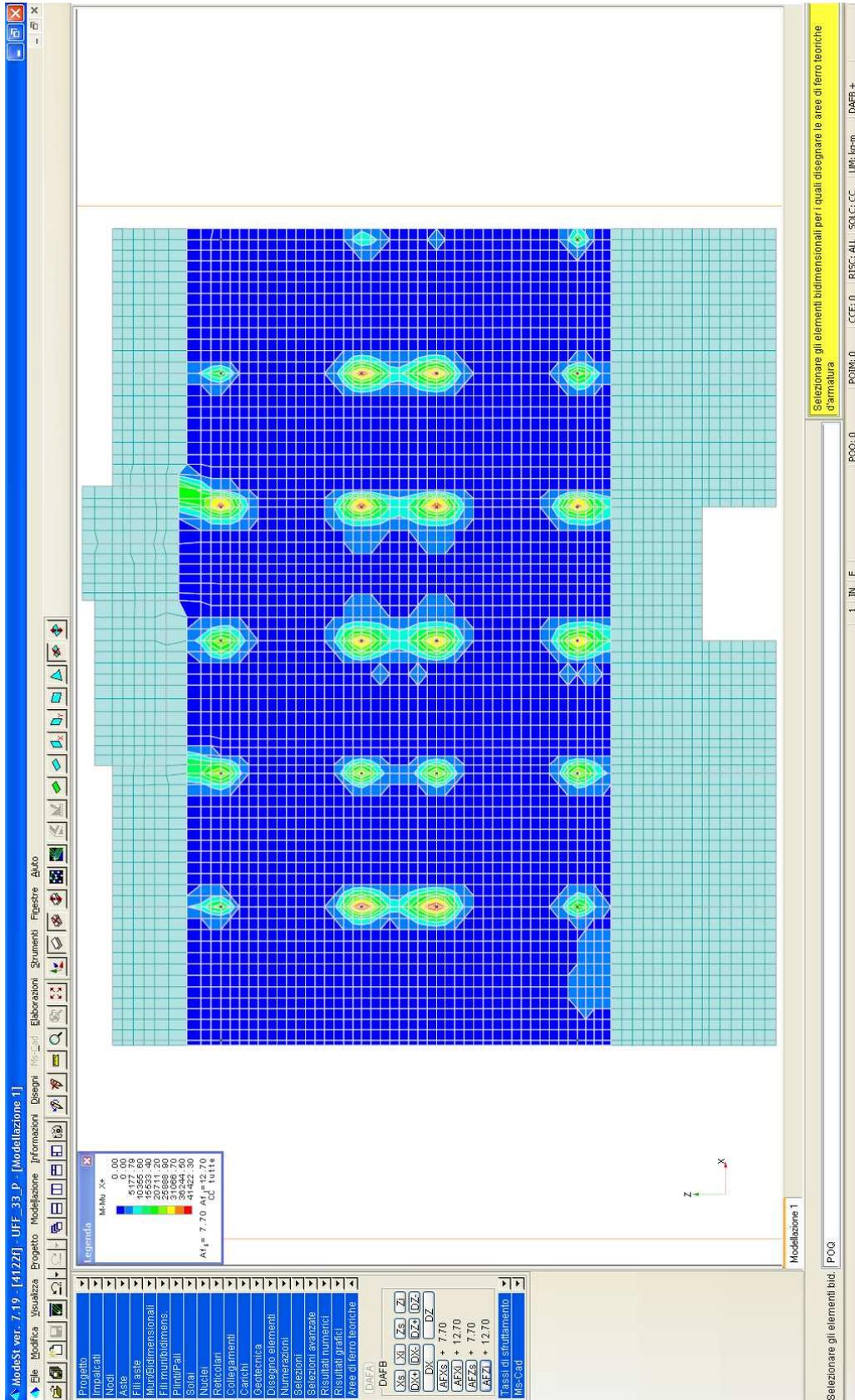
5.3. MAPPE DI ARMATURA ELEMENTI PLATEA DI FONDAZIONE











Modest ver. 7.19 - [41220] - UFF_33_P - [Modellazione 1]

File Modifica Igualizza Progetto Modellazione Informazioni Disegni Modelli Elaborazioni Strumenti Finestre Aiuto

Progetto
 Impalcati
 Nodi
 Assie
 Fili laste
 Murfi bidimensionali
 Fili tridimens.
 Puntipali
 Solai
 Nervi
 Reticolari
 Collamenti
 Carichi
 Geotecnica
 Disegno elementi
 Numerazioni
 Selezioni
 Selezioni avanzate
 Risultati numerici
 Risultati grafici
 Area di ferro teoriche

Leggenda
 M-Mu X-
 0.00
 4832.73
 14549.76
 14549.76
 19339.00
 25096.40
 33829.10
 42561.80
 4832.73
 CC* tutte
 At= 0.00

Z
X

Modellazione 1

POQ.0
 1_IM_F
 CCE.0
 RISC.ALL.
 50LC.CC
 LIM.kg-m
 DAFB+

Selezionare gli elementi bidimensionali per i quali disegnare le aree di ferro teoriche d'armatura.

Selezionare gli elementi bid

ModelSt ver. 7.19 - [4122] - UFF_33_P - [Modellazione 1]
Progetto Modellazione Informazioni Disegni Modelli Elaborazioni Strumenti Finestre Aiuto

Progetto

- Impalcati
- Node
- ASie
- File/asse
- Mappe dimensionali
- File multidimens
- Print/Pali
- Solar
- Nuclei
- Relcolari
- Collamenti
- Carichi
- Geometrica
- Disegno elementi
- Numerazioni
- Selezioni
- Selezioni avanzate
- Resulti numerici
- Resulti grafici
- Area di ferro teoriche

Legenda M-Mu Z4

0,00
11836,00
23672,00
35508,00
47344,00
59180,00
71016,00
82852,00
94688,00
106524,00
118360,00

A_T=7,70 CC Tutle

Modelazione 1

Selezionare gli elementi bidimensionali per i quali disegnare le aree di ferro teoriche d'armatura

1 JM F

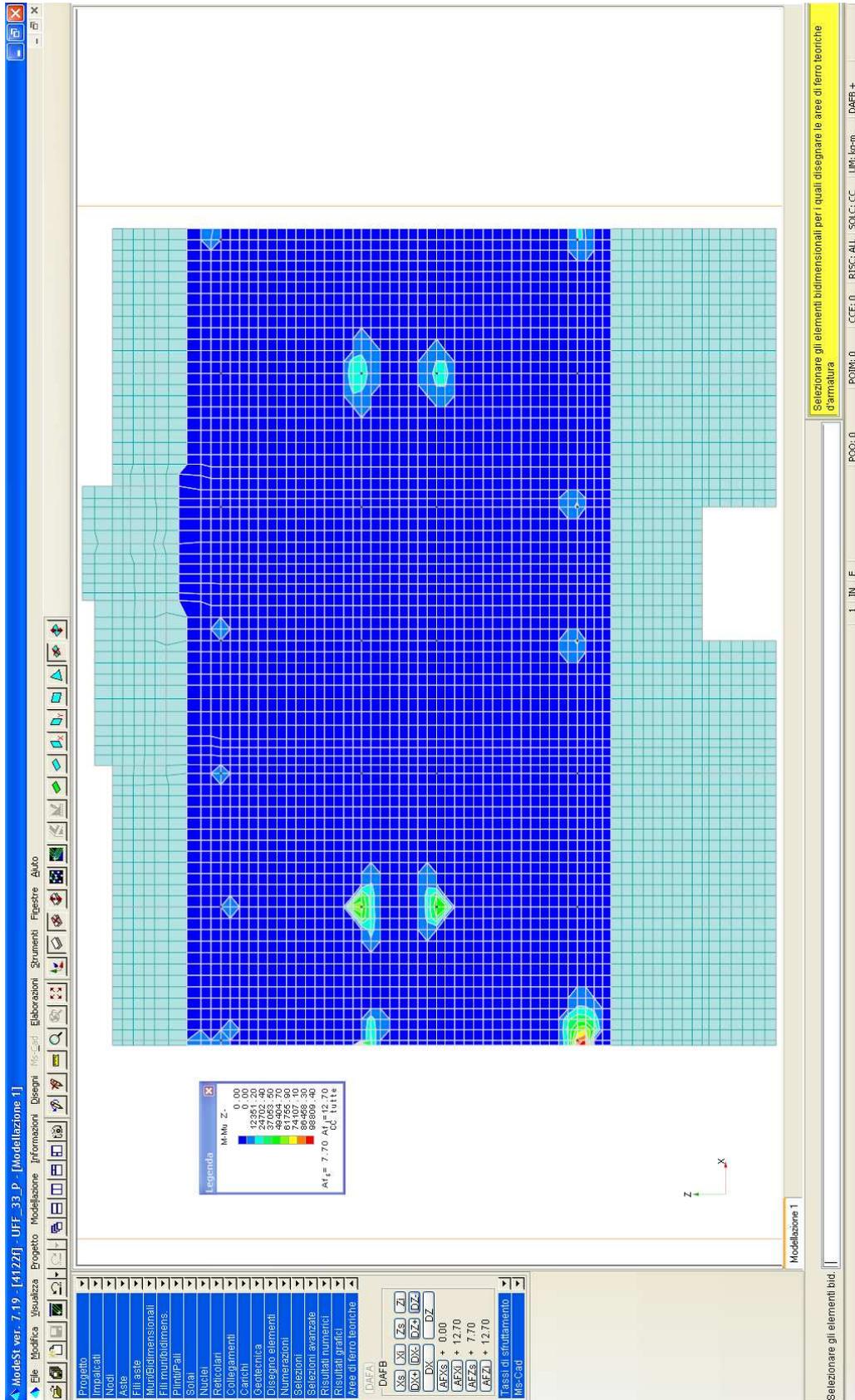
POQ:0 POIM:0 CCE:0 RISC:ALL SOCC:CC UMI:kg/m DAFB +

Selezionare gli elementi bid

- DAFB
- XS1
- XI
- Z3
- Z1
- DX4
- DX3
- DX2
- OZ2
- OZ1
- DX
- DZ
- AFS1 + 0,00
- AFS2 + 12,70
- AFS3 + 7,70
- AFZ1 + 0,00

Tassi di sfruttamento

Me-Card



Modest ver. 7.19 - [41220] - UFF_33_P - [Modellazione 1]

File Modifica Igualizza Progetto Modellazione Informazioni Disegni Mod... Elaborazioni Strumenti Finestre Aiuto

Progetto
Impalcati
Assie
Filigrane
Muridimensionali
Filidimensionali
PuntiPali
Soletti
Nuclei
Rettangoli
Colonnati
Curtchi
Geometrica
Disegno elementi
Numerazioni
Selezioni avanzate
Risultati numerici
Risultati grafici
Area di ferro teoriche

DAFB
 X3 X1 X2 Z1
 DX3 DX1 DX2 DZ1 DZ2
 DX DZ
 AF33 + 7.70
 AF33 + 0.00
 AF33 + 0.00
 AF33 + 0.00

Tassi di sfruttamento
Me-Card

Modellazione 1

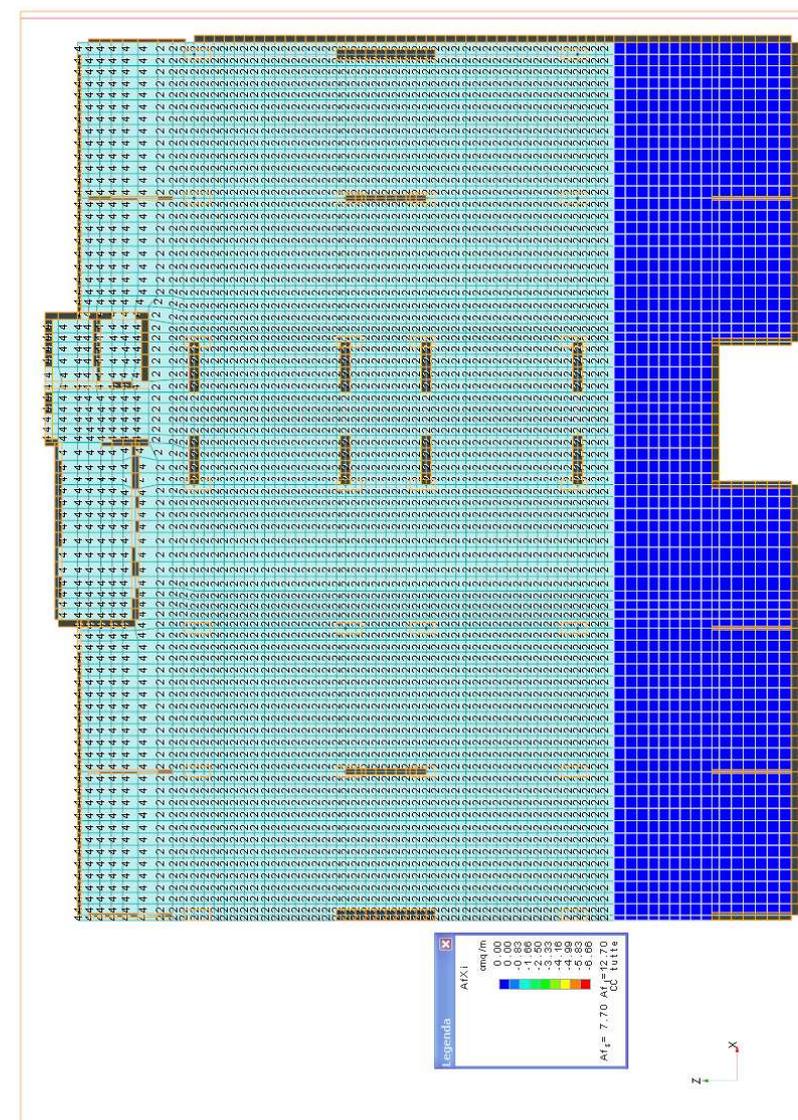
Selezionare gli elementi bidimensionali per i quali disegnare le aree di ferro teoriche
 CCE: 0 RISC: ALL 500.CC
 POIN: 0
 1 IM F
 LIM: kg/m
 DAFB +

Selezionare gli elementi bidimensionali per i quali disegnare le aree di ferro teoriche
 CCE: 0 RISC: ALL 500.CC
 POIN: 0
 1 IM F
 LIM: kg/m
 DAFB +

ModelSt ver. 7.19 - [41220] - UFF_33_P - [Modellazione 1]

Progetto: UFF_33_P - [Modellazione 1]

Elaborazioni: Stumenti: Finestre: Altro:



Selezione gli elementi bidimensionali per i quali disegnare le aree di ferro teoriche d'armatura.

1 - IM - F
POQ: 0
CCE: 0
RISC: ALL
50KG: CC
UMI: kg/m
DAFB: +

Tassi di sfruttamento											
DAFB											
Xs	Xl	Zs	Zl	OZ	OZ						
DXs	DXl	DXZ	DXZ	OZ	OZ						
DX											
AFXS	+ 7.70										
AFXL	+ 12.70										
AFZS	+ 0.00										
AFZL	+ 0.00										

Legenda: AXI (cm/m)

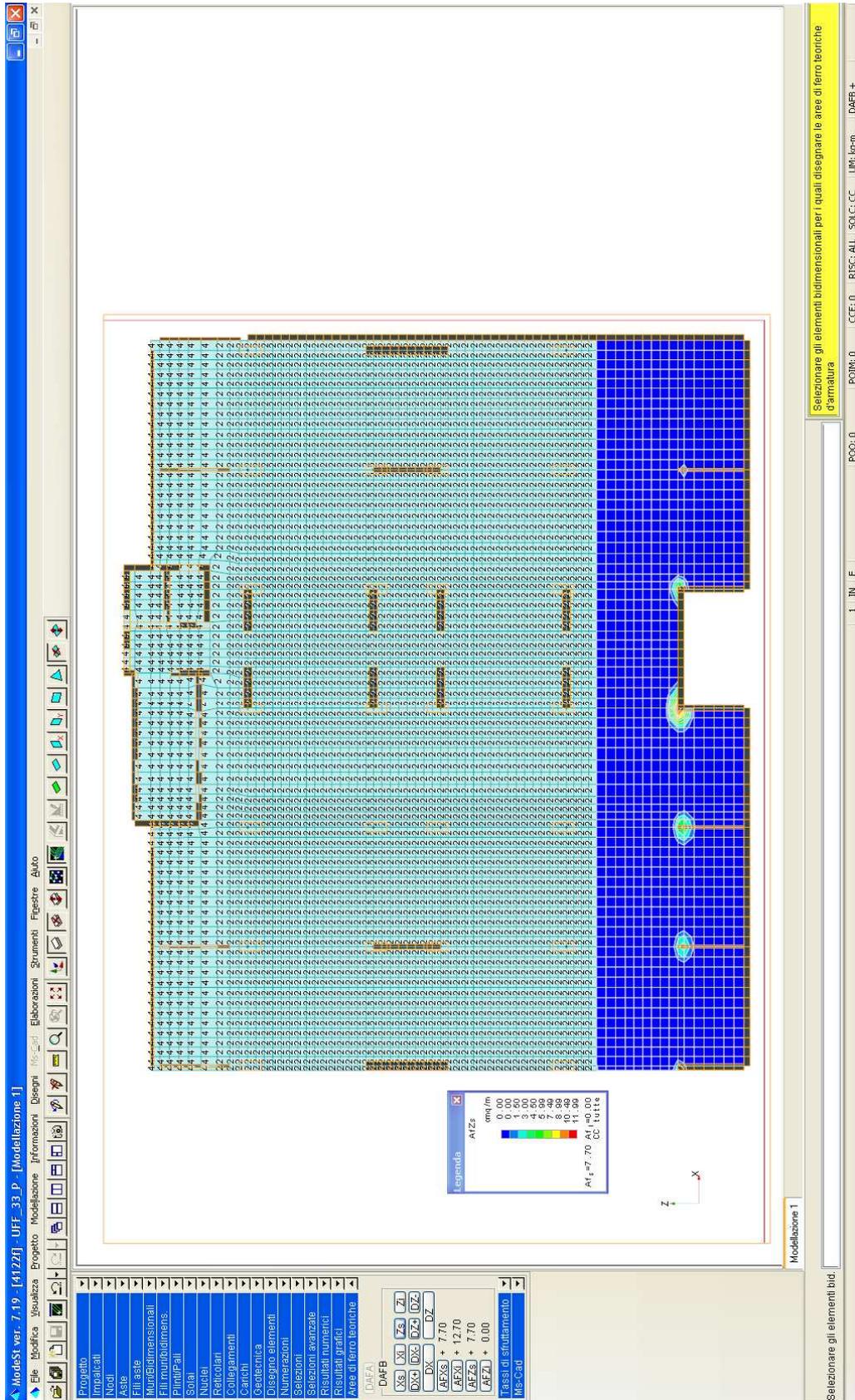
Color Range	Value (cm/m)
Dark Blue	0.00
Blue	0.83
Light Blue	1.67
Cyan	2.50
Green	3.33
Light Green	4.17
Yellow-Green	5.00
Yellow	5.83
Orange	6.67
Red-Orange	7.50
Red	8.33
Dark Red	9.17
Dark Red	10.00
Dark Red	10.83
Dark Red	11.67
Dark Red	12.50
Dark Red	13.33
Dark Red	14.17
Dark Red	15.00
Dark Red	15.83
Dark Red	16.67
Dark Red	17.50
Dark Red	18.33
Dark Red	19.17
Dark Red	20.00

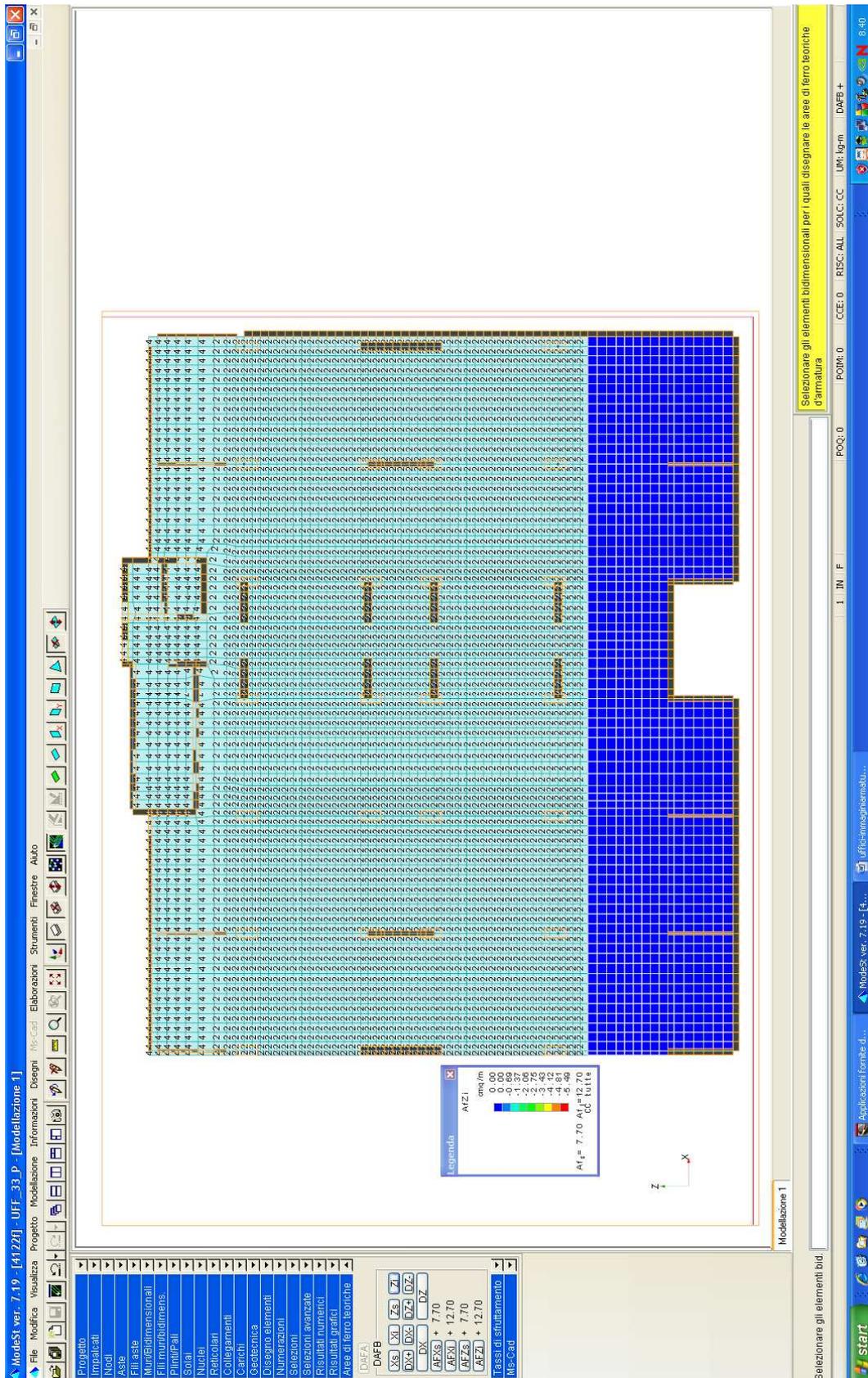
AFx = 7.70 AFy = 12.70 CC tutte

Modellazione 1

Selezione gli elementi bid

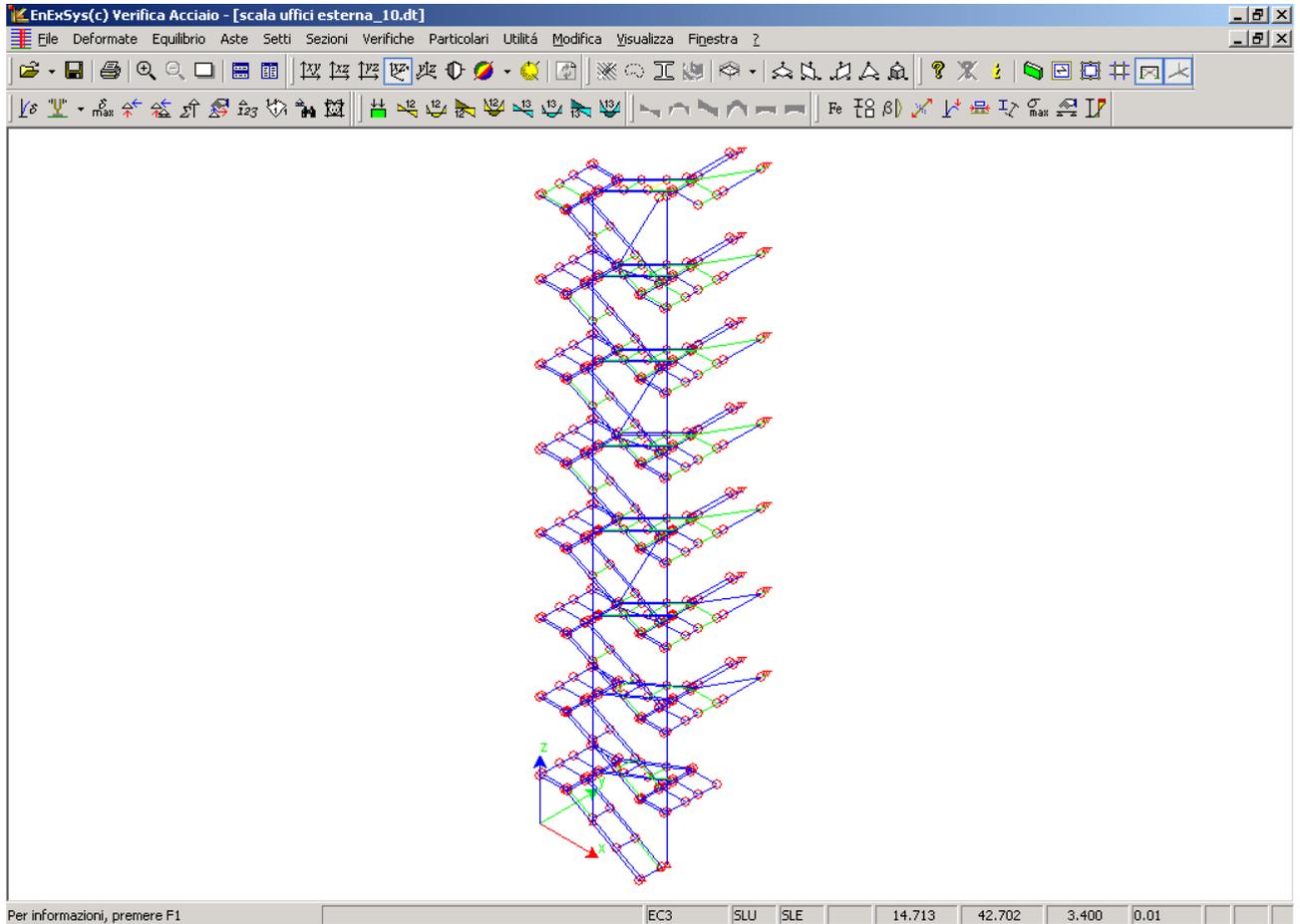
Progetto: UFF_33_P - [Modellazione 1]





6. MODELLAZIONE E

6.1. PERCENTUALE DI SFRUTTAMENTO DEI PROFILATI METALLICI



Nel seguito sono riportati, per ogni profilato impiegato la percentuale di profili che sviluppano uno stato di sollecitazione massimo rispettivamente:

- I Campo: minore del 33% della capacità resistente massima.
- II Campo: minore del 66% della capacità resistente massima.
- III Campo: NON superiore alla massima capacità resistente.
- IV Campo: SUPERIORE alla massima capacità resistente (Aste NON verificate).

Sezione tipo	I Campo	II Campo	III Campo	IV Campo
1 HEA 300	1.00 (16)	0.00 (0)	0.00 (0)	0.00 (0)
2 Tubi Quadri 70x4.0	0.39 (24)	0.56 (35)	0.05 (3)	0.00 (0)
1 IPE 200	0.73 (115)	0.27 (43)	0.00 (0)	0.00 (0)
2 HEA 300	1.00 (62)	0.00 (0)	0.00 (0)	0.00 (0)
3 Tubi 76.1X4.0	0.46 (43)	0.53 (50)	0.01 (1)	0.00 (0)
4 HEB 120	0.40 (8)	0.60 (12)	0.00 (0)	0.00 (0)
6 IPE 200	1.00 (35)	0.00 (0)	0.00 (0)	0.00 (0)
2 Tubi 101.6X6.3/controventi verticali	1.00 (6)	0.00 (0)	0.00 (0)	0.00 (0)
3 Tubi 76.1X8.0/controventi pianerottolo	0.29 (2)	0.71 (5)	0.00 (0)	0.00 (0)

7. CABINA ENEL

7.1. PARAMETRI DI CALCOLO STRUTTURA IN ELEVAZIONE

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con: ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti: Xfinest ver. 8.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08

Tipo di calcolo: analisi sismica dinamica

Schematizzazione piani rigidi: metodo Master-Slave

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <kg/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: ISOSHELL
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: No
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per Buckling: No
- Trascura Buckling torsionale: No

Dati struttura

- Zona sismica: zona 3
- Sito di costruzione: LON. 11.18240 LAT. 43.75800
- Contenuto tra ID reticolo: 20058 20057 20280 20279

Simbologia

TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 Ag = Accelerazione orizzontale massima al sito
 FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale

TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

TCC Ag	FO	TC*
SLO	0.4461	2.57
SLD	0.5363	2.60
SLV	1.2629	2.39

- Tipo di opera: Opera ordinaria
- Vita nominale V_N : 50.00
- Classe d'uso: classe II
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 6.50 <m>
- Numero piani edificio: 1
- Coefficiente θ : 0
- Edificio regolare in altezza: no
- Edificio regolare in pianta: no
- Forze orizzontali convenzionali per stati limite non sismici: no

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. o prefabbricato a telaio di un piano

Coeff. C_1	0.075
Periodo T_1	0.30531
Coeff. λ SLO	1.00
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovrarigidità (α_s/α_1)	1.05
Valore di riferimento del fattore di struttura (q_0)	3.15
Fattore riduttivo (K_w)	1.00
Fattore di struttura (q)	1.50

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica: 1.00
- Modi da calcolare: 120
- Modi da considerare: con singola massa superiore a 1.00%
- Smorzamento spettro: 5.00

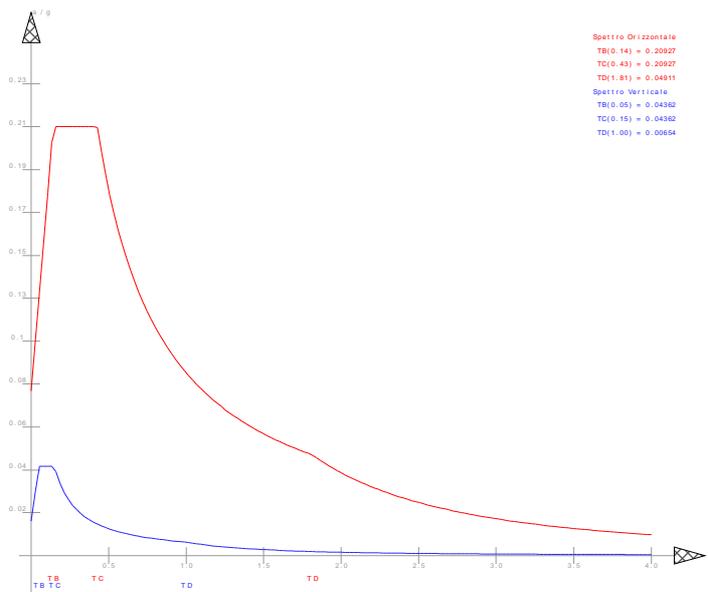


Figura numero 2: Spettro allo SLD

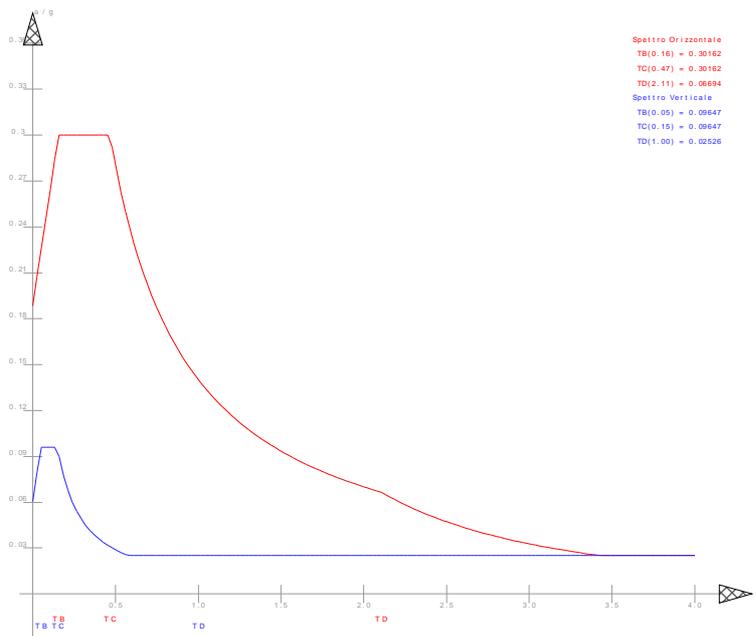


Figura numero 3: Spettro allo SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Dati di piano

Simbologia

- Imp. = Numero dell'impalcato
- Lx = Dimensione del piano in dir. X
- Ly = Dimensione del piano in dir. Y
- Ex = Eccentricità in dir. X
- Ey = Eccentricità in dir. Y
- Ea = Eccentricità complessiva

Imp.	Lx	Ly	Ex	Ey	Ea
<m>	<m>	<m>	<m>	<m>	<m>
1	4.30	11.51	0.22	0.58	0.61

Condizioni di carico elementari

Simbologia

- CCE = Numero della condizione di carico elementare
- Comm. = Commento
- s = Coeff. di riduzione
- Mx = Moltiplicatore della massa in dir. X
- My = Moltiplicatore della massa in dir. Y
- Mz = Moltiplicatore della massa in dir. Z
- Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
- Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
- Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	s	Mx	My	Mz	Jpx	Jpy	Jpz
1	pp e perm	1.00	1.00	1.00	0.00	0.00	0.00	1.00
2	permanente solette	1.00	1.00	1.00	0.00	0.00	0.00	1.00
3	parcheggio	1.00	1.00	1.00	0.00	0.00	0.00	1.00
4	carrabile	1.00	1.00	1.00	0.00	0.00	0.00	1.00
5	copertura (1)	1.00	1.00	1.00	0.00	0.00	0.00	1.00
6	PERMANENTE PORTATO SOLAIO	1.00	1.00	1.00	0.00	0.00	0.00	1.00
7	spinta statica della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
8	spinta accidentale terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
9	VARIAZIONE TERMICA UNIFORME	1.00	0.00	0.00	0.00	0.00	0.00	0.00
10	Momento torcente - SLO	--	--	--	--	--	--	--
11	Sisma dir. X - SLO	--	--	--	--	--	--	--
12	Sisma dir. Y - SLO	--	--	--	--	--	--	--
13	Momento torcente - SLD	--	--	--	--	--	--	--
14	Sisma dir. X - SLD	--	--	--	--	--	--	--
15	Sisma dir. Y - SLD	--	--	--	--	--	--	--
16	Momento torcente - SLV	--	--	--	--	--	--	--
17	Sisma dir. X - SLV	--	--	--	--	--	--	--

18 Sisma dir. Y - SLV -- -- -- -- -- -- --

Ambienti di carico

Simbologia

N Numero

Comm. Commento

1 pp e perm

2 permanente solette

3 parcheggio

4 carrabile

5 copertura (1)

6 PERMANENTE PORTATO SOLAIO

7 spinta statica della terra

8 spinta accidentale terra

9 VARIAZIONE TERMICA UNIFORME

F azioni orizzontali convenzionali

SLU Stato limite ultimo

SLR Stato limite per combinazioni rare

SLF Stato limite per combinazioni frequenti

SLQ Stato limite per combinazioni quasi permanenti o di danno

N	Comm.	1	2	3	4	5	6	7	8	9	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	si	no	no	no										
2	Calcolo statico	si	no	si	si	si	si								

Combinazioni delle cce

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLU S = Stato limite ultimo (azione sismica)

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SLV = Stato limite di salvaguardia della vita

SLC = Stato limite di prevenzione del collasso

SLO = Stato limite di operatività

An. = Tipo di analisi

L = Lineare

NL = Non lineare

Bk = Buckling

S = Si

N = No

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	8	9	Mt	±S	X	±S	Y
1	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30		
2	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30		
3	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30	1.00	
4	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30	1.00	
5	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	0.30		
6	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	-0.30		
7	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	0.30	1.00	
8	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	-0.30	1.00		
9	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30		
10	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30		
11	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30	1.00	
12	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30	1.00	
13	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	0.30		
14	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	-0.30		
15	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	0.30	1.00	
16	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	-0.30	1.00		
17	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30	0.30	
18	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30	
19	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30		
20	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30		
21	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30	0.30	
22	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30	
23	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30		
24	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30		
25	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30	0.30	
26	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30	
27	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30		
28	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30		
29	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30	0.30	
30	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30	-0.30	

31	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30
32	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30
33	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	0.90	0.00	0.00	0.00
34	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	-0.90	0.00	0.00	0.00
35	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	0.90	0.00	0.00	0.00
36	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	-0.90	0.00	0.00	0.00
37	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	0.90	0.00	0.00	0.00
38	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	-0.90	0.00	0.00	0.00
39	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	0.90	0.00	0.00	0.00
40	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	-0.90	0.00	0.00	0.00
41	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	0.90	0.00	0.00	0.00
42	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	-0.90	0.00	0.00	0.00
43	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	0.90	0.00	0.00	0.00
44	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	-0.90	0.00	0.00	0.00
45	statica copertura	SLE R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	1.00	0.40	0.60	0.00	0.00	0.00
46	statica copertura	SLE R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	1.00	0.40	-0.60	0.00	0.00	0.00
47	statica copertura	SLE R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	1.00	0.40	0.60	0.00	0.00	0.00
48	statica copertura	SLE R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	1.00	0.40	-0.60	0.00	0.00	0.00
49	statica (piazza)	SLE R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	1.00	0.60	0.00	0.00	0.00
50	statica (piazza)	SLE R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	1.00	-0.60	0.00	0.00	0.00
51	statica (piazza)	SLE R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	1.00	0.60	0.00	0.00	0.00
52	statica (piazza)	SLE R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	1.00	-0.60	0.00	0.00	0.00
53	statica (parcheggio)	SLE R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	0.60	0.00	0.00	0.00
54	statica (parcheggio)	SLE R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	-0.60	0.00	0.00	0.00
55	statica (parcheggio)	SLE R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	0.60	0.00	0.00	0.00
56	statica (parcheggio)	SLE R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	-0.60	0.00	0.00	0.00
57	statica copertura	SLE F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
58	statica copertura	SLE F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
59	statica copertura	SLE F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
60	statica copertura	SLE F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
61	statica (piazza)	SLE F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
62	statica (piazza)	SLE F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
63	statica (piazza)	SLE F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
64	statica (piazza)	SLE F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
65	statica (parcheggio)	SLE F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
66	statica (parcheggio)	SLE F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
67	statica (parcheggio)	SLE F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
68	statica (parcheggio)	SLE F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
69		SLE Q	L	N	1.00	1.00	0.60	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
70		SLE Q	L	N	1.00	1.00	0.60	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00

Elenco baricentri e masse impalcati

Simbologia

Imp. = Numero dell'impalcato
 X = Coordinata X
 Y = Coordinata Y
 Z = Coordinata Z
 Mo = Massa orizzontale
 Jpz = Momento d'inerzia polare intorno all'asse Z

Imp.	X	Y	Z	Mo	Jpz
<m>	<m>	<m>	<m>	<KG>	<KG ² mq>
1	0.03	14.59	6.50	2674.53	37243.40

Totali masse impalcati

Mo	Jpz
<KG>	<KG ² mq>
2674.53	37243.40

Elenco masse nodi

Simbologia

Nodo = Numero del nodo
 Mo = Massa orizzontale

| Nodo | Mo |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| <KG> |
-2654	13.04	-2653	12.81	-2652	12.81	-2651	12.81	-2650	6.28	-2649	3.14	-2648	11.32	-2647	5.66
-2646	12.18	-2645	12.81	-2644	12.93	-2643	12.81	-2642	8.63	-2641	10.72	-2640	7.45	-2639	10.14
-2638	5.07	-2637	10.73	-2636	11.47	-2635	12.14	-2634	7.73	-2633	8.18	-2632	5.62	-2631	6.68
-2630	2.81	-2629	5.95	-2628	5.62	-2627	2.81	-2625	5.62	-2624	11.47	-2622	11.47	-2621	11.47
-2620	11.47	-2619	12.14	-2618	11.47	-2617	11.47	-2615	11.47	-2614	11.47	-2613	11.47	-2612	9.60
-2611	12.14	-2610	11.47	-2609	11.47	-2607	11.47	-2606	10.14	-2605	5.07	-2603	10.14	-2602	11.69
-2601	10.92	-2600	11.58	-2599	12.37	-2598	11.69	-2597	10.92	-2596	11.58	-2594	11.69	-2593	7.73
-2592	9.60	-2591	6.68	-2589	7.73	-2588	6.59	-2587	3.30	-2586	5.73	-2585	6.59	-2584	3.30
-2583	6.59	-2582	5.73	-2581	5.73	-2580	6.59	-2579	3.30	-2578	6.16	-2577	5.73	-2576	5.73
-2575	6.16	-2574	5.91	-2573	2.95	-2572	5.14	-2571	5.14	-2569	5.14	-2568	5.91	-2567	2.95
-2566	5.52	-2564	5.91	-2563	2.95	-2562	5.52	-2561	5.91	-2560	5.14	-2559	5.14	-2557	5.14
-2556	5.14	-2555	5.14	-2554	5.14	-2553	5.14	-2552	5.14	-2551	5.91	-2550	5.52	-2549	2.95
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-1373	51.76	-1372	48.76	-1371	49.20	-1370	37.75	-1369	25.48	-1368	46.71	-1367	72.48	-1366	72.48
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-1357	82.73	-1356	154.98	-1355	52.85	-1354	52.85	-1353	154.98	-1352	82.73	-1351	49.64	-1350	73.91
-1349	75.29	-1348	57.02	-1347	55.98	-1346	55.98	-1345	57.02	-1344	75.29	-1343	73.91	-1342	49.80
-1341	73.91	-1340	55.98	-1339	37.72	-1338	37.72	-1337	55.98	-1336	73.91	-1335	49.80	-1334	82.73
-1333	99.28	-1332	105.70	-1331	154.98	-1330	154.98	-1329	105.70	-1328	99.28	-1327	82.73	-1326	90.72
-1324	77.03	-1323	77.03	-1322	90.72	-1321	72.22	-1320	108.43	-1319	108.43	-1318	72.22	-1317	39.29
-1292	39.29	-1286	23.95	-1284	23.95	-1279	70.35	-1273	42.79	-1271	42.79	-1265	70.35	-1262	70.35
-1257	72.14	-1253	43.72	-1251	43.72	-1248	42.79	-1242	42.79	-1240	70.35	-1235	72.14	-1232	72.22
-1227	45.10	-1223	38.66	-1217	38.66	-1214	108.43	-1212	108.43	-1206	72.22	-1079	45.10	-1074	87.95
-1073	26.42	-1072	73.30	-1071	54.77	-1070	22.02	-1069	110.70	-1068	75.50	-1067	110.70	-1066	38.74
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-1041	65.48	-1040	48.75	-1039	19.67	-1038	65.48	-1037	19.67	-1036	66.70	-1035	51.38	-1034	20.04
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-1025	65.48	-1024	19.67	-1023	66.70	-1022	20.04	-1021	51.38	-1020	73.29	-1019	22.02	-1018	43.98
-1017	13.21	-1016	49.64	-1015	110.70	-1014	110.70	-1013	38.74	-1012	37.75	-1011	62.07	-1010	37.75
-1009	13.21	-1008	62.07	-1007	73.29	-1006	22.02	-1005	43.98	-1004	49.64	-1003	13.21	-1002	28.37
-1001	52.71	-1000	51.13	-997	3.30	-994	28.37	-993	52.71	-992	51.13	-991	32.91	-990	39.77
-989	37.24	-988	39.77	-987	32.91	-986	34.64	-985	37.24	-984	3.30	-975	6.16	-974	5.73
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-935	4.34	-934	2.81	-933	7.15	-932	6.68	-931	6.68	-930	9.60	-929	9.60	-928	11.47
-927	11.47	-926	11.47	-925	11.47	-924	11.58	-923	11.58	-922	10.92	-921	10.92	-920	5.07
-919	9.95	-918	10.04	-917	5.91	-916	11.04	-915	10.27	-914	11.04	-913	11.07	-912	3.13
-911	5.84	-910	5.44	-909	5.84	-908	3.13	-907	4.59	-906	2.98	-905	7.57	-904	7.07
-903	7.07	-901	10.16	-900	10.16	-899	12.14	-898	12.14	-897	12.14	-896	12.14	-895	12.25
-894	12.25	-893	11.55	-892	11.55	-890	5.37	-889	10.53	-888	10.63	-886	6.25	-885	11.69
-884	10.87	-883	11.69	-882	11.71	-880	17.17	-878	31.90	-877	30.94	-876	27.26	-875	28.00
-874	31.68	-873	29.47	-872	31.68	-871	28.00	-870	27.26	-869	30.94	-868	31.90	-866	17.17
-865	34.51	-863	64.13	-862	62.20	-861	54.80	-860	56.28	-859	63.68	-858	59.24	-857	63.68
-856	56.28	-855	54.80	-854	62.20	-853	64.13	-851	34.51	-850	33.69	-848	65.34	-847	62.45
-846	55.01	-845	56.50	-844	65.27	-843	56.80	-842	65.27	-841	56.50	-840	55.01	-839	62.45
-838	65.34	-836	33.69	-835	29.86	-833	86.62	-832	65.56	-831	57.75	-830	59.31	-829	91.61
-828	31.57	-827	91.61	-826	59.31	-825	57.75	-824	65.56	-823	86.62	-821	29.86	-820	140.53
-818	83.14	-817	72.67	-816	72.97	-815	88.44	-814	120.54	-813	120.54	-812	88.44	-811	72.97
-810	72.67	-809	83.14	-808	140.53	-807	23.34	-806	74.11	-805	58.00	-804	66.83	-803	92.33
-786	138.06	-785	43.97	-784	138.06	-783	92.33	-782	66.83	-781	58.00	-780	74.11	-778	23.34
-777	27.11	-775	53.02	-774	50.54	-773	48.66	-772	57.85	-771	68.95	-770	57.50	-769	68.95
-768	57.85	-767	48.66	-766	50.54	-765	53.02	-763	27.11	-762	26.57	-760	49.38	-759	47.89
-758	37.26	-757	30.83	-756	34.88	-755	32.45	-754	34.88	-753	41.73	-752	45.73	-751	47.89
-750	49.38	-748	26.57	-747	19.88	-745	38.47	-744	36.80	-743	34.04	-742	30.67	-741	27.33
-740	23.87	-739	27.33	-738	41.57	-737	42.52	-736	36.80	-735	38.47	-733	19.88	-732	12.45
-730	42.85	-729	34.35	-728	39.58	-727	38.70	-726	32.31	-725	9.54	-724	32.31	-723	38.70
-722	39.58	-721	34.35	-720	42.85	-718	12.45	-717	140.53	-715	60.02	-714	49.3		

-534	52.36	-533	50.98	-532	57.87	-531	60.39	-529	31.37	-528	40.17	-526	74.64	-525	72.40
-524	63.78	-523	65.51	-522	74.13	-521	68.95	-520	74.13	-519	65.51	-518	63.78	-517	72.40
-516	74.64	-514	40.17	-513	40.68	-511	75.60	-510	73.33	-509	64.60	-508	66.34	-507	75.07
-506	69.83	-505	75.07	-504	66.34	-503	64.60	-502	73.33	-501	75.60	-499	40.68	-483	27.47
-481	51.04	-480	49.51	-479	43.62	-478	44.80	-477	50.69	-476	47.15	-475	50.69	-474	44.80
-473	43.62	-472	49.51	-471	51.04	-469	27.47	-468	5.85	-466	10.86	-465	10.54	-464	9.28
-463	9.53	-462	10.79	-461	10.03	-460	10.79	-459	9.53	-458	9.28	-457	10.54	-456	10.86
-454	5.85	-453	11.69	-451	21.72	-450	21.07	-449	18.56	-448	19.07	-447	21.57	-446	20.07
-445	21.57	-444	19.07	-443	18.56	-442	21.07	-441	21.72	-439	11.69	-438	5.85	-436	10.86
-435	10.54	-434	9.28	-433	9.53	-432	10.79	-431	10.03	-430	10.79	-429	9.53	-428	9.28
-427	10.54	-426	10.86	-424	5.85	-423	11.69	-421	21.72	-420	21.07	-419	18.56	-418	19.07
-417	21.57	-416	20.07	-415	21.57	-414	19.07	-413	18.56	-412	21.07	-411	21.72	-409	11.69
14	146.55	16	136.46	18	136.46	20	146.55								

Totali masse nodi

Mo
<KG>
76822.50

Elenco forze sismiche di impalcato allo SLO**Simbologia**

Imp. = Numero dell'impalcato
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y
Mz = Momento intorno all'asse Z

Imp. cx cy Mz
<kgm>
1 0.07 0.07 5547.19

Totali forze sismiche

Mz
<kgm>
5547.19

Elenco forze sismiche di impalcato allo SLD

Imp. cx cy Mz
<kgm>
1 0.07 0.07 6753.33

Totali forze sismiche

Mz
<kgm>
6753.33

Elenco forze sismiche di impalcato allo SLV

Imp. cx cy Mz
<kgm>
1 0.07 0.07 9733.50

Totali forze sismiche

Mz
<kgm>
9733.50

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione**Simbologia**

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi
 Φ_x = Coefficiente di partecipazione in dir. X
 Φ_y = Coefficiente di partecipazione in dir. Y
 Φ_z = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φ_x	Φ_y	Φ_z	%Mx	%My	%Mz	%Jpz
1 *	0.16	89.25	0.44	279.32	0.00	0.00	98.14	0.00	0.00	
2 *	0.08	37.49	241.43	-0.83	0.00	73.32	0.00	0.00	0.04	
3 *	0.06	37.49	-84.50	-0.90	0.00	8.98	0.00	0.00	0.28	
4 *	0.04	13.88	0.98	5.84	0.00	0.00	0.04	0.00	10.34	
5 *	0.03	12.28	5.97	-1.50	0.00	0.04	0.00	0.00	1.39	
6	0.03	5.39	1.43	-0.16	0.00	0.00	0.00	0.00	0.00	
7	0.03	0.66	-11.48	-0.11	0.00	0.17	0.00	0.00	0.23	
8	0.03	0.66	-0.61	0.14	0.00	0.00	0.00	0.00	0.78	
9	0.03	1.97	-3.64	-0.24	0.00	0.02	0.00	0.00	0.84	
10 *	0.03	1.97	-1.60	0.38	0.00	0.00	0.00	0.00	1.46	
11	0.03	5.71	-0.31	-0.30	0.00	0.00	0.00	0.00	0.09	

12	0.02	5.45	-0.79	0.55	0.00	0.00	0.00	0.00	0.27
13 *	0.02	2.50	-20.79	-0.66	0.00	0.54	0.00	0.00	15.93
14	0.02	2.12	25.30	0.04	0.00	0.81	0.00	0.00	0.13
15 *	0.02	0.87	-80.87	-0.17	0.00	8.23	0.00	0.00	1.80
16	0.02	0.87	-20.98	-0.07	0.00	0.55	0.00	0.00	0.38
17 *	0.02	3.17	30.34	-0.91	0.00	1.16	0.00	0.00	33.32
18 *	0.02	2.22	45.10	-0.21	0.00	2.56	0.00	0.00	0.23
19	0.02	2.22	-0.68	-15.96	0.00	0.00	0.32	0.00	0.04
20	0.02	2.31	-12.62	-0.10	0.00	0.20	0.00	0.00	0.15
21	0.02	0.90	0.04	0.32	0.00	0.00	0.00	0.00	0.00
22 *	0.02	0.90	-0.84	-0.20	0.00	0.00	0.00	0.00	3.50
23	0.02	1.20	1.57	-0.06	0.00	0.00	0.00	0.00	0.06
24	0.02	1.20	0.62	0.00	0.00	0.00	0.00	0.00	0.01
25	0.02	3.72	-0.06	0.01	0.00	0.00	0.00	0.00	0.02
26	0.01	0.03	0.03	-0.02	0.00	0.00	0.00	0.00	0.00
27	0.01	0.03	-0.00	-0.13	0.00	0.00	0.00	0.00	0.00
28	0.01	5.87	-11.36	-0.02	0.00	0.16	0.00	0.00	0.01
29	0.01	0.44	0.18	0.21	0.00	0.00	0.00	0.00	0.26
30	0.01	0.44	-0.09	-0.00	0.00	0.00	0.00	0.00	0.00
31	0.01	2.16	11.96	0.91	0.00	0.18	0.00	0.00	0.53
32	0.01	2.16	-0.87	15.10	0.00	0.00	0.29	0.00	0.10
33	0.01	2.60	-0.16	3.03	0.00	0.00	0.01	0.00	0.00
34	0.01	0.39	-0.43	10.71	0.00	0.00	0.14	0.00	0.01
35	0.01	0.39	-0.25	2.70	0.00	0.00	0.01	0.00	0.00
36	0.01	0.46	-7.93	-0.91	0.00	0.08	0.00	0.00	0.01
37	0.01	2.01	-0.02	-13.28	0.00	0.00	0.22	0.00	0.01
38	0.01	0.84	0.19	0.30	0.00	0.00	0.00	0.00	0.00
39	0.01	0.84	0.13	6.60	0.00	0.00	0.05	0.00	0.00
40	0.01	1.17	0.45	-0.38	0.00	0.00	0.00	0.00	0.11
41	0.01	1.17	-0.20	0.62	0.00	0.00	0.00	0.00	0.00
42	0.01	1.70	0.34	0.84	0.00	0.00	0.00	0.00	0.00
43	0.01	0.72	-24.91	0.02	0.00	0.78	0.00	0.00	0.00
44	0.01	0.61	1.34	-0.00	0.00	0.00	0.00	0.00	0.00
45	0.01	0.61	1.60	-0.05	0.00	0.00	0.00	0.00	0.04
46	0.01	0.75	-6.53	0.01	0.00	0.05	0.00	0.00	0.00
47	0.01	0.90	7.01	-0.01	0.00	0.06	0.00	0.00	0.10
48	0.01	0.51	-0.45	-0.00	0.00	0.00	0.00	0.00	0.00
49	0.01	0.51	0.12	0.52	0.00	0.00	0.00	0.00	0.00
50	0.01	1.97	0.23	0.25	0.00	0.00	0.00	0.00	0.01
51	0.01	0.87	0.59	0.05	0.00	0.00	0.00	0.00	0.01
52	0.01	0.77	-1.56	-0.02	0.00	0.00	0.00	0.00	0.02
53	0.01	0.77	0.69	-0.06	0.00	0.00	0.00	0.00	0.00
54	0.01	0.50	-0.94	0.03	0.00	0.00	0.00	0.00	0.42
55	0.01	0.50	-0.13	-0.08	0.00	0.00	0.00	0.00	0.04
56	0.01	0.56	-0.34	-0.01	0.00	0.00	0.00	0.00	0.00
57	0.01	0.56	-0.16	0.48	0.00	0.00	0.00	0.00	0.02
58	0.01	0.07	0.02	-0.06	0.00	0.00	0.00	0.00	0.00
59	0.01	0.07	0.19	-0.01	0.00	0.00	0.00	0.00	0.21
60	0.01	0.48	-5.17	0.01	0.00	0.03	0.00	0.00	0.00
61	0.01	0.48	-2.08	0.01	0.00	0.01	0.00	0.00	0.07
62	0.01	1.50	1.66	0.10	0.00	0.00	0.00	0.00	0.00
63	0.01	0.24	0.67	-0.08	0.00	0.00	0.00	0.00	0.13
64	0.01	0.24	0.28	1.40	0.00	0.00	0.00	0.00	0.00
65	0.01	0.85	-0.02	-0.01	0.00	0.00	0.00	0.00	0.00
66	0.01	0.09	3.29	0.10	0.00	0.01	0.00	0.00	0.03
67	0.01	0.09	3.80	0.09	0.00	0.02	0.00	0.00	0.04
68	0.01	0.50	6.81	-0.14	0.00	0.06	0.00	0.00	0.00
69	0.01	0.29	0.50	0.02	0.00	0.00	0.00	0.00	0.00
70	0.01	0.29	-1.37	0.51	0.00	0.00	0.00	0.00	0.00
71	0.01	1.15	-3.04	-0.14	0.00	0.01	0.00	0.00	0.03
72	0.01	0.37	-0.62	0.00	0.00	0.00	0.00	0.00	0.00
73	0.01	0.37	0.36	-0.02	0.00	0.00	0.00	0.00	0.00
74	0.01	0.61	-10.13	0.01	0.00	0.13	0.00	0.00	0.00
75	0.01	1.06	-0.04	0.03	0.00	0.00	0.00	0.00	0.00
76	0.01	0.78	0.38	-0.02	0.00	0.00	0.00	0.00	0.00
77	0.01	0.68	5.12	-0.16	0.00	0.03	0.00	0.00	0.20
78	0.01	0.60	0.69	0.32	0.00	0.00	0.00	0.00	0.00
79	0.01	0.60	0.03	3.71	0.00	0.00	0.02	0.00	0.00
80	0.01	1.04	0.07	9.28	0.00	0.00	0.11	0.00	0.00
81	0.01	0.84	-0.21	0.01	0.00	0.00	0.00	0.00	0.01
82	0.01	0.69	0.30	-0.10	0.00	0.00	0.00	0.00	0.08
83	0.01	0.69	0.01	-0.12	0.00	0.00	0.00	0.00	0.00
84	0.01	1.05	-3.74	0.13	0.00	0.02	0.00	0.00	0.02
85	0.01	0.82	0.09	0.50	0.00	0.00	0.00	0.00	0.00
86	0.01	0.82	-2.45	-0.11	0.00	0.01	0.00	0.00	0.01
87	0.01	0.18	-0.73	-0.94	0.00	0.00	0.00	0.00	0.07
88	0.01	0.07	-0.60	0.80	0.00	0.00	0.00	0.00	0.03
89	0.01	0.05	-0.32	0.86	0.00	0.00	0.00	0.00	0.00
90	0.01	0.05	-0.00	0.01	0.00	0.00	0.00	0.00	0.00
91	0.01	0.56	-0.01	0.02	0.00	0.00	0.00	0.00	0.00
92	0.01	0.59	-0.21	-0.17	0.00	0.00	0.00	0.00	0.00
93	0.01	0.49	1.04	0.07	0.00	0.00	0.00	0.00	0.06
94	0.01	0.15	0.31	-0.02	0.00	0.00	0.00	0.00	0.16
95	0.01	0.15	2.63	0.09	0.00	0.01	0.00	0.00	0.04
96	0.01	0.18	0.03	0.01	0.00	0.00	0.00	0.00	0.00
97	0.01	0.18	2.75	0.02	0.00	0.01	0.00	0.00	0.05
98	0.01	0.40	0.77	0.01	0.00	0.00	0.00	0.00	0.00
99	0.01	0.40	-0.16	0.23	0.00	0.00	0.00	0.00	0.00
100	0.01	0.96	-0.15	0.70	0.00	0.00	0.00	0.00	0.00
101	0.01	0.18	0.64	0.00	0.00	0.00	0.00	0.00	0.00
102	0.01	0.18	-0.01	0.00	0.00	0.00	0.00	0.00	0.00
103	0.01	0.83	0.04	-0.00	0.00	0.00	0.00	0.00	0.00
104	0.01	0.83	-2.12	0.02	0.00	0.01	0.00	0.00	0.00
105	0.01	0.38	-2.24	-0.12	0.00	0.01	0.00	0.00	0.01
106	0.01	0.38	0.02	-0.11	0.00	0.00	0.00	0.00	0.00
107	0.01	0.59	0.29	0.01	0.00	0.00	0.00	0.00	0.00
108	0.01	0.09	0.49	0.07	0.00	0.00	0.00	0.00	0.01
109	0.01	0.09	-0.25	0.05	0.00	0.00	0.00	0.00	0.01

110	0.01	0.52	0.25	0.61	0.00	0.00	0.00	0.00	0.00
111	0.01	0.31	1.98	-0.06	0.00	0.00	0.00	0.00	0.08
112	0.01	0.31	2.25	0.08	0.00	0.01	0.00	0.00	0.03
113	0.01	0.14	-9.40	-0.10	0.00	0.11	0.00	0.00	0.00
114	0.01	0.14	-1.60	0.01	0.00	0.00	0.00	0.00	0.00
115	0.01	0.17	0.37	0.28	0.00	0.00	0.00	0.00	0.00
116	0.01	0.17	0.18	-0.00	0.00	0.00	0.00	0.00	0.00
117	0.00	1.22	-2.65	0.39	0.00	0.01	0.00	0.00	0.00
118	0.00	0.43	-0.30	-1.09	0.00	0.00	0.00	0.00	0.10
119	0.00	0.43	-0.84	2.61	0.00	0.00	0.01	0.00	0.02
120	0.00	0.48	0.06	0.50	0.00	0.00	0.00	0.00	0.00

Tot.cons.

94.84 98.19 0.00 68.29

Elenco coefficienti di risposta**Simbologia**

Modo = Numero del modo di vibrare

Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X

Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di operatività

Modo	Sx	Sy
1	17.19	17.19
2	12.99	12.99
3	11.28	11.28
4	9.64	9.64
5	9.28	9.28
6	9.00	9.00
7	8.88	8.88
8	8.87	8.87
9	8.79	8.79
10	8.75	8.75
11	8.64	8.64
12	8.51	8.51
13	8.42	8.42
14	8.38	8.38
15	8.34	8.34
16	8.33	8.33
17	8.28	8.28
18	8.16	8.16
19	8.13	8.13
20	8.08	8.08
21	8.05	8.05
22	8.03	8.03
23	7.96	7.96
24	7.95	7.95
25	7.87	7.87
26	7.83	7.83
27	7.83	7.83
28	7.76	7.76
29	7.70	7.70
30	7.69	7.69
31	7.66	7.66
32	7.64	7.64
33	7.59	7.59
34	7.57	7.57
35	7.57	7.57
36	7.56	7.56
37	7.54	7.54
38	7.52	7.52
39	7.51	7.51
40	7.50	7.50
41	7.49	7.49
42	7.48	7.48
43	7.45	7.45
44	7.44	7.44
45	7.44	7.44
46	7.43	7.43
47	7.42	7.42
48	7.41	7.41
49	7.41	7.41
50	7.40	7.40
51	7.37	7.37
52	7.36	7.36
53	7.36	7.36
54	7.35	7.35
55	7.34	7.34
56	7.34	7.34
57	7.33	7.33
58	7.32	7.32
59	7.32	7.32
60	7.31	7.31
61	7.31	7.31
62	7.30	7.30
63	7.29	7.29
64	7.29	7.29
65	7.28	7.28
66	7.26	7.26
67	7.26	7.26
68	7.26	7.26
69	7.25	7.25
70	7.25	7.25

71	7.24	7.24
72	7.23	7.23
73	7.23	7.23
74	7.22	7.22
75	7.22	7.22
76	7.20	7.20
77	7.20	7.20
78	7.20	7.20
79	7.19	7.19
80	7.19	7.19
81	7.18	7.18
82	7.18	7.18
83	7.17	7.17
84	7.17	7.17
85	7.16	7.16
86	7.16	7.16
87	7.15	7.15
88	7.15	7.15
89	7.15	7.15
90	7.15	7.15
91	7.15	7.15
92	7.15	7.15
93	7.14	7.14
94	7.14	7.14
95	7.14	7.14
96	7.14	7.14
97	7.14	7.14
98	7.13	7.13
99	7.13	7.13
100	7.13	7.13
101	7.12	7.12
102	7.12	7.12
103	7.11	7.11
104	7.11	7.11
105	7.10	7.10
106	7.10	7.10
107	7.10	7.10
108	7.09	7.09
109	7.09	7.09
110	7.08	7.08
111	7.08	7.08
112	7.08	7.08
113	7.08	7.08
114	7.08	7.08
115	7.08	7.08
116	7.08	7.08
117	7.07	7.07
118	7.07	7.07
119	7.06	7.06
120	7.06	7.06

21	9.66	9.66
22	9.65	9.65
23	9.56	9.56
24	9.54	9.54
25	9.45	9.45
26	9.40	9.40
27	9.40	9.40
28	9.33	9.33
29	9.25	9.25
30	9.24	9.24
31	9.21	9.21
32	9.18	9.18
33	9.12	9.12
34	9.09	9.09
35	9.09	9.09
36	9.09	9.09
37	9.06	9.06
38	9.04	9.04
39	9.03	9.03
40	9.01	9.01
41	9.00	9.00
42	8.99	8.99
43	8.95	8.95
44	8.94	8.94
45	8.94	8.94
46	8.93	8.93
47	8.91	8.91
48	8.91	8.91
49	8.90	8.90
50	8.89	8.89
51	8.85	8.85
52	8.84	8.84
53	8.84	8.84
54	8.83	8.83
55	8.82	8.82
56	8.82	8.82
57	8.81	8.81
58	8.80	8.80
59	8.80	8.80
60	8.78	8.78
61	8.78	8.78
62	8.77	8.77
63	8.76	8.76
64	8.76	8.76
65	8.75	8.75
66	8.72	8.72
67	8.72	8.72
68	8.72	8.72
69	8.71	8.71
70	8.71	8.71
71	8.71	8.71
72	8.69	8.69
73	8.69	8.69
74	8.68	8.68
75	8.67	8.67
76	8.66	8.66
77	8.65	8.65
78	8.65	8.65
79	8.64	8.64
80	8.64	8.64
81	8.63	8.63
82	8.62	8.62
83	8.62	8.62
84	8.61	8.61
85	8.61	8.61
86	8.60	8.60
87	8.59	8.59
88	8.59	8.59
89	8.59	8.59
90	8.59	8.59
91	8.59	8.59
92	8.59	8.59
93	8.58	8.58
94	8.58	8.58
95	8.58	8.58

Stato limite di danno

Modo	Sx	Sy
1	20.93	20.93
2	15.58	15.58
3	13.52	13.52
4	11.57	11.57
5	11.14	11.14
6	10.80	10.80
7	10.66	10.66
8	10.64	10.64
9	10.56	10.56
10	10.51	10.51
11	10.38	10.38
12	10.22	10.22
13	10.11	10.11
14	10.06	10.06
15	10.02	10.02
16	10.00	10.00
17	9.94	9.94
18	9.80	9.80
19	9.76	9.76
20	9.70	9.70

96 8.58 8.58
 97 8.57 8.57
 98 8.57 8.57
 99 8.57 8.57
 100 8.56 8.56
 101 8.56 8.56
 102 8.56 8.56
 103 8.55 8.55
 104 8.54 8.54
 105 8.54 8.54
 106 8.54 8.54
 107 8.53 8.53
 108 8.52 8.52
 109 8.52 8.52
 110 8.51 8.51
 111 8.51 8.51
 112 8.51 8.51
 113 8.51 8.51
 114 8.51 8.51
 115 8.50 8.50
 116 8.50 8.50
 117 8.50 8.50
 118 8.49 8.49
 119 8.49 8.49
 120 8.49 8.49

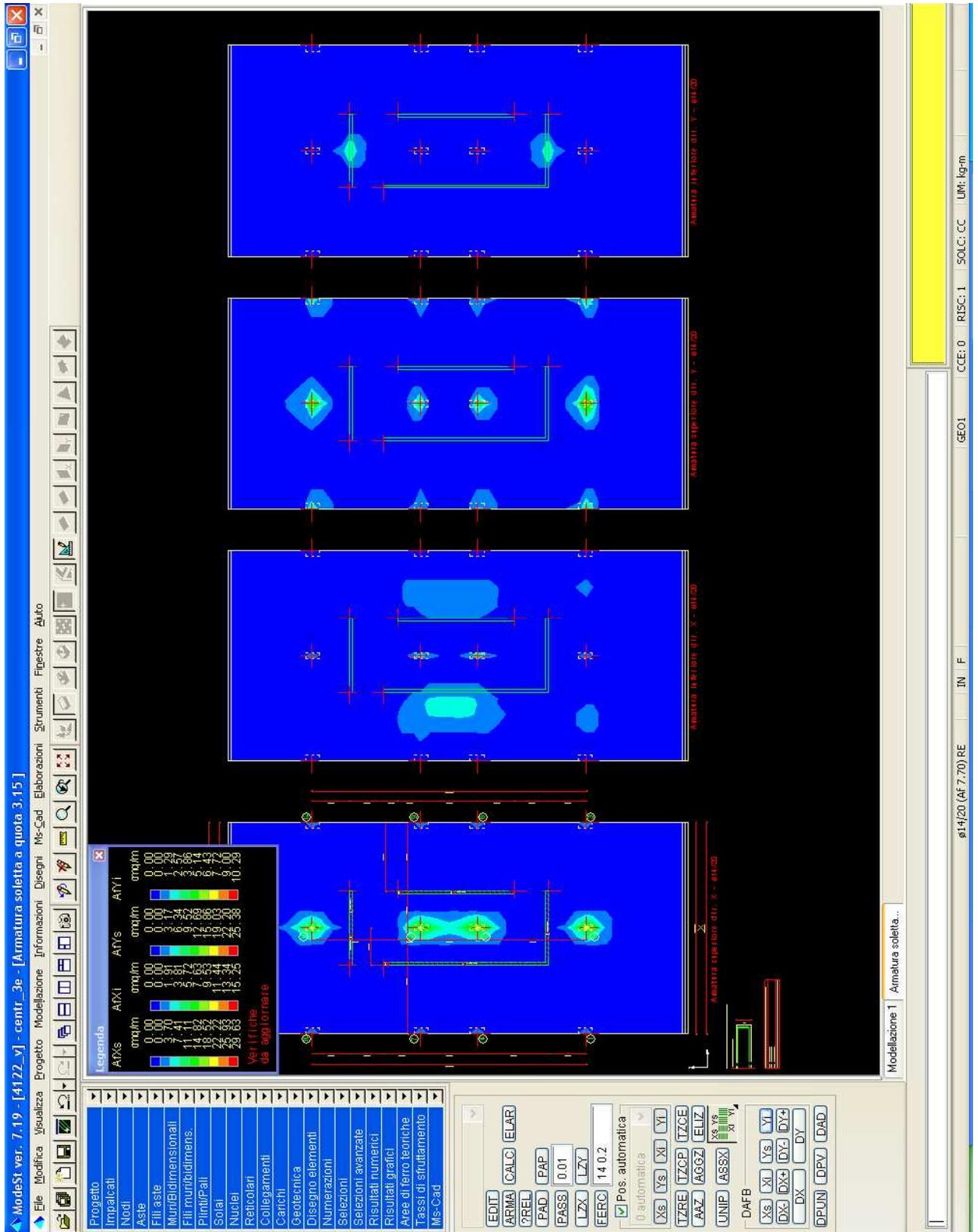
Stato limite di salvaguardia della vita

Modo Sx Sy
 1 30.16 30.16
 2 24.92 24.92
 3 23.29 23.29
 4 21.74 21.74
 5 21.40 21.40
 6 21.13 21.13
 7 21.02 21.02
 8 21.00 21.00
 9 20.94 20.94
 10 20.90 20.90
 11 20.79 20.79
 12 20.67 20.67
 13 20.58 20.58
 14 20.54 20.54
 15 20.51 20.51
 16 20.49 20.49
 17 20.45 20.45
 18 20.33 20.33
 19 20.30 20.30
 20 20.26 20.26

21 20.23 20.23
 22 20.22 20.22
 23 20.15 20.15
 24 20.13 20.13
 25 20.06 20.06
 26 20.02 20.02
 27 20.02 20.02
 28 19.96 19.96
 29 19.90 19.90
 30 19.89 19.89
 31 19.87 19.87
 32 19.85 19.85
 33 19.80 19.80
 34 19.78 19.78
 35 19.77 19.77
 36 19.77 19.77
 37 19.75 19.75
 38 19.73 19.73
 39 19.72 19.72
 40 19.71 19.71
 41 19.70 19.70
 42 19.69 19.69
 43 19.66 19.66
 44 19.66 19.66
 45 19.65 19.65
 46 19.65 19.65
 47 19.63 19.63
 48 19.63 19.63
 49 19.62 19.62
 50 19.61 19.61
 51 19.58 19.58
 52 19.58 19.58
 53 19.57 19.57
 54 19.56 19.56
 55 19.56 19.56
 56 19.56 19.56
 57 19.55 19.55
 58 19.54 19.54
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 61 19.53 19.53
 62 19.52 19.52
 63 19.51 19.51
 64 19.51 19.51
 65 19.50 19.50
 66 19.48 19.48
 67 19.48 19.48
 68 19.48 19.48
 69 19.47 19.47
 70 19.47 19.47
 71 19.47 19.47

72 19.45 19.45
 73 19.45 19.45
 74 19.45 19.45
 75 19.44 19.44
 76 19.43 19.43
 77 19.42 19.42
 78 19.42 19.42
 79 19.42 19.42
 80 19.41 19.41
 81 19.41 19.41
 82 19.40 19.40
 83 19.40 19.40
 84 19.40 19.40
 85 19.39 19.39
 86 19.39 19.39
 87 19.38 19.38
 88 19.38 19.38
 89 19.38 19.38
 90 19.38 19.38
 91 19.38 19.38
 92 19.37 19.37
 93 19.37 19.37
 94 19.37 19.37
 95 19.37 19.37
 96 19.36 19.36
 97 19.36 19.36
 98 19.36 19.36
 99 19.36 19.36
 100 19.35 19.35
 101 19.35 19.35
 102 19.35 19.35
 103 19.34 19.34
 104 19.34 19.34
 105 19.33 19.33
 106 19.33 19.33
 107 19.33 19.33
 108 19.32 19.32
 109 19.32 19.32
 110 19.31 19.31
 111 19.31 19.31
 112 19.31 19.31
 113 19.31 19.31
 114 19.31 19.31
 115 19.31 19.31
 116 19.31 19.31
 117 19.30 19.30
 118 19.30 19.30
 119 19.30 19.30
 120 19.29 19.29

7.2. MAPPE D'ARMATURA SOLETTA PIANO TERRA



ModeSt ver. 7.19 - [4122_v] - centr_3e - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto Impalcati Nodi Aste Fili aste Fili multidimensionali Plinti/Pali Soletta Nuclei Reticolari Collegamenti Canchi Geotecnica Disegno elementi Numerazioni Selezioni Selezioni avanzate Risultati numerici Risultati grafici Aree di ferro teoriche Tassi di sfruttamento Ms-Cad

Legenda

ADXS	ADXI	ATVs	ATYI
0,00	0,00	0,00	0,00
3,70	3,70	3,70	3,70
7,41	7,41	7,41	7,41
11,11	11,11	11,11	11,11
14,82	14,82	14,82	14,82
18,52	18,52	18,52	18,52
22,23	22,23	22,23	22,23
25,93	25,93	25,93	25,93
29,63	29,63	29,63	29,63

Verifiche da aggiornare

ARMATURA SUPERIORE Q.T. X - 0,00-30
ARMATURA SUPERIORE Q.T. Y - 0,00-30
ARMATURA SUPERIORE Q.T. X - 0,00-30
ARMATURA SUPERIORE Q.T. Y - 0,00-30

Modellazione 1 Armatura soletta...

Selezionare la zona di armatura (diffusa o concentrata) alla quale assegnare l'armatura corrente

CCE: 0 RISC: 1 SOLC: CC UMI: Iq-m AAZ

28.33 -7.81 GEO1

ø18/20 (AF 12.72) RE IN F

Selezionare la zona

EDIT ARMA CALC ELAR
ZREL
PAD PAP
PASS 0.01
LZX LZV
EERC 18 0.2
 Pos. automatica
D automatica
XS Ys XI YI
TZRE TZCP TZOE
AAZ AGOZ ELIZ
UNIP ASSX
DAFB
XS XI YS YI
DX DX+ DY DY+
DX DY
DPUN DPV DAD

ModeSt ver. 7.19 - [4122_v] - centr_3e - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Fibrebre Aiuto

Legenda

ADXS	ADXI	ATVs	ATYI
0.00	0.00	0.00	0.00
3.70	3.34	3.10	3.29
7.41	6.68	6.20	6.57
11.11	9.92	9.30	9.86
14.82	13.63	12.80	13.54
18.52	17.33	16.40	17.43
22.23	21.03	19.90	21.38
25.93	24.73	23.40	25.29

Verifiche da aggiornare

Progetto

- Impalcati
- Nodi
- Aste
- Fili aste
- Multipidimensionali
- Fili multidimens.
- Plinti/Pali
- Solai
- Nucleri
- Reticolari
- Collegamenti
- Canichi
- Geotecnica
- Disegno elementi
- Numerazioni
- Selezioni
- Selezioni avanzate
- Risultati numerici
- Risultati grafici
- Arete di ferro teoriche
- Tassi di sfruttamento
- Ms-Cad

EDIT

ARMA CALC ELAR

ZREL

PAD PAP

PASS 0.01

LZX LZV

EERC 22 0.2

Pos. automatica

automatica

X8 Y8 X1 Y1

TZRE TZCP TZOE

AAZ AGOZ ELIZ

UNIP ASSX

DAFB

X8 X1 Y8 Y1

DX- DX+ DY- DY+

DX DY

DPUN DPV DAD

Modellazione 1 Armatura soletta...

Selezionare la zona

Selezionare la zona di armatura (diffusa o concentrata) alla quale assegnare l'armatura corrente

CCE: 0 RISC: 1 SOLC: CC UMI: Iq-m AAZ

33.67 -0.96 GEO1

ø22/20 (AF 19.0) RE IN F

ModeSt ver. 7.19 - [4122_v] - centr_3e - [Armatura soletta a quota 3.15]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto Impalcati Nodi Aste Fili aste MultiDimensionali Fili multidimens. Pilinti/Pali Soletta Nuclei Reticolari Collegamenti Canchi Geotecnica Disegno elementi Numerazioni Selezioni Selezioni avanzate Risultati numerici Risultati grafici Aree di ferro teoriche Tassi di sfruttamento Ms-Cad

EDIT ARMA CALC ELAR ?REL PAD PAP PASS 0.01 LZ LZV EERC 22 0.14 Pos. automatica 0 automatica XS Ys Xi Yi TZRE TZCP TZOE AAZ AGOZ ELIZ UNIP ASSX DAFB XS Xi Ys Yi DX- DX+ DY- DY+ DPUN DPV DAD

Armatura superiore dir. X - Ø22/14

Armatura superiore dir. Y - Ø22/14

Armatura inferiore dir. X - Ø22/14

Legenda

AXI	AYI	AXI	AYI
0.00	0.00	0.00	0.00
3.70	3.17	0.00	0.00
11.41	8.94	0.00	0.00
18.52	14.56	0.00	0.00
22.72	19.03	0.00	0.00
25.93	22.20	0.00	0.00
29.14	25.38	0.00	0.00

Modellazione 1 Armatura soletta...

Selezionare la zona

Selezionare la zona di armatura (diffusa o concentrata) alla quale assegnare l'armatura corrente

CCE: 0 RISC: 1 SOLC: CC UMI: Iq-m AAZ

15.24 -8.32 GEO1

Ø22/14 (AF 27.15) RE IN F

7.3. PARAMETRI DI CALCOLO PER CALCOLO FONDAZIONI CABINA ENEL

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
ModeSt ver. 7.19, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
Xfinest ver. 8.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica dinamica
Schematizzazione piani rigidi: metodo Master-Slave
Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <kg/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: ISOSHELL
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: No
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per Buckling: No
- Trascura Buckling torsionale: No

Dati struttura

- Zona sismica: zona 3
- Sito di costruzione: LON. 11.18240 LAT. 43.75800
Contenuto tra ID reticolo: 20058 20057 20280 20279

Simbologia

TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 Ag = Accelerazione orizzontale massima al sito
 FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

TCC Ag FO TC*
 SLO 0.4461 2.57 0.25
 SLD 0.5363 2.60 0.26

SLV 1.2629 2.39 0.30

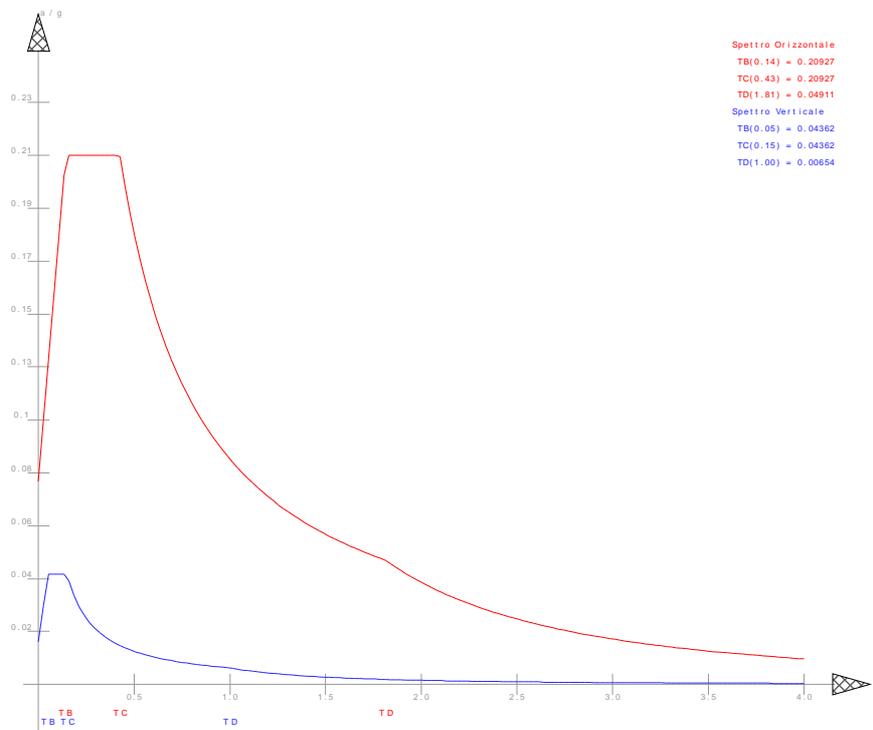
- Tipo di opera: Opera ordinaria
- Vita nominale V_N : 50.00
- Classe d'uso: classe II
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 6.50 <m>
- Numero piani edificio: 1
- Coefficiente θ : 0
- Edificio regolare in altezza: no
- Edificio regolare in pianta: no
- Forze orizzontali convenzionali per stati limite non sismici: no

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. o prefabbricato a telaio a più piani e più campate

Coeff. C_1	0.075
Periodo T_1	0.30531
Coeff. λ SLO	1.00
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovrarresistenza (α_s/α_c)	1.15
Valore di riferimento del fattore di struttura (q_0)	3.45
Fattore riduttivo (K_w)	1.00
Fattore di struttura (q)	1.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica: 1.00
- Modi da calcolare: 120
- Modi da considerare: con singola massa superiore a 1.00%
- Smorzamento spettro: 5.00

**Figura numero 2: Spettro allo SLD**

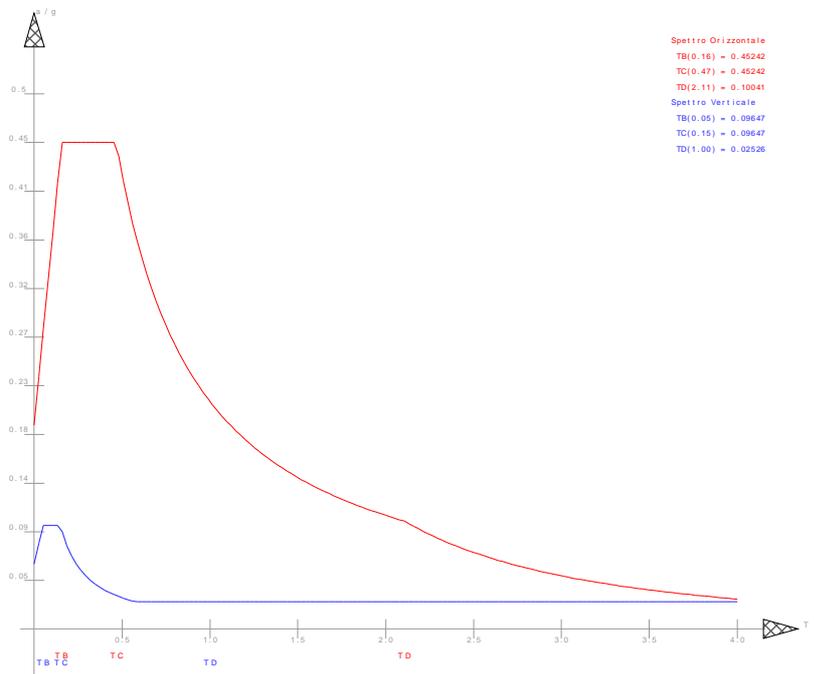


Figura numero 3: Spettro allo SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Dati di piano

Simbologia

- Imp. = Numero dell'impalcato
- Lx = Dimensione del piano in dir. X
- Ly = Dimensione del piano in dir. Y
- Ex = Eccentricità in dir. X
- Ey = Eccentricità in dir. Y
- Ea = Eccentricità complessiva

Imp.	Lx	Ly	Ex	Ey	Ea
<m>	<m>	<m>	<m>	<m>	<m>
1	4.30	11.51	0.22	0.58	0.61

Condizioni di carico elementari

Simbologia

- CCE = Numero della condizione di carico elementare
- Comm. = Commento
- s = Coeff. di riduzione
- Mx = Moltiplicatore della massa in dir. X
- My = Moltiplicatore della massa in dir. Y
- Mz = Moltiplicatore della massa in dir. Z
- Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
- Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
- Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	s	Mx	My	Mz	Jpx	Jpy	Jpz
1	pp e perm	1.00	1.00	1.00	0.00	0.00	0.00	1.00
2	permanente solette	1.00	1.00	1.00	0.00	0.00	0.00	1.00
3	parcheggio	1.00	1.00	1.00	0.00	0.00	0.00	1.00
4	carrabile	1.00	1.00	1.00	0.00	0.00	0.00	1.00
5	copertura (1)	1.00	1.00	1.00	0.00	0.00	0.00	1.00
6	PERMANENTE PORTATO SOLAIO	1.00	1.00	1.00	0.00	0.00	0.00	1.00
7	spinta statica della terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
8	spinta accidentale terra	1.00	0.00	0.00	0.00	0.00	0.00	0.00
9	VARIAZIONE TERMICA UNIFORME	1.00	0.00	0.00	0.00	0.00	0.00	0.00
10	Momento torcente - SLO	--	--	--	--	--	--	--
11	Sisma dir. X - SLO	--	--	--	--	--	--	--
12	Sisma dir. Y - SLO	--	--	--	--	--	--	--
13	Momento torcente - SLD	--	--	--	--	--	--	--

14	Sisma dir. X - SLD	--	--	--	--	--	--	--	--	--	--	--
15	Sisma dir. Y - SLD	--	--	--	--	--	--	--	--	--	--	--
16	Momento torcente - SLV	--	--	--	--	--	--	--	--	--	--	--
17	Sisma dir. X - SLV	--	--	--	--	--	--	--	--	--	--	--
18	Sisma dir. Y - SLV	--	--	--	--	--	--	--	--	--	--	--

Ambienti di carico**simbologia**

N Numero

Comm. Commento

1 pp e perm

2 permanente solette

3 parcheggio

4 carrabile

5 copertura (1)

6 PERMANENTE PORTATO SOLAIO

7 spinta statica della terra

8 spinta accidentale terra

9 VARIAZIONE TERMICA UNIFORME

F azioni orizzontali convenzionali

SLU Stato limite ultimo

SLR Stato limite per combinazioni rare

SLF Stato limite per combinazioni frequenti

SLQ Stato limite per combinazioni quasi permanenti o di danno

N Comm.	1	2	3	4	5	6	7	8	9	S	SLU	SLR	SLF	SLQ
1 Calcolo sismico	si	no	no	no										
2 Calcolo statico	si	no	si	si	si	si	si							

Combinazioni delle cce**Simbologia**

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLU S = Stato limite ultimo (azione sismica)

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SLV = Stato limite di salvaguardia della vita

SLC = Stato limite di prevenzione del collasso

SLO = Stato limite di operatività

An. = Tipo di analisi

L = Lineare

NL = Non lineare

Bk = Buckling

S = Si

N = No

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	8	9	Mt	±S X	±S Y
1	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30
2	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30
3	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	0.30	1.00
4	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	-0.30	1.00
5	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	0.30
6	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	-0.30
7	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	0.30	1.00
8	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	-0.30	1.00
9	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	0.30
10	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	1.00	-0.30
11	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	0.30	1.00
12	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	-0.30	1.00
13	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	0.30
14	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	1.00	-0.30
15	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	0.30	1.00
16	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-1.00	-0.30	1.00
17	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	0.30	0.30
18	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	-0.30	-0.30
19	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30
20	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30
21	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	0.30	0.30
22	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	-0.30	-0.30
23	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30
24	sismica	SLV	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30
25	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	0.30	0.30
26	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	-0.30	-0.30

27	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30	
28	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30	
29	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	0.30	0.30	
30	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	1.00	-0.30	-0.30	
31	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	0.30	1.00	0.30	
32	sismica	SLD	L	N	1.00	1.00	0.60	0.15	0.00	1.00	1.00	0.15	0.00	-0.30	1.00	-0.30	
33	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	0.90	0.00	0.00	0.00	
34	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	-0.90	0.00	0.00	0.00	
35	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	0.90	0.00	0.00	0.00	
36	statica copertura	SLU	L	N	1.30	1.50	1.05	0.60	1.50	1.50	1.30	0.60	-0.90	0.00	0.00	0.00	
37	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	0.90	0.00	0.00	0.00	
38	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	-0.90	0.00	0.00	0.00	
39	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	0.90	0.00	0.00	0.00	
40	statica (piazza)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	1.50	1.30	1.50	-0.90	0.00	0.00	0.00	
41	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	0.90	0.00	0.00	0.00	
42	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	-0.90	0.00	0.00	0.00	
43	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	0.90	0.00	0.00	0.00	
44	statica (parcheggio)	SLU	L	N	1.30	1.50	1.50	0.60	0.75	1.50	1.30	0.60	-0.90	0.00	0.00	0.00	
45	statica copertura	SLE	R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	0.40	0.60	0.00	0.00	0.00	
46	statica copertura	SLE	R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	0.40	-0.60	0.00	0.00	0.00	
47	statica copertura	SLE	R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	0.40	0.60	0.00	0.00	0.00	
48	statica copertura	SLE	R	L	N	1.00	1.00	0.70	0.40	1.00	1.00	0.40	-0.60	0.00	0.00	0.00	
49	statica (piazza)	SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	0.60	0.00	0.00	0.00	
50	statica (piazza)	SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	-0.60	0.00	0.00	0.00	
51	statica (piazza)	SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	0.60	0.00	0.00	0.00	
52	statica (piazza)	SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	1.00	1.00	-0.60	0.00	0.00	0.00	
53	statica (parcheggio)	SLE	R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	0.60	0.00	0.00	0.00
54	statica (parcheggio)	SLE	R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	-0.60	0.00	0.00	0.00
55	statica (parcheggio)	SLE	R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	0.60	0.00	0.00	0.00
56	statica (parcheggio)	SLE	R	L	N	1.00	1.00	1.00	0.40	0.50	1.00	1.00	0.40	-0.60	0.00	0.00	0.00
57	statica copertura	SLE	F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
58	statica copertura	SLE	F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
59	statica copertura	SLE	F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
60	statica copertura	SLE	F	L	N	1.00	1.00	0.60	0.00	0.20	1.00	1.00	0.00	0.00	0.00	0.00	0.00
61	statica (piazza)	SLE	F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
62	statica (piazza)	SLE	F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
63	statica (piazza)	SLE	F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
64	statica (piazza)	SLE	F	L	N	1.00	1.00	0.60	0.40	0.00	1.00	1.00	0.40	0.00	0.00	0.00	0.00
65	statica (parcheggio)	SLE	F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
66	statica (parcheggio)	SLE	F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
67	statica (parcheggio)	SLE	F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
68	statica (parcheggio)	SLE	F	L	N	1.00	1.00	0.70	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
69		SLE	Q	L	N	1.00	1.00	0.60	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00
70		SLE	Q	L	N	1.00	1.00	0.60	0.00	0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00

Elenco baricentri e masse impalcati

Simbologia

Imp. = Numero dell'impalcato
 X = Coordinata X
 Y = Coordinata Y
 Z = Coordinata Z
 Mo = Massa orizzontale
 Jpz = Momento d'inerzia polare intorno all'asse Z

Imp.	X	Y	Z	Mo	Jpz
<m>	<m>	<m>	<KG>	<KG>	<KG*mq>
1	0.01	14.50	6.50	2908.77	41502.40

Totali masse impalcati

Mo	Jpz
<KG>	<KG*mq>
2908.77	41502.40

Elenco masse nodi

Simbologia

Nodo = Numero del nodo
 Mo = Massa orizzontale

Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo
<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>	<KG>
-1002	113.46	-1001	210.85	-1000	204.52	-997	13.19	-994	113.46	-993	210.85	-992	204.52
-990	159.09	-989	148.96	-988	159.09	-987	131.64	-986	138.57	-985	148.96	-976	13.19
-974	22.94	-973	24.66	-972	11.81	-971	22.09	-970	11.81	-969	22.09	-968	11.81
-966	22.09	-965	20.55	-964	22.09	-963	20.55	-940	11.81	-939	22.09	-938	20.55
-936	11.81	-935	17.36	-934	11.25	-933	28.61	-932	26.71	-931	26.71	-930	38.41
-928	45.89	-927	45.89	-926	45.89	-925	45.89	-924	46.32	-923	46.32	-922	43.66
-920	20.29	-919	39.81	-918	40.17	-917	23.63	-916	44.18	-915	41.09	-914	44.18
-912	12.50	-911	23.37	-910	21.74	-909	23.37	-908	12.50	-907	18.37	-906	11.90
-904	28.26	-903	28.26	-901	40.64	-900	40.64	-899	48.56	-898	48.56	-897	48.56
-895	49.01	-894	49.01	-893	46.20	-892	46.20	-890	21.47	-889	42.12	-888	42.50
-885	46.74	-884	43.48	-883	46.74	-882	46.85	-880	68.66	-878	127.60	-877	123.77
-875	111.99	-874	126.72	-873	117.88	-872	126.72	-871	111.99	-870	109.04	-869	123.77
-866	68.66	-865	138.03	-863	256.51	-862	248.81	-861	219.19	-860	225.11	-859	254.73
-857	254.73	-856	225.11	-855	219.19	-854	248.81	-853	256.51	-851	138.03	-850	138.58
-847	249.79	-846	220.06	-845	226.00	-844	255.74	-843	237.90	-842	255.74	-841	226.00
-839	249.79	-838	257.53	-836	138.58	-835	145.48	-833	270.35	-832	262.23	-831	231.01
-829	268.48	-828	249.74	-827	268.48	-826	237.26	-825	231.01	-824	262.23	-823	270.35
-820	287.68	-818	299.66	-817	290.66	-816	291.90	-815	353.77	-814	400.32	-813	400.32

-811	291.90	-810	290.66	-809	299.66	-808	287.68	-792	128.71	-790	239.18	-789	232.00	-788	267.31
-787	369.33	-786	417.93	-785	388.77	-784	417.93	-783	369.33	-782	267.31	-781	232.00	-780	239.18
-778	128.71	-777	112.14	-775	208.40	-774	202.14	-773	194.63	-772	231.42	-771	266.73	-770	248.13
-769	266.73	-768	231.42	-767	194.63	-766	202.14	-765	208.40	-763	112.14	-762	106.28	-760	197.50
-759	191.57	-758	149.02	-757	123.30	-756	139.53	-755	129.79	-754	139.53	-753	166.91	-752	182.94
-751	191.57	-750	197.50	-748	106.28	-747	81.65	-745	151.74	-744	147.18	-743	136.15	-742	122.67
-741	107.20	-740	99.72	-739	107.20	-738	166.28	-737	170.07	-736	147.18	-735	151.74	-733	81.65
-732	76.23	-730	141.66	-729	137.41	-728	158.32	-727	154.78	-726	100.08	-725	93.09	-724	100.08
-723	154.78	-722	158.32	-721	137.41	-720	141.66	-718	76.23	-717	236.03	-715	203.68	-714	197.56
-713	227.63	-712	222.55	-711	143.89	-710	143.89	-709	222.55	-708	227.63	-707	197.56	-706	203.68
-705	236.03	-704	130.95	-702	243.36	-701	236.05	-700	271.98	-699	265.90	-698	171.93	-697	159.93
-696	171.93	-695	265.90	-694	271.98	-693	236.05	-692	243.36	-690	130.95	-689	130.95	-687	243.36
-686	236.05	-685	271.98	-684	265.90	-683	171.93	-682	159.93	-681	171.93	-680	265.90	-679	271.98
-678	236.05	-677	243.36	-675	130.95	-674	258.61	-672	245.63	-671	238.26	-670	274.52	-669	268.39
-668	173.53	-667	173.53	-666	268.39	-665	274.52	-664	238.26	-663	245.63	-662	258.61	-661	124.60
-659	231.56	-658	224.60	-657	258.79	-656	253.01	-655	163.59	-654	152.17	-653	163.59	-652	253.01
-651	258.79	-650	224.60	-649	231.56	-647	124.60	-646	113.61	-644	211.12	-643	204.79	-642	198.37
-641	182.20	-640	149.15	-639	138.75	-638	149.15	-637	230.68	-636	235.95	-635	204.79	-634	211.12
-632	113.61	-631	114.63	-629	213.03	-628	206.63	-627	160.74	-626	133.00	-625	150.50	-624	140.00
-623	150.50	-622	232.77	-621	238.09	-620	206.63	-619	213.03	-617	114.63	-616	114.34	-614	212.49
-613	206.11	-612	197.71	-611	240.56	-610	281.95	-609	262.28	-608	281.95	-607	291.85	-606	237.48
-605	206.11	-604	212.49	-602	114.34	-601	128.71	-599	239.18	-598	232.00	-597	267.31	-596	369.33
-595	417.93	-594	388.77	-593	417.93	-592	369.33	-591	267.31	-590	232.00	-589	239.18	-587	128.71
-571	243.71	-569	217.93	-568	211.39	-567	222.06	-566	282.05	-565	319.16	-564	319.16	-563	282.05
-562	222.06	-561	211.39	-560	217.93	-559	243.71	-558	87.95	-556	163.45	-555	158.54	-554	139.67
-553	143.44	-552	162.32	-551	150.99	-550	162.32	-549	143.44	-548	139.67	-547	158.54	-546	163.45
-544	87.95	-543	128.41	-541	238.64	-540	231.47	-539	203.92	-538	209.43	-537	236.99	-536	220.45
-535	236.99	-534	209.43	-533	203.92	-532	231.47	-531	238.64	-529	128.41	-528	160.66	-526	298.57
-525	289.61	-524	255.13	-523	262.02	-522	296.50	-521	275.82	-520	296.50	-519	262.02	-518	255.13
-517	289.61	-516	298.57	-514	160.66	-513	162.72	-511	302.38	-510	293.31	-509	258.39	-508	265.37
-507	300.29	-506	279.34	-505	300.29	-504	265.37	-503	258.39	-502	293.31	-501	302.38	-499	162.72
-483	109.87	-481	204.18	-480	198.05	-479	174.47	-478	179.18	-477	202.76	-476	188.62	-475	202.76
-474	179.18	-473	174.47	-472	198.05	-471	204.18	-469	109.87	-468	23.38	-466	43.45	-465	42.14
-464	37.13	-463	38.13	-462	43.15	-461	40.14	-460	43.15	-459	38.13	-458	37.13	-457	42.14
-456	43.45	-454	23.38	-453	46.76	-451	86.90	-450	84.29	-449	74.25	-448	76.26	-447	86.30
-446	80.28	-445	86.30	-444	76.26	-443	74.25	-442	84.29	-441	86.90	-439	46.76	-438	23.38
-436	43.45	-435	42.14	-434	37.13	-433	38.13	-432	43.15	-431	40.14	-430	43.15	-429	38.13
-428	37.13	-427	42.14	-426	43.45	-424	23.38	-423	46.76	-421	86.90	-420	84.29	-419	74.25
-418	76.26	-417	86.30	-416	80.28	-415	86.30	-414	76.26	-413	74.25	-412	84.29	-411	86.90
-409	46.76	14	423.32	16	287.86	18	260.29	20	498.82						

Totali masse nodi

Mo
<KG>
76217.20

Elenco forze sismiche di impalcato allo SLO**Simbologia**

Imp. = Numero dell'impalcato
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y
Mz = Momento intorno all'asse Z

Imp.	cx	cy	Mz
<kgm>			
1	0.07	0.07	6004.85

Totali forze sismiche

Mz
<kgm>
6004.85

Elenco forze sismiche di impalcato allo SLD

Imp.	cx	cy	Mz
<kgm>			
1	0.07	0.07	7310.50

Totali forze sismiche

Mz
<kgm>
7310.50

Elenco forze sismiche di impalcato allo SLV

Imp.	cx	cy	Mz
<kgm>			
1	0.07	0.07	15804.80

Totali forze sismiche

Mz
<kgm>
15804.80

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione

Simbologia

Modo = Numero del modo di vibrare
 C = * indica che il modo è stato considerato
 Per. = Periodo
 Diff. = Minima differenza percentuale dagli altri periodi
 Φ_x = Coefficiente di partecipazione in dir. X
 Φ_y = Coefficiente di partecipazione in dir. Y
 Φ_z = Coefficiente di partecipazione in dir. Z
 %Mx = Percentuale massa partecipante in dir. X
 %My = Percentuale massa partecipante in dir. Y
 %Mz = Percentuale massa partecipante in dir. Z
 %Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φ_x	Φ_y	Φ_z	%Mx	%My	%Mz	%Jpz
1	*	0.17	17.34	1.91	279.72	0.00	0.00	98.88	0.00	0.00
2	*	0.14	17.34	-276.70	2.02	0.00	96.76	0.01	0.00	0.01
3	*	0.08	34.76	17.05	-0.40	0.00	0.37	0.00	0.00	1.16
4		0.06	34.76	-22.57	-1.22	0.00	0.64	0.00	0.00	0.26
5	*	0.04	13.37	1.19	6.15	0.00	0.00	0.05	0.00	7.38
6	*	0.03	13.37	-29.76	0.10	0.00	1.12	0.00	0.00	0.02
7		0.03	0.99	0.08	0.03	0.00	0.00	0.00	0.00	0.86
8		0.03	0.99	0.43	0.09	0.00	0.00	0.00	0.00	0.00
9	*	0.03	0.52	-1.92	-0.09	0.00	0.00	0.00	0.00	5.96
10	*	0.03	0.52	-1.88	0.19	0.00	0.00	0.00	0.00	1.77
11	*	0.03	2.43	-0.83	-0.27	0.00	0.00	0.00	0.00	1.47
12		0.02	4.66	-0.06	-1.38	0.00	0.00	0.00	0.00	0.08
13		0.02	3.69	0.26	-0.26	0.00	0.00	0.00	0.00	0.87
14	*	0.02	3.44	-0.83	0.32	0.00	0.00	0.00	0.00	22.99
15		0.02	0.14	0.32	0.00	0.00	0.00	0.00	0.00	0.01
16		0.02	0.14	-0.28	0.00	0.00	0.00	0.00	0.00	0.00
17	*	0.02	1.95	1.43	-0.10	0.00	0.00	0.00	0.00	6.17
18	*	0.02	3.21	-0.64	-0.33	0.00	0.00	0.00	0.00	24.82
19	*	0.02	5.47	0.11	-0.22	0.00	0.00	0.00	0.00	3.03
20		0.02	1.58	-0.01	0.14	0.00	0.00	0.00	0.00	0.01
21		0.02	0.48	0.02	-0.08	0.00	0.00	0.00	0.00	0.42
22		0.02	0.48	-0.00	0.07	0.00	0.00	0.00	0.00	0.04
23		0.02	0.92	-0.01	-15.94	0.00	0.00	0.32	0.00	0.03
24		0.02	1.06	-2.47	0.04	0.00	0.01	0.00	0.00	0.00
25		0.02	3.88	-0.00	0.39	0.00	0.00	0.00	0.00	0.00
26		0.01	4.00	0.35	0.01	0.00	0.00	0.00	0.00	0.00
27		0.01	0.34	2.32	-0.01	0.00	0.01	0.00	0.00	0.12
28		0.01	0.34	0.01	-0.22	0.00	0.00	0.00	0.00	0.00
29		0.01	0.03	-1.37	-0.34	0.00	0.00	0.00	0.00	0.65
30		0.01	0.03	-0.49	-0.37	0.00	0.00	0.00	0.00	0.60
31		0.01	1.31	0.06	-18.25	0.00	0.00	0.42	0.00	0.07
32		0.01	1.31	0.01	-0.01	0.00	0.00	0.00	0.00	0.00
33		0.01	0.46	-0.02	-0.59	0.00	0.00	0.00	0.00	0.00
34		0.01	0.28	-0.01	-0.22	0.00	0.00	0.00	0.00	0.00
35		0.01	0.28	-1.44	-0.13	0.00	0.00	0.00	0.00	0.05
36		0.01	1.92	0.02	4.62	0.00	0.00	0.03	0.00	0.01
37		0.01	0.37	-0.04	0.19	0.00	0.00	0.00	0.00	0.00
38		0.01	0.37	-0.02	-8.51	0.00	0.00	0.09	0.00	0.03
39		0.01	0.99	-0.02	0.96	0.00	0.00	0.00	0.00	0.01
40		0.01	1.94	-0.07	0.01	0.00	0.00	0.00	0.00	0.00
41		0.01	0.22	-0.10	0.34	0.00	0.00	0.00	0.00	0.00
42		0.01	0.22	0.08	3.96	0.00	0.00	0.02	0.00	0.00
43		0.01	1.99	0.09	-0.21	0.00	0.00	0.00	0.00	0.00
44		0.01	1.13	-5.50	0.05	0.00	0.04	0.00	0.00	0.00
45		0.01	1.13	-0.04	0.00	0.00	0.00	0.00	0.00	0.00
46		0.01	0.67	-1.73	0.02	0.00	0.00	0.00	0.00	0.01
47		0.01	0.67	-0.09	-0.01	0.00	0.00	0.00	0.00	0.00
48		0.01	1.75	-0.12	0.03	0.00	0.00	0.00	0.00	0.08
49		0.01	1.75	0.09	0.01	0.00	0.00	0.00	0.00	0.05
50		0.01	3.70	0.02	0.18	0.00	0.00	0.00	0.00	0.00
51		0.01	1.38	-0.11	0.19	0.00	0.00	0.00	0.00	0.00
52		0.01	1.38	0.04	0.06	0.00	0.00	0.00	0.00	0.00
53		0.01	1.88	1.25	0.00	0.00	0.00	0.00	0.00	0.00
54		0.01	2.80	0.00	0.06	0.00	0.00	0.00	0.00	0.00
55		0.01	0.90	0.22	0.00	0.00	0.00	0.00	0.00	0.00
56		0.01	0.25	-0.01	-0.03	0.00	0.00	0.00	0.00	0.00
57		0.01	0.25	0.04	1.21	0.00	0.00	0.00	0.00	0.00
58		0.01	1.45	0.25	-0.03	0.00	0.00	0.00	0.00	0.17
59		0.01	0.15	-2.15	0.01	0.00	0.01	0.00	0.00	0.01
60		0.01	0.15	1.36	-0.04	0.00	0.00	0.00	0.00	0.02
61		0.01	0.98	-1.03	0.15	0.00	0.00	0.00	0.00	0.00
62		0.01	1.10	-0.21	-0.02	0.00	0.00	0.00	0.00	0.08
63		0.01	0.41	-0.21	0.05	0.00	0.00	0.00	0.00	0.00
64		0.01	0.41	-2.38	-0.07	0.00	0.01	0.00	0.00	0.00
65		0.01	1.68	-0.01	-0.19	0.00	0.00	0.00	0.00	0.00
66		0.01	0.24	-0.07	-0.00	0.00	0.00	0.00	0.00	0.00
67		0.01	0.24	0.02	-0.11	0.00	0.00	0.00	0.00	0.00
68		0.01	0.24	0.66	-0.00	0.00	0.00	0.00	0.00	0.08
69		0.01	0.24	0.40	-0.00	0.00	0.00	0.00	0.00	0.13
70		0.01	2.95	0.00	0.28	0.00	0.00	0.00	0.00	0.00
71		0.01	0.81	1.16	0.12	0.00	0.00	0.00	0.00	0.00
72		0.01	0.81	1.24	-0.12	0.00	0.00	0.00	0.00	0.00
73		0.01	1.59	-0.05	-2.00	0.00	0.00	0.01	0.00	0.00
74		0.01	1.06	0.16	-0.29	0.00	0.00	0.00	0.00	0.31
75		0.01	0.05	1.06	-0.13	0.00	0.00	0.00	0.00	0.02
76		0.01	0.05	-0.07	-0.07	0.00	0.00	0.00	0.00	0.00
77		0.01	0.17	-0.37	-0.25	0.00	0.00	0.00	0.00	0.00
78		0.01	0.72	-0.01	-0.00	0.00	0.00	0.00	0.00	0.00
79		0.01	0.72	0.08	0.10	0.00	0.00	0.00	0.00	0.00
80		0.01	2.36	0.89	-0.01	0.00	0.00	0.00	0.00	0.00
81		0.01	1.16	0.84	0.00	0.00	0.00	0.00	0.00	0.00
82		0.01	0.82	-0.02	-0.01	0.00	0.00	0.00	0.00	0.00

83	0.01	0.35	0.09	-0.12	0.00	0.00	0.00	0.00	0.00
84	0.01	0.05	0.38	-0.03	0.00	0.00	0.00	0.00	0.04
85	0.01	0.05	-0.19	0.04	0.00	0.00	0.00	0.00	0.00
86	0.01	0.24	-0.27	-0.00	0.00	0.00	0.00	0.00	0.02
87	0.01	0.34	-0.62	0.03	0.00	0.00	0.00	0.00	0.01
88	0.01	0.34	-1.39	-0.04	0.00	0.00	0.00	0.00	0.00
89	0.01	0.17	0.79	0.02	0.00	0.00	0.00	0.00	0.00
90	0.01	0.17	1.38	-0.01	0.00	0.00	0.00	0.00	0.00
91	0.01	0.36	-1.82	-0.01	0.00	0.00	0.00	0.00	0.00
92	0.01	0.28	-2.40	-0.07	0.00	0.01	0.00	0.00	0.01
93	0.01	0.28	0.32	0.08	0.00	0.00	0.00	0.00	0.01
94	0.01	0.07	-0.26	-0.02	0.00	0.00	0.00	0.00	0.04
95	0.01	0.07	1.59	-0.05	0.00	0.00	0.00	0.00	0.01
96	0.01	0.58	-0.80	-0.04	0.00	0.00	0.00	0.00	0.13
97	0.01	0.13	-2.13	0.04	0.00	0.01	0.00	0.00	0.03
98	0.01	0.13	0.61	0.04	0.00	0.00	0.00	0.00	0.00
99	0.01	0.25	0.23	-0.04	0.00	0.00	0.00	0.00	0.00
100	0.01	0.76	0.08	0.03	0.00	0.00	0.00	0.00	0.03
101	0.01	0.19	-0.08	0.11	0.00	0.00	0.00	0.00	0.00
102	0.01	0.19	0.01	0.01	0.00	0.00	0.00	0.00	0.00
103	0.01	0.13	0.00	0.01	0.00	0.00	0.00	0.00	0.00
104	0.01	0.13	-0.04	0.05	0.00	0.00	0.00	0.00	0.02
105	0.00	1.59	-0.15	0.08	0.00	0.00	0.00	0.00	0.00
106	0.00	0.29	-0.47	0.01	0.00	0.00	0.00	0.00	0.02
107	0.00	0.29	-0.05	-0.01	0.00	0.00	0.00	0.00	0.00
108	0.00	0.53	1.27	0.03	0.00	0.00	0.00	0.00	0.06
109	0.00	0.80	-0.15	0.00	0.00	0.00	0.00	0.00	0.00
110	0.00	0.15	-0.02	-0.08	0.00	0.00	0.00	0.00	0.00
111	0.00	0.15	0.10	0.01	0.00	0.00	0.00	0.00	0.00
112	0.00	0.54	0.65	0.04	0.00	0.00	0.00	0.00	0.00
113	0.00	0.54	0.96	-0.01	0.00	0.00	0.00	0.00	0.01
114	0.00	0.58	1.24	-0.14	0.00	0.00	0.00	0.00	0.02
115	0.00	0.73	0.27	-0.27	0.00	0.00	0.00	0.00	0.00
116	0.00	0.04	1.50	-0.02	0.00	0.00	0.00	0.00	0.04
117	0.00	0.04	-0.64	0.07	0.00	0.00	0.00	0.00	0.01
118	0.00	0.90	0.34	0.41	0.00	0.00	0.00	0.00	0.00
119	0.00	0.36	-4.20	0.00	0.00	0.02	0.00	0.00	0.00
120	0.00	0.36	0.41	0.17	0.00	0.00	0.00	0.00	0.00

Tot.cons.

98.27 98.94 0.00 74.78

Elenco coefficienti di risposta**Simbologia**

Modo = Numero del modo di vibrare

Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X

Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di operatività

Modo Sx	Sy
1	17.19 17.19
2	17.19 17.19
3	13.06 13.06
4	11.42 11.42
5	9.63 9.63
6	9.29 9.29
7	8.78 8.78
8	8.75 8.75
9	8.67 8.67
10	8.66 8.66
11	8.61 8.61
12	8.52 8.52
13	8.44 8.44
14	8.38 8.38
15	8.32 8.32
16	8.32 8.32
17	8.29 8.29
18	8.24 8.24
19	8.03 8.03
20	7.96 7.96
21	7.94 7.94
22	7.93 7.93
23	7.92 7.92
24	7.91 7.91
25	7.86 7.86
26	7.82 7.82
27	7.77 7.77
28	7.77 7.77
29	7.74 7.74
30	7.74 7.74
31	7.71 7.71
32	7.70 7.70
33	7.63 7.63
34	7.62 7.62
35	7.62 7.62
36	7.60 7.60
37	7.58 7.58
38	7.57 7.57
39	7.57 7.57
40	7.55 7.55
41	7.53 7.53
42	7.53 7.53

43	7.51	7.51
44	7.50	7.50
45	7.49	7.49
46	7.47	7.47
47	7.46	7.46
48	7.45	7.45
49	7.43	7.43
50	7.39	7.39
51	7.36	7.36
52	7.35	7.35
53	7.34	7.34
54	7.32	7.32
55	7.30	7.30
56	7.30	7.30
57	7.29	7.29
58	7.29	7.29
59	7.27	7.27
60	7.27	7.27
61	7.26	7.26
62	7.26	7.26
63	7.25	7.25
64	7.24	7.24
65	7.23	7.23
66	7.22	7.22
67	7.22	7.22
68	7.21	7.21
69	7.21	7.21
70	7.20	7.20
71	7.18	7.18
72	7.17	7.17
73	7.16	7.16
74	7.15	7.15
75	7.15	7.15
76	7.15	7.15
77	7.15	7.15
78	7.14	7.14
79	7.14	7.14
80	7.13	7.13
81	7.12	7.12
82	7.11	7.11
83	7.11	7.11
84	7.11	7.11
85	7.11	7.11
86	7.11	7.11
87	7.10	7.10
88	7.10	7.10

89	7.10	7.10
90	7.10	7.10
91	7.10	7.10
92	7.10	7.10
93	7.10	7.10
94	7.09	7.09
95	7.09	7.09
96	7.09	7.09
97	7.09	7.09
98	7.09	7.09
99	7.09	7.09
100	7.08	7.08
101	7.08	7.08
102	7.08	7.08
103	7.08	7.08
104	7.08	7.08
105	7.07	7.07
106	7.06	7.06
107	7.06	7.06
108	7.06	7.06
109	7.06	7.06
110	7.05	7.05
111	7.05	7.05
112	7.05	7.05
113	7.05	7.05
114	7.05	7.05
115	7.04	7.04
116	7.04	7.04
117	7.04	7.04
118	7.03	7.03
119	7.03	7.03
120	7.03	7.03

Stato limite di danno

Modo Sx	Sy
1	20.93 20.93
2	20.93 20.93
3	15.65 15.65
4	13.69 13.69
5	11.56 11.56
6	11.15 11.15
7	10.53 10.53
8	10.51 10.51
9	10.40 10.40
10	10.39 10.39

11	10.34	10.34
12	10.23	10.23
13	10.14	10.14
14	10.06	10.06
15	9.99	9.99
16	9.99	9.99
17	9.95	9.95
18	9.90	9.90
19	9.64	9.64
20	9.56	9.56
21	9.54	9.54
22	9.53	9.53
23	9.52	9.52
24	9.50	9.50
25	9.45	9.45
26	9.39	9.39
27	9.34	9.34
28	9.33	9.33
29	9.30	9.30
30	9.30	9.30
31	9.26	9.26
32	9.24	9.24
33	9.16	9.16
34	9.16	9.16
35	9.16	9.16
36	9.13	9.13
37	9.10	9.10
38	9.10	9.10
39	9.09	9.09
40	9.07	9.07
41	9.05	9.05
42	9.04	9.04
43	9.02	9.02
44	9.00	9.00
45	8.99	8.99
46	8.97	8.97
47	8.97	8.97
48	8.95	8.95
49	8.93	8.93
50	8.87	8.87
51	8.85	8.85
52	8.83	8.83
53	8.82	8.82
54	8.79	8.79
55	8.77	8.77
56	8.77	8.77
57	8.76	8.76
58	8.75	8.75
59	8.74	8.74
60	8.74	8.74
61	8.73	8.73
62	8.72	8.72
63	8.71	8.71
64	8.70	8.70
65	8.69	8.69
66	8.67	8.67
67	8.67	8.67
68	8.67	8.67
69	8.66	8.66
70	8.65	8.65
71	8.62	8.62
72	8.62	8.62
73	8.61	8.61
74	8.60	8.60
75	8.59	8.59
76	8.59	8.59
77	8.59	8.59
78	8.58	8.58
79	8.58	8.58
80	8.56	8.56
81	8.55	8.55
82	8.55	8.55
83	8.54	8.54
84	8.54	8.54
85	8.54	8.54
86	8.54	8.54
87	8.54	8.54
88	8.53	8.53
89	8.53	8.53
90	8.53	8.53

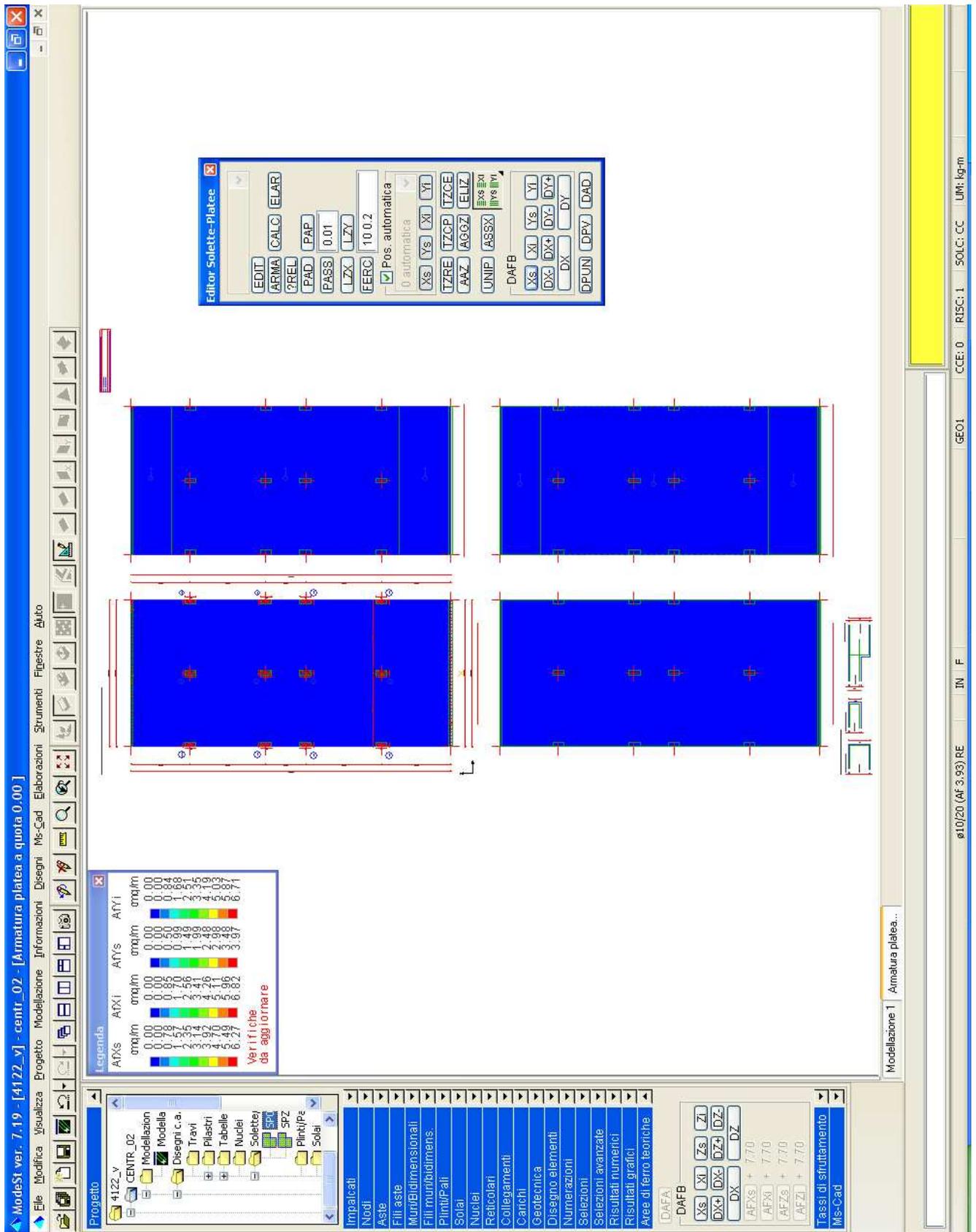
91	8.53	8.53
92	8.53	8.53
93	8.53	8.53
94	8.52	8.52
95	8.52	8.52
96	8.52	8.52
97	8.52	8.52
98	8.52	8.52
99	8.52	8.52
100	8.51	8.51
101	8.51	8.51
102	8.51	8.51
103	8.50	8.50
104	8.50	8.50
105	8.50	8.50
106	8.49	8.49
107	8.49	8.49
108	8.49	8.49
109	8.48	8.48
110	8.47	8.47
111	8.47	8.47
112	8.47	8.47
113	8.47	8.47
114	8.47	8.47
115	8.46	8.46
116	8.46	8.46
117	8.46	8.46
118	8.45	8.45
119	8.45	8.45
120	8.45	8.45

45	20.71	20.71
46	20.67	20.67
47	20.66	20.66
48	20.62	20.62
49	20.59	20.59
50	20.49	20.49
51	20.43	20.43
52	20.41	20.41
53	20.39	20.39
54	20.34	20.34
55	20.30	20.30
56	20.29	20.29
57	20.28	20.28
58	20.26	20.26
59	20.23	20.23
60	20.23	20.23
61	20.22	20.22
62	20.20	20.20
63	20.17	20.17
64	20.17	20.17
65	20.15	20.15
66	20.11	20.11
67	20.11	20.11
68	20.10	20.10
69	20.10	20.10
70	20.06	20.06
71	20.02	20.02
72	20.01	20.01
73	19.99	19.99
74	19.97	19.97
75	19.96	19.96
76	19.96	19.96
77	19.96	19.96
78	19.94	19.94
79	19.93	19.93
80	19.91	19.91
81	19.89	19.89
82	19.88	19.88
83	19.87	19.87
84	19.86	19.86
85	19.86	19.86
86	19.86	19.86
87	19.86	19.86
88	19.86	19.86
89	19.85	19.85
90	19.85	19.85
91	19.85	19.85
92	19.84	19.84
93	19.84	19.84
94	19.83	19.83
95	19.83	19.83
96	19.83	19.83
97	19.82	19.82
98	19.82	19.82
99	19.82	19.82
100	19.81	19.81
101	19.80	19.80
102	19.80	19.80
103	19.80	19.80
104	19.80	19.80
105	19.78	19.78
106	19.77	19.77
107	19.77	19.77
108	19.76	19.76
109	19.76	19.76
110	19.74	19.74
111	19.74	19.74
112	19.74	19.74
113	19.73	19.73
114	19.73	19.73
115	19.72	19.72
116	19.71	19.71
117	19.71	19.71
118	19.70	19.70
119	19.70	19.70
120	19.69	19.69

Stato limite di salvaguardia della vita

Modo	Sx	Sy
1	45.24	45.24
2	43.41	43.41
3	33.10	33.10
4	29.45	29.45
5	25.48	25.48
6	24.71	24.71
7	23.58	23.58
8	23.53	23.53
9	23.33	23.33
10	23.31	23.31
11	23.21	23.21
12	23.02	23.02
13	22.84	22.84
14	22.70	22.70
15	22.57	22.57
16	22.57	22.57
17	22.50	22.50
18	22.39	22.39
19	21.92	21.92
20	21.76	21.76
21	21.72	21.72
22	21.71	21.71
23	21.68	21.68
24	21.65	21.65
25	21.55	21.55
26	21.45	21.45
27	21.35	21.35
28	21.34	21.34
29	21.28	21.28
30	21.28	21.28
31	21.21	21.21
32	21.18	21.18
33	21.03	21.03
34	21.02	21.02
35	21.01	21.01
36	20.97	20.97
37	20.91	20.91
38	20.91	20.91
39	20.89	20.89
40	20.84	20.84
41	20.81	20.81
42	20.80	20.80
43	20.77	20.77
44	20.73	20.73

7.4. MAPPE D'ARMATURA PLATEA DI FONDAZIONE



ModeSt ver. 7.19 - [4122_y] - centr_02 - [Armatura platea a quota 0.00]

File Modifica Visualizza Progetto Modellazione Informazioni Disegni Ms-Cad Elaborazioni Strumenti Finestre Aiuto

Progetto

- 4122_y
- CENTR_02
- Modellazione
- Modello
- Disegni c.a.
- Travi
- Pilastri
- Table
- Nuclei
- Solette
- SPZ
- SPZ
- Plinti/Pz
- Solai

Impalcati

- Nodi
- Aste
- Filli aste
- Muri/Bidimensionali
- Filli multidimens.
- Plinti/Pali
- Solai
- Nuclei
- Reticolari
- Collegamenti
- Carichi
- Geotecnica
- Disegno elementi
- Numerazioni
- Selezioni avanzate
- Risultati numerici
- Risultati grafici
- Area di ferro teoriche

DAFA

- DAFB
- XS) XI) ZI) ZI
- DX+ DX- DZ+ DZ-
- DX DX- DZ
- AFXS) + 7.70
- AFXI) + 7.70
- AFXZ) + 7.70
- AFXI) + 7.70

Tassi di strutturamento

Ms-Cad

Legenda

M-MU X-	M-MU X+	M-MU Y-	M-MU Y+
0.01E+000	0.00E+000	0.00E+000	0.01E+000
-1.25E-003	-1.25E-003	-1.25E-003	-1.25E-003
-2.50E-003	-2.50E-003	-2.50E-003	-2.50E-003
-3.75E-003	-3.75E-003	-3.75E-003	-3.75E-003
-5.00E-003	-5.00E-003	-5.00E-003	-5.00E-003
-6.25E-003	-6.25E-003	-6.25E-003	-6.25E-003
-7.50E-003	-7.50E-003	-7.50E-003	-7.50E-003
-8.75E-003	-8.75E-003	-8.75E-003	-8.75E-003
-1.00E-002	-1.00E-002	-1.00E-002	-1.00E-002

Verifiche da aggiornare

Editor Solette-Platee

EDIT ARMA CALC ELAR

?REL PAD PAP PASS 0.01 LZV LZY

FERC 10.0.2

Pos. automatica

0 automatica

XS) YS) XI) YI) TZRE TZCP TZCE AAZ AGGZ ELIZ UNIP ASSX

DAFB

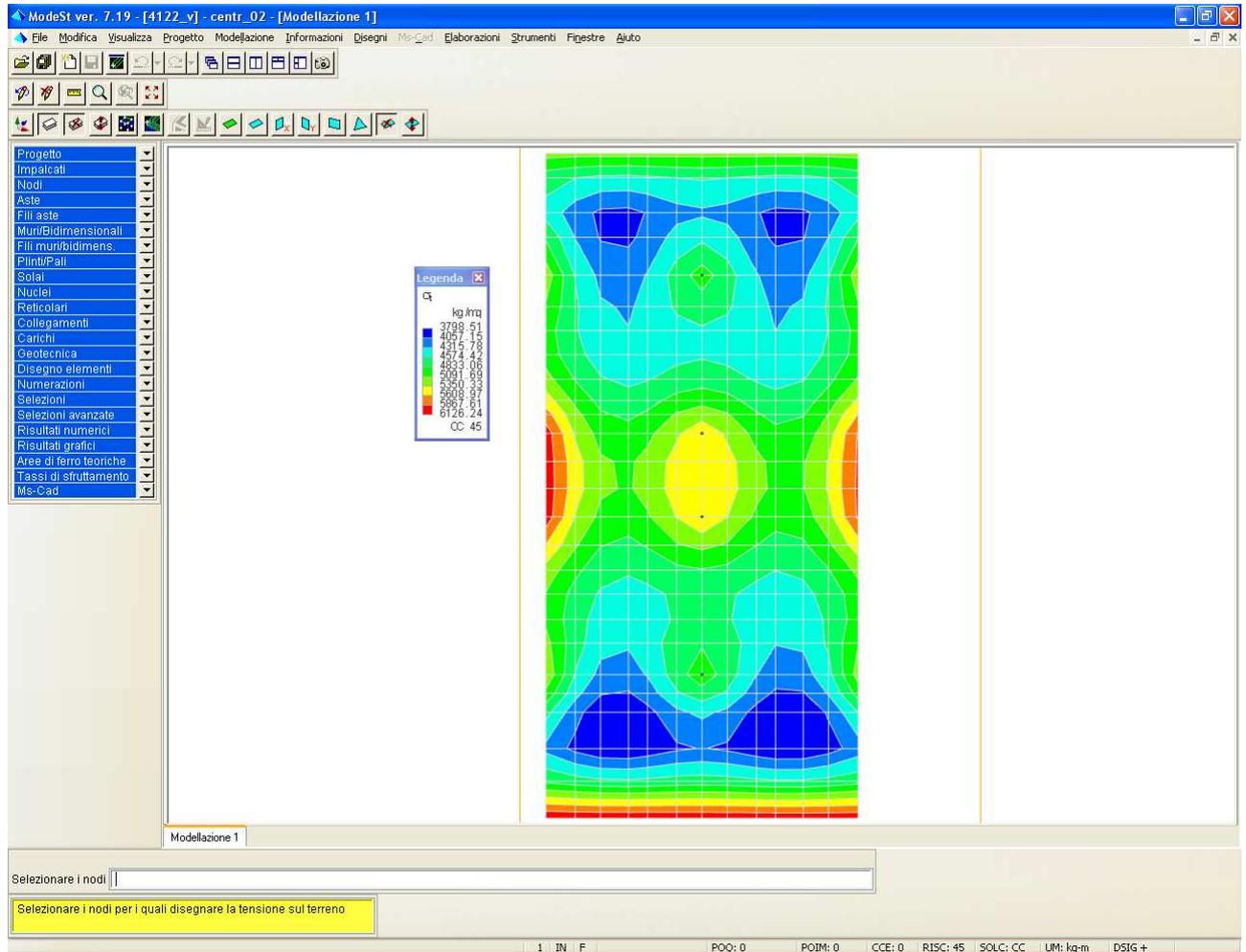
XS) XI) YS) YI) DX+ DX- DY+ DY- DPUN DPV DAD

Modellazione 1 Armatura platea...

ø10/20 (AF 3.93) RE ITN F GEO1 CCE: 0 RISC: 1 SOLC: CC UMT: Igr-m

7.5. TENSIONE SUL TERRENO

Si riporta il diagramma delle pressioni sul terreno allo SLE (cc 45)



7.6. ALLEGATI IN FORMATO DIGITALE

Ulteriori e più completi dettagli sono stati riportati sul supporto informatico allegato.

